### **PROJECT REPORT** Synthetic Minor Permit Application



### McCain Foods USA, Inc. / Othello Facility

**Prepared By:** 

Hui Cheng, P.E. – Senior Consultant Sam Najmolhoda - Consultant

#### TRINITY CONSULTANTS

20819 72<sup>nd</sup> Avenue South Suite 610 Kent, WA 98032 (253) 867-5600

April 2022

Project 224801.0006



### **TABLE OF CONTENTS**

1.	EXECUTIVE SUMMARY 1	1-1
<b>2</b> .	FACILITY DESCRIPTION 2	2-1
3.	EMISSION CALCULATIONS       3         3.1       Production Lines       3         3.1.1       Lines 1-3       3         3.1.2       Line 4       3	<b>3-1</b> <b>3-1</b> 3-1 3-2
	3.2         Boilers and HVACs         3           3.2.1         Boilers 1 and 2, Lines 1-3 HVACs         3           3.2.2         Boiler 3         3           3.2.3         Line 4 HVACs         3	<b>3-2</b> 3-2 3-2 3-3
	3.3       Flare       3         3.4       Emergency Generators       3         3.5       Facility-Wide PTE       3	3-3 3-4 3-6
4.	REGULATORY REVIEW44.1NOC Applicability44.2PSD Applicability44.3Title V Operating Permits44.4Federal Standards44.5State And Local Regulatory Applicability4	-1  -1  -1  -1  -1  -1
5.	PROPOSED PERMIT ACTIONS55.1Synthetic Minor Limits5.2Other Proposed Permit Modifications	5-1 5-1 5-2
AP	PENDIX A. PROCESS FLOW DIAGRAM A	۱-1
AP	PENDIX B. APPLICATION FORMS B	3-1
AP	PENDIX C. EMISSION CALCULATIONS	)-1
AP	PENDIX D. EQUIPMENT SPECIFICATIONS	)-1

McCain Foods USA Inc. (McCain) owns and operates a potato processing facility located in Othello, Washington (the Othello facility). The Othello facility operates under Approval Order 19AQ-E056, issued by the Washington Department of Ecology (Ecology). This approval order was issued on October 1, 2019.

Based on the emission estimates submitted in the Notice of Construction (NOC) application for Approval Order 19AQ-E056, the post-expansion project facility-wide potential to emit (PTE) exceeds the Title V Air Operating Permit (AOP) major source thresholds for oxides of nitrogen (NO<sub>X</sub>) and carbon monoxide (CO). In the NOC application, McCain stated that a Title V AOP application would be submitted within 12 months from the startup date of Line 4, in accordance with the requirements under Washington Administrative Code (WAC) 173-401-500. Line 4 started in November 2021. After reviewing historical operation data and projected production levels, McCain has elected to request emission limits that will allow the facility to remain a synthetic minor source. As a synthetic minor source, a Title V AOP application will not be required. This report constitutes McCain's application to become a synthetic minor source and includes McCain's proposed emission limits for CO and NO<sub>X</sub>.

This synthetic minor permit application contains the following sections:

- Section 2: Facility Description
- Section 3: Requested Permit Changes
- Section 4: Regulatory Review
- Appendix A: Process Flow Diagram
- Appendix B: Application Forms
- Appendix C: Emission Calculations
- Appendix D: Equipment Specifications

### 2. FACILITY DESCRIPTION

McCain operates the Othello facility under Approval Order 19AQ-E056. This order has established limits on production rates for Line 1 through 3 and separate operating limits for the recently-added Line 4. Current operations at the Othello facility include:

- Line 1 for processing battered or conventional french fry products. Line 1 includes a steam-heated dryer and a two-stage fryer.
- Line 2 for processing conventional french fry products. Line 2 includes a steam-heated dryer and a single-stage fryer.
- Line 3 for processing co-product potato products. Line 3 includes a direct-fired natural gas dryer and a single-stage fryer.
- Line 4 for processing battered, conventional and co-product potato products. Line 4 includes a potato dryer and a two-stage fryer.
- An air washer (Line 1 air washer) controlling particulate matter (PM) emissions from Line 1 Stage B of the two-stage fryer.
- > An air washer (Line 2 air washer) controlling PM emissions from Line 2 single-stage fryer.
- A wet electrostatic precipitator (the Wet ESP) controlling PM emissions from Line 3 single-stage fryer and Line 1 Stage A of the two-stage fryer.
- A wet ESP (Line 4 wet ESP) controlling PM emissions from Line 4 dryer and fryer.
- ▶ Two natural gas-fired boilers, Boiler 1 and Boiler 2, providing process steam for Lines 1 and 2.
- One natural gas and biogas-fired boiler, Boiler 3, providing process steam for Line 4.
- A flare as a backup to Boiler 3 for burning off remaining biogas.
- A scrubber for removing hydrogen sulfide from the biogas.
- A wastewater treatment plant with a covered anaerobic lagoon system.
- ▶ Heating, ventilation, and air conditioning systems (HVAC) with natural gas combustion for all lines.

A process flow diagram for the Othello facility is provided in Appendix A.

Emission calculations for the facility-wide PTE are developed using the same methodology provided in McCain's NOC application for Approval Order 19AQ-E056 with the proposed natural-gas usage limits to remain a synthetic minor source. This section describes the methodologies and assumptions used to calculate emissions from each source at the facility. Detailed emission calculations are provided in Appendix C.

### 3.1 **Production Lines**

Emissions from production lines include primarily PM and Volatile organic compound (VOC). Emissions of sulfur dioxide (SO<sub>2</sub>), NO<sub>X</sub> and CO are from Line 3 dryer only since it is natural gas-fired.

#### 3.1.1 Lines 1-3

Line 1 consists of a steam-heated dryer and a two-stage fryer and is capable of manufacturing conventional or battered french fry products. Line 2 consists of a steam-heated dryer and a single stage fryer and only manufactures conventional french fry products. Line 3 consists of a direct-fired dryer and a co-product fryer, manufacturing potato co-products only.

PM smaller than 10 microns ( $PM_{10}$ ) and smaller than 2.5 microns ( $PM_{2.5}$ ) emissions from the dryers at Lines 1, 2, and 3 are determined using Othello's dryer emission factor of 0.25 lb/finished ton product.  $PM_{10}$  and  $PM_{2.5}$  emissions from the fryers at Lines 1, 2, and 3 are connected to various control devices:

- ► Line 1 Stage A fryer exhaust and Line 3 fryer exhaust are routed to the Wet ESP. PM emissions are estimated based on the Wet ESP emission limit of 0.0262 grain per dry standard cubic feet (gr/dscf), scaled to a lb/finished ton emission factor. The emission limit for the Wet ESP is from Condition 3.d of Approval Order 19AQ-E056.
- Line 1 Stage B fryer exhaust is routed to the Line 1 Air Washer. The Stage B fryer is used for both conventional and batter products. PM emissions are estimated based on the Line 1 Air Washer test result depending on the product type, with a 20% safety factor.
- Line 2 is only used to manufacture conventional products, and the Line 2 fryer exhaust is routed to the Line 2 Air Washer. Therefore, the same emission factor from the Line 1 Air Washer for conventional products is used (including the 20% safety factor).

VOC emissions are only expected from the fryers. Since the air washers and the Wet ESP are not used to control VOC emissions, VOC emissions from all fryers are estimated based on Othello's fryer emission factor of 0.092 lb/finished ton for Lines 1 through 3.

Since the Line 3 dryer is direct fired, SO<sub>2</sub> and VOC emissions from natural gas combustion are also included using AP-42 Chapter 1.4 emission factors. NO<sub>x</sub> and CO emissions are based on a 1994 source test from McCain's Ontario, OR facility, which are the best available data for a direct-fired dryer. Speciated hazardous air pollutant (HAP) emissions are based on emission factors from Ventura County Air Pollution Control District AB2588 Combustion Emission Factors for natural gas. In the previous permit application submittal, the Line 3 dryer was conservatively calculated with a capacity of 10 MMBtu/hr. McCain confirmed the current size of the burners used at the Line 3 dryer. The dryer was retrofitted in 2011 with two 1.2 MMBtu/hr burners. This is also consistent with the equipment rating listed in Approval Order 19AQ-E056.

#### 3.1.2 Line 4

Line 4 consists of a potato dryer and a two-stage fryer, both of which are steam heated, and the line produces both conventional products and battered french fry products.

PM<sub>10</sub> and PM<sub>2.5</sub> emissions from Line 4 are controlled by the Line 4 Wet ESP. Emissions from the Line 4 Wet ESP are estimated based on McCain's recent source test performed at the Burley, ID plant. The lb/ton finished product emission factor is derived from emission testing results at the Burley, ID plant. A 20% safety factor is applied to those results to conservatively estimate emissions.

Similar to PM emissions, the lb/ton emission factor for VOC emissions from Line 4 is derived from the Burley, ID plant test results, and a 20% safety factor is applied for conservatism. Note that only total hydrocarbons (THC) were tested at Burley, and it is conservatively assumed that THC emissions are the same as VOC.

### 3.2 Boilers and HVACs

#### 3.2.1 Boilers 1 and 2, Lines 1-3 HVACs

The maximum heat inputs for Boiler 1 and Boiler 2 are 65.98 MMBtu/hr and 95.55 MMBtu/hr, respectively. Both boilers are natural gas-fired. The existing Boiler 1 and Boiler 2 were installed before 2000, and no source test data is available. Therefore, PM<sub>10</sub>, PM<sub>2.5</sub>, SO<sub>2</sub>, NO<sub>x</sub>, CO, and VOC emissions from the existing boilers are based on AP-42 Chapter 1.4 emission factors for a boiler without any control. Speciated HAP emissions are also based on emission factors from Ventura County Air Pollution Control District AB2588 Combustion Emission Factors for natural gas.

HVAC units are used exclusively for comfort air conditioning purposes. Since they are not considered fugitive sources, the emissions are included for determining major source applicability. All HVAC units at the Othello facility are natural gas-fired. Emissions of PM<sub>10</sub>, PM<sub>2.5</sub>, SO<sub>2</sub>, NO<sub>X</sub>, CO, and VOC are conservatively calculated based on AP-42 Chapter 1.4 emission factors for small boilers without any control. The total heat input of Lines 1-3 HVACs is 48.87 MMBtu/hr based on the inventory of the HVAC units. Since the emission factors for Boilers 1 and 2 and Lines 1-3 HVACs are the same, emissions from these emission units are combined using the maximum hourly heat input of 210.4 MMBtu/hr, and the natural gas limit of 1,314.28 million standard cubic feet per year (scf/year) under Condition 1.f of Approval Order 19AQ-E056.

#### 3.2.2 Boiler 3

Boiler 3 fires both natural gas and biogas. When biogas generation rate is low or biogas is unable to be routed to the boiler, Boiler 3 fires natural gas only. Therefore, emissions are calculated for two scenarios: natural gas only, and dual fuel (biogas and natural gas).

Emissions of PM<sub>10</sub>, PM<sub>2.5</sub>, SO<sub>2</sub>, and VOC from firing natural gas are calculated using emission factors from AP-42 Chapter 1.4, for small boilers less than 100 MMBtu/hr. NO<sub>x</sub> and CO emissions are estimated based on the burner emission limit of 30 and 50 parts per million (ppm), respectively, at 3% oxygen per Condition 4.e of Approval Order No. 19AQ-E056. Emissions from natural gas combustion are based on the maximum heat input of 97.6 MMBtu/hr. The PTE for the natural gas combustion scenario is based on the natural gas usage limit of 838.3 million scf/yr, per Condition 2.c of Approval Order 19AQ-E056.

When firing dual fuel, biogas will provide a portion of the heat input. On an hourly basis, the emission calculations are based on the maximum hourly biogas generation rate of 850 standard cubic feet per minute

(scfm). On an annual basis, the maximum biogas generation rate is limited to 325 million scf per Condition 4.e.vii of Approval Order No. 19AQ-E056. Emissions of PM<sub>10</sub>, PM<sub>2.5</sub>, and VOC are not expected to be different for biogas and natural gas combustion; therefore, emissions of these pollutants from dual fuel firing use the same emission factors from AP-42 Chapter 1.4. Emissions of NO<sub>X</sub> and CO are dependent on the burner design; therefore, NO<sub>X</sub> and CO emissions during dual fuel firing are based on the emission limits of 30 and 50 ppm, respectively.

Emissions of SO<sub>2</sub> when firing dual fuel are determined by the hydrogen sulfide (H<sub>2</sub>S) content of the biogas. The H<sub>2</sub>S content in the biogas stream is expected to be as high as 5000 ppm. McCain installed a sulfur scrubber to remove H<sub>2</sub>S from the biogas and has an outlet concentration limit of 200 ppm H<sub>2</sub>S. Emissions of SO<sub>2</sub> and H<sub>2</sub>S from biogas combustion assume 98% destruction efficiency of H<sub>2</sub>S converting to SO<sub>2</sub> in the waste stream after scrubber treatment. Hourly and annual SO<sub>2</sub> total emissions for the dual fuel scenario also includes natural gas combustion emissions, in supplement to the heat input provided by biogas.

Speciated pollutants, including HAPs, are based on emission factors from Ventura County Air Pollution Control District AB2588 Combustion Emission Factors. This source provides emission factors for natural gas external combustion sources in the size range of 10-100 MMBtu/hr in units of Ib/MMscf, but does not specify the heating value to convert the factors from Ib/MMscf to Ib/MMBtu. For biogas, our emission calculations assume that the natural gas external combustion factors are representative, even though the heating value of biogas is much lower than that of natural gas. To adjust for the difference in heating value between natural gas and biogas, the Ib/MMscf natural gas factors are applied to the biogas combustion rate in scfm directly, which is conservative for estimating speciated HAP emissions from biogas combustion.

#### 3.2.3 Line 4 HVACs

Similar to Lines 1-3 HVACs, the Line 4 HVACs are used exclusively for comfort air conditioning purposes and all are natural gas-fired. McCain proposes a limit of 95 million scf/yr (96,900 MMBtu/yr) limit for Line 4 HVACs instead of the limit of 573,000 MMBtu/yr per Condition 4.a of Approval Order 19AQ-E056. Emissions of PM<sub>10</sub>, PM<sub>2.5</sub>, SO<sub>2</sub>, NO<sub>x</sub>, CO, and VOC are conservatively calculated based on AP-42 Chapter 1.4 emission factors for small uncontrolled boilers.

McCain proposes a facility-wide natural gas usage limit (in addition to the Boiler 3 natural gas usage limit) to establish the  $NO_X$  and CO limits that will make McCain's Othello plant a synthetic minor source. For simplicity and to allow for maximum operational flexibility for other combustion sources, it is assumed for the purposes of the PTE that each of the other combustion sources will operate at capacity, and the natural gas usage limit is factored into the calculations via HVAC unit combustion. Details of the proposed limits are included in Section 5 below.

### 3.3 Flare

A flare is used to burn off any generated biogas that cannot be routed to Boiler 3 for use. The flare uses propane as the pilot gas. To conservatively estimate the emissions from the flare, the emissions presented in this section assume a scenario in which all biogas generated is routed to the flare (i.e., 850 scfm and 325 million scf per year).

Emissions of PM<sub>10</sub>, PM<sub>2.5</sub>, NO<sub>x</sub>, and CO from biogas combustion are estimated based on flare factors from AP-42 Chapter 2.4, Municipal Solid Waste Landfills (October 2008 draft version). The factors for landfill flares are representative of biogas combustion, because the heating value of biogas is similar to that of landfill gas (both are about half the heating value of natural gas). Additionally, these factors are listed on the basis of standard cubic foot methane burned, which should provide a representative estimate for biogas

combustion when adjusted to the heating value of biogas. The lb/million dscf methane factor is converted to lb/MMBtu using methane's high heating value (HHV) of 1011 Btu/scf.

VOC emissions from the flare are conservatively estimated using the AP-42 Chapter 1.4 factor for boiler natural gas combustion. The factor in Ib/MMscf is converted to Ib/MMBtu using the default natural gas heating value of 1020 Btu/scf.

 $SO_2$  and  $H_2S$  emissions are estimated using the mass balance approach, assuming the sulfur scrubber reduces the  $H_2S$  content of the biogas to 200 ppm, and the flare achieves a 98% destruction efficiency of  $H_2S$ , equaling the sulfur oxide (SO<sub>x</sub>) limit of 1.78 lb/hr.

Propane combustion emissions from the flare pilot are estimated based on the AP-42 Chapter 1.5 factors. Note that the estimated propane usage is 8,400 gallons per year based on limited data from flare operations since the startup of the wastewater treatment plant. The emission estimates provided in the original NOC application was based on actual propane usage at another facility which has a different flare make/model. The actual propane usage at the Othello facility is higher than the original estimate because the use of pilot gas is continuous to avoid flame-out. Since propane emissions account for less than 5% of the total emissions at the flare, the flare emissions affect facility-wide emissions marginally. Table 3-1 shows the comparison of the emission estimates from the originally application and with the updated propane usage rate.

	Emission Rates	S Provided in NOC		
	Application for No. 19AQ-E056		Updated Emis	ssion Rates
Pollutant	(lb/hr)	(tpy)	(lb/hr)	(tpy)
PM10 / PM2.5	0.48	1.53	0.48	1.54
SO <sub>2</sub>	1.78	5.68	1.78	5.68
NOx	1.25	3.99	1.26	4.04
VOC	0.18	0.56	0.18	0.56
СО	1.48	4.71	1.48	4.73
H <sub>2</sub> S	0.02	0.06	0.02	0.06
HAPs	0.15	0.48	0.15	0.48
CO <sub>2</sub> e	3,745	11,932	3,755	11,977

#### Table 3-1. Flare Emission Comparison

Similar to Boiler 3 emissions, speciated HAP emissions are based on emission factors from Ventura County Air Pollution Control District AB2588 Combustion Emission Factors. The heating values of propane and biogas are used to convert the factors provided in Ib/MMscf to Ib/MMBtu.

### 3.4 **Emergency Generators**

McCain operates two emergency generators at the Othello facility. The first generator has a Cummins engine with a maximum engine output of 465 horsepower (hp). This engine was manufactured in 1996 and therefore predates NSPS Subpart IIII promulgation. Therefore, emission factors for criteria pollutants for the PTE calculations are taken from the EPA's AP-42, Table 3.3-1 Emission Factors for Uncontrolled Gasoline and Diesel Industrial Engines. Emission factors for greenhouse gas (GHG) emissions are obtained from 40 CFR 98, Tables C-1 and C-2.

The second emergency generator is a Caterpillar C9 generator with a Tier III certified engine and a maximum engine output of 480 hp. Therefore, for the purposes of PM, CO, and NO<sub>x</sub> emissions calculations

the Tier III limits for those pollutants is used for the PTE calculations. SO<sub>2</sub> emissions calculations are obtained from AP-42 Table 3.3-1. For PM<sub>10</sub> and PM<sub>2.5</sub> emissions, the combined filterable and condensable PM emissions are conservatively assumed to be equal to the filterable PM emissions plus the total hydrocarbon (HC) emissions. All HC are assumed to be VOC, and the highest HC emission rate across all operating loads specified in vendor specifications are conservatively used to calculate VOC, PM<sub>10</sub>, and PM<sub>2.5</sub> emissions. As with the first emergency generator, emission factors for GHG emissions are obtained from 40 CFR 98, Tables C-1 and C-2.

For calculating PTE, it is assumed that all generators will operate up to 500 hours per year in accordance with U.S. EPA policy for estimating PTE for emergency engines.<sup>1</sup>

In both instances, the emergency generators have a brake horsepower (bhp) of less than 500 bhp. Therefore, the generators are exempt from permitting under Washington's minor new source review program per WAC 173-400-110(4)(h)(xxxix). Because the emergency generators are not a fugitive source as defined in WAC 173-401, the emissions are included when determining the facility-wide PTE for the purposes of Title V applicability.

<sup>&</sup>lt;sup>1</sup> The generators will only be used as emergency backup generators. Per U.S. EPA memorandum for emergency equipment that was authored by John S. Seitz, dated September 6, 1995, (<u>https://www.epa.gov/sites/production/files/2015-</u>08/documents/emgen.pdf), "500 hours is an appropriate default of assumption for estimating the number of hours that an emergency generator could be expected to operate under worst-case conditions".

### 3.5 Facility-Wide PTE

A summary of the PTE for the Othello facility, after accounting for the requested synthetic minor permit limits, is provided in Table 3-1 below.

Emission Point	Annual Emission Rate (tpy)							
	<b>PM</b> <sub>10</sub>	PM <sub>2.5</sub>	SO <sub>2</sub>	NOx	VOC	СО	HAPs	CO <sub>2</sub> e
Line 1	35.29	35.29			15.76			
Line 2	30.64	30.64			7.88			
Line 3	7.81	7.81	0.01	1.58	2.08	3.84	8.45E-04	1,231
Boiler 1 & 2, Lines 1-3 HVACs	4.92	4.92	0.39	64.68	3.56	54.33	0.05	77,258
Boiler 3	3.19	3.19	5.87	15.57	2.31	15.78	0.04	50,058
Line 4	8.41	8.41			53.59			
Flare	1.54	1.54	5.68	4.04	0.56	4.73	0.48	11,977
Line 4 HVAC Systems	0.36	0.36	0.03	4.75	0.26	3.99	3.90E-03	5,673
Emergency Generators	0.32	0.32	0.48	4.39	0.31	1.47	6.12E-03	259
Facility-Wide Potential Emissions	92.5	92.5	12.5	95.0	86.3	84.1	0.6	146,456
Title V Threshold	100	100	100	100	100	100	25	
Title V Required?	No	No	No	No	No	No	No	

#### Table 3-2. Facility-Wide Potential To Emit (tpy)

This section identifies the regulatory requirements applicable to the proposed permitting actions.

### 4.1 NOC Applicability

An NOC permit application must be filed and an approval order issued by Ecology prior to the construction or modification of an affected facility per WAC 173-400-110(2)(a). The only emission units included in the PTE above that were not previously represented in Order of Approval No. 19AQ-E056 were the emergency engines. However, per WAC 173-400-110(4)(h)(xxxix), emergency engines with a maximum combustion rating of 500 hp or less are exempt from NOC permitting. Therefore, no emission units are subject to the NOC review requirements under WAC 173-400-110 through -114. An NOC application is required for modifying Approval Order No. 19AQ-E056 to establish the synthetic minor limits.

Additionally, estimated emissions from the flare have increased compared to the original application due to new information. McCain proposes to revise the emission limits for the flare under Condition 4.c of Approval Order No. 19AQ-E056 as part of this permit modification effort.

### 4.2 **PSD Applicability**

PSD is the major New Source Review permitting program for attainment pollutants. The Othello facility is located in Adams County, which is an attainment area for all criteria pollutants. Currently, the Othello facility is not a major source under the PSD program. There is no construction or modification associated with the establishment of synthetic minor status. Therefore, PSD review is not required for this permit action.

### 4.3 Title V Operating Permits

The Othello facility is currently operated under Approval Order No. 19AQ-E056, indicating a Title V permit application would be required within 12 months of startup of Line 4. Based on McCain's review of historical data and projections for future productions, McCain is proposing to establish synthetic minor limits to keep the PTE of the Othello facility below Title V major source thresholds. Therefore, the Title V operating permit requirements under WAC 173-410 does not apply.

### 4.4 Federal Standards

WAC 173-400-115 adopts federal New Source Performance Standards (NSPS) by reference. NSPS apply to certain types of equipment that are newly constructed, modified, or reconstructed after a given applicability date. Since no construction or physical modification of any equipment is taking place, there will be no change to NSPS applicability or requirements to the existing equipment.

National Emission Standards for Hazardous Air Pollutants (NESHAPs) have been established in 40 CFR Part 61 and Part 63 to control emissions of HAP from stationary sources. This permitting application does not impact existing requirements or trigger any additional NESHAP requirements at the facility.

### 4.5 State And Local Regulatory Applicability

There are no physical changes or new sources proposed as part of this permit action. However, the propane usage at the flare is higher than the estimated usage provided in the original NOC application, resulting in

and emission increase in NO<sub>x</sub>, CO, VOC, and TAPs. Therefore, the regulatory applicability discussions below focus on these emissions.

### 4.5.1 Washington Toxic Air Pollutant Regulations

In Washington, all new sources emitting TAPs are required to demonstrate compliance with the Washington TAP program pursuant to WAC 173-460. Ecology has established a de minimis emission rate, a small quantity emission rate (SQER), and an acceptable source impact level (ASIL) for each listed TAP. If the total project-related TAP emissions increase exceeds the de minimis level for a pollutant, then permitting and a control technology review is triggered. If the emissions increases exceed their respective SQERs, further determination of compliance with the ASIL using air dispersion modeling is required.

With the proposed higher propane usage at the flare, TAP emissions are updated from the original application. In the original application, six TAPs had Line 4 project emissions greater than the SQER, and dispersion modeling analysis was performed to demonstration compliance with the ASILs for these six TAPs. As mentioned in Section 3.3, the updated propane emissions only increase the total TAP emissions marginally (less than 1% increase for all TAPs). Table 4-1 shows the updated TAP emissions compared to the current version of WAC 173-460-150. The updated emissions show that only five TAPs (i.e., less acrolein) exceed the SQER and require compliance demonstration against the ASILs.

Pollutant	Averaging Period	Updated Project Emission Rate <sup>a</sup>	Emission Rates from Original Application	De Minimis <sup>b</sup>	SQER <sup>b</sup>	Modeling Required?	Increase Compared to Original Application °
Ponzono	Voor	57.20	57 25		2 1E 1 01	Voc	0.07%
	Teal	37.29	37.25	1.0E+00	2.12+01	Tes	0.07 %
Formaldenyde	Year	392.05	391.75	1.4E+00	2.7E+01	Yes	0.08%
Naphthalene	Year	3.87	3.86	2.4E-01	4.8E+00	No	0.07%
Acetaldehyde	Year	16.96	16.95	3.0E+00	6.0E+01	No	0.07%
Acrolein	24-hr	0.02	0.02	1.3E-03	2.6E-02	No	0.04%
Propylene	24-hr	4.45	4.45	1.1E+01	2.2E+02	De Minimis	0.04%
Toluene	24-hr	0.14	0.14	1.9E+01	3.7E+02	De Minimis	0.03%
Xylenes	24-hr	0.09	0.09	8.2E-01	1.6E+01	De Minimis	0.02%
Ethyl Benzene	Year	476.31	475.94	3.2E+00	6.5E+01	Yes	0.08%
Hexane	24-hr	0.05	0.05	2.6E+00	5.2E+01	De Minimis	0.04%
H <sub>2</sub> S	24-hr	0.93	0.93	7.4E-03	1.5E-01	Yes	0.00%
SO <sub>2</sub>	1-hr	3.60	3.60	4.6E-01	1.2E+00	Yes	0.00%
NO <sub>2</sub>	1-hr	0.48	0.48	4.6E-01	8.7E-01	No	0.22%
CO	1-hr	5.08	5.08	1.1E+00	4.3E+01	No	0.14%

#### Table 4-1. Updated TAP Emissions Summary

a. Project emissions are conservatively determined to be the sum of the dual fuel scenario for the new boiler and the projected biogas emissions for the flare for all TAPs.

b. De Minimis and SQER are updated to WAC 173-460-150 (effective December 31, 2019).

c. No emission increase to H<sub>2</sub>S and SO<sub>2</sub> because they are driven by biogas combustion.

The dispersion modeling analysis performed with the original application demonstrated that the modeled concentrations from Boiler 3 and the flare combined were 1-2% of the respective ASILs. Since the propane

emissions increases from the original application are marginal, the model results for these five TAPs are scaled based on the modeled concentrations from the original application. The estimated model results for the increased propane usage at the flare and the comparison to the current ASILs are provided in Table 4-2. As shown in Table 4-2, the model results have no noticeable increase from the modeled concentrations submitted in the original application, and remain well below the respective ASILs. Therefore, no further analysis is required.

Pollutant	Averaging Period	Modeled Concentration in Original Application <sup>a</sup> (µq/m <sup>3</sup> )	Estimated Model Results <sup>b</sup> (µq/m <sup>3</sup> )	Current ASIL (µq/m <sup>3</sup> )	% of ASIL
Benzene	Year	0.0005	0.0005	3.7E-01	0%
Formaldehyde	Year	0.003	0.003	1.7E-01	2%
Ethyl Benzene	Year	0.004	0.004	4.0E-01	1%
$H_2S$	24-hr	0.03	0.03	2.0E+00	1%
SO <sub>2</sub>	1-hr	8	8	6.6E+02	1%

Table 4-2. Updated TAP Results

a. The modeled concentration represents the total impact from Boiler 3 (firing dual fuel) and the flare (including pilot gas). The results are conservative because the flare would not be operated if all biogas generated is fired at Boiler 3.

b. The estimated model results are simply scaling the modeled concentrations from the original application by the percentage increase in the emission rates from Table 4-1.

### 5.1 Synthetic Minor Limits

As noted in the NOC application for Order of Approval No. 19AQ-E056, potential NO<sub>X</sub> and CO emissions may be above the Title V major source threshold of 100 tpy after startup of Line 4. McCain is requesting synthetic minor limits to constrain potential emissions from the Othello facility to levels below the major source threshold. Since NO<sub>X</sub> and CO emissions are solely generated from combustion, the synthetic minor limits will be focused on natural gas usage for various emission units.

Currently, Order of Approval No. 19AQ-E056 includes the following operation limits:

- Condition 1.f: Lines 1-3, Boilers 1 and 2, Line 3 dryer, and Lines 1-3 HVACs should be limited to 1,314.28 million cubic feet per calendar year;
- Condition 2.c: The annual natural gas usage for Boiler 3 is limited to 838.3 million standard cubic feet per year, or 855,000 MMBtu per year.
- Condition 4.a: The natural gas for the Line 4 HVAC units is limited to a combined 65.35 MMBtu/yr or 573,000 MMBtu/yr or less.
- Condition 4.e.vii: The biogas fed to Boiler 3 during dual fire scenario is limited to 850 standard cubic feet per minute or 325 million standard cubic feet per year.

Based on McCain's review of historical natural gas usage and projected production rates, McCain proposes to change the natural gas usage limit for Line 4 HVAC units to 96,900 MMBtu per year. The other limits will remain applicable to the site, but McCain proposes to convert all natural gas usage limits to a MMBtu per year basis to be consistent throughout the facility and for the ease of demonstrating compliance.<sup>2</sup> This approach will result in a facility-wide natural gas usage limit of 2,292,442 MMBtu per year. In addition, McCain proposes a 95 tpy NO<sub>X</sub> emission limit for the Othello facility. Lastly, limiting the natural gas usage for these units will reduce the facility-wide PTE for CO to 84 tpy. Therefore, McCain does not propose a separate CO emission limit for the Othello facility.

In order to demonstrate compliance against the operation limits and the 95 tpy NO<sub>x</sub> limit for the Othello facility, McCain proposes the following monitoring method:

- McCain will record the facility-wide natural gas usage determined by natural gas bills on a monthly basis.
- If any 12-month rolling facility-wide natural gas usage exceeds 1,340,566 MMBtu (equivalent to 1,314.28 million scf), McCain will review the monthly natural gas usage for the following units to compare against their applicable natural gas usage limits for that 12-month period:
  - Boilers 1 and 2, Line 3 dryer, and Lines 1-3 HVACs combined natural gas usage should not exceed 1,340,566 MMBtu determined by the natural gas bills for Lines 1-3;
  - Boiler 3 natural gas usage should not exceed 854,976 MMBtu determined by natural gas bills for Boiler 3;
  - Line 4 HVACs natural gas usage should not exceed 96,900 MMBtu determined by the Line 4 total usage and Boiler 3 usage.

<sup>&</sup>lt;sup>2</sup> The natural gas usage is billed on therms basis, which can be converted to MMBtu without any adjustment for standard conditions.

### 5.2 Other Proposed Permit Modifications

McCain proposes the following modifications or removal for the conditions in Order of Approval No. 19AQ-E056:

- Equipment table on the first page of the permit:
  - Change the manufacturer for item 8 to "Eclipse Combustion". As mentioned in Section 3.1.1, the Line 3 dryer were retrofit in 2011 with two 1.2 MMBtu/hr Eclipse burners. The rating of 3.2 MMBtu/hr is incorrect. A copy of the Eclipse burner specification is provided in Appendix D.
  - Change the equipment rating for Items 10-12 to their respective maximum heat input. The capacities of the Boilers 1 and 2 and Lines 1-2 HVACs are provided in Section 3.2.1.
- Condition 1.f: Remove "in order to limit nitrogen oxide emissions to no more than 92 tons per calendar year" from this condition. McCain is proposing a new facility-wide NO<sub>x</sub> emission limit of 95 tpy and this NO<sub>x</sub> limit on units for Lines 1-3 will potentially be conflicting and confusing for permit compliance.
- Condition 1.h: Remove this condition. Condition 1.h is solely used to explain the basis for setting the 92 tpy limits for PM and NO<sub>x</sub> for Lines 1-3 and procedures for adjustment of the limits. With the proposed facility-wide NO<sub>x</sub> limit, this condition will no longer be valid since a new permit will be issued.
- Condition 2.e.i: Remove this condition. Condition 2.e.i sets a temperature limit for the flare. However, temperature measurement is not feasible for an open-flame flare. The flare is firing propane continuously which ignites the biogas when sending to the flare. Additionally, the flare has an auto-restart system preventing flame-out. The design and proper operational practices of the flare will ensure the flare is operating in design conditions; thus a temperature limit is not necessary for compliance.
- Condition 4.a: Change the natural gas limit for Line 4 HVACs from "573,000 MMBtu/yr" to "96,900 MMBtu per year" to match the proposed synthetic minor limit.
- ► Condition 4.c: Change the NO<sub>X</sub>, CO and VOC limits with the updated propane usage rate. Specifically:
  - NOx to 1.26 lb/hr, 4.04 ton/yr;
  - CO to 1.48 lb/hr, 4.73 ton/yr; and
  - VOC to 0.18 pounds per hour.
- Condition 4.e.v: Add "when firing natural gas" for the SO<sub>x</sub> limit of 0.04 pounds per hour. This limit is consistent with the emission calculations submitted for Order of Approval No. 19AQ-E056 and Appendix C. The hourly SO<sub>x</sub> emission rate will be higher when firing biogas because of higher sulfur content in biogas compared to natural gas.
- Condition 4.e.vii: Add "on an hourly basis" for the 850 standard cubic feet per minute limit. McCain tracks the biogas generation rate instantaneously and the reading could be higher than 850 scfm but the hourly flow rate is expected to be lower than 51,000 scf. Adding the clarification here would avoid potential compliance issues.

APPENDIX A. PROCESS FLOW DIAGRAM



**APPENDIX B. APPLICATION FORMS** 



A notice of construction permit is required before installing a new source of air pollution or modifying an existing source of air pollution. This application applies to facilities in Ecology's jurisdiction. Submit this application for review of your project. For general information about completing the application, refer to Ecology Forms ECY 070-410a-g, "Instructions for Ecology's Notice of Construction Application."

Ecology offers up to two hours of free pre-application assistance. We encourage you to schedule a pre-application meeting with the contact person specified for the location of your proposal, below. If you use up your two hours of free pre-application assistance, we will continue to assist you after you submit Part 1 of the application and the application fee. You may schedule a meeting with us at any point in the process.

Upon completion of the application, please enclose a check for the initial fee and mail to:

Department of Ecology Cashiering Unit P.O. Box 47611 Olympia, WA 98504-7611 For Fiscal Office Use Only: 001-NSR-216-0299-000404

C	Check the box for the location of your proposal. For assistance, call the contact listed below:				
	Ecology Permitting Office	Contact			
CRO	<b>Chelan, Douglas, Kittitas, Klickitat, or Okanogan County</b> Ecology Central Regional Office – Air Quality Program	Lynnette Haller (509) 457-7126 <u>lynnette.haller@ecy.wa.gov</u>			
ERO	Adams, Asotin, Columbia, Ferry, Franklin, Garfield, Grant, Lincoln, Pend Oreille, Stevens, Walla Walla or Whitman County Ecology Eastern Regional Office – Air Quality Program	Karin Baldwin (509) 329-3452 <u>karin.baldwin@ecy.wa.gov</u>			
	<b>San Juan County</b> Ecology Northwest Regional Office – Air Quality Program	David Adler (425) 649-7267 <u>david.adler@ecy.wa.gov</u>			
	For actions taken at Kraft and Sulfite Paper Mills and Aluminum Smelters Ecology Industrial Section – Waste 2 Resources Program Permit manager:	James DeMay (360) 407-6868 james.demay@ecy.wa.gov			
NWP	For actions taken on the US Department of Energy Hanford Reservation Ecology Nuclear Waste Program	Lilyann Murphy (509) 372-7951 <u>lilyann.murphy@ecy.wa.gov</u>			

Check the box below for the fee that applies to your application.



#### New project or equipment:

	<b>\$1,500:</b> Basic project initial fee covers up to 16 hours of review.
\$10,000: Complex project initial fee covers up to 106 hours of review.	<b>\$10,000:</b> Complex project initial fee covers up to 106 hours of review.

#### Change to an existing permit or equipment:

	<b>\$200:</b> Administrative or simple change initial fee covers up to 3 hours of review
	Ecology may determine your change is complex during completeness review of your application. If your project is complex, you must pay the additional \$675 before we will continue working on your application.
$\bowtie$	<b>\$875:</b> Complex change initial fee covers up to 10 hours of review
	\$350 flat fee: Replace or alter control technology equipment under WAC 173-400-114
	Ecology will contact you if we determine your change belongs in another fee category. You must pay the fee associated with that category before we will continue working on your application.

Read each	n statement, then check the box next to it to acknowledge that you agree.
	The initial fee you submitted may not cover the cost of processing your application. Ecology will track the number of hours spent on your project. If the number of hours Ecology spends exceeds the hours included in your initial fee, Ecology will bill you \$95 per hour for the extra time.
	You must include all information requested by this application. Ecology may not process your application if it does not include all the information requested.
$\square$	Submittal of this application allows Ecology staff to visit and inspect your facility.



### **Notice of Construction Application** Part 1: General Information

#### I. Project, Facility, and Company Information

1. Project Name
Synthetic Minor Status
2. Facility Name
McCain Foods USA, Inc.
3. Facility Street Address
100 Lee Street, Othello, WA 99344
4. Facility Legal Description
NW 1/4 of the NW 1/4 of sec. 34 T 16 N., R 29, E.W.M. Farm Unit 89 in Block 45, Parcel
#2629280120001
5. Company Legal Name (if different from Facility Name)
6. Company Mailing Address (street, city, state, zip)

#### **II.** Contact Information and Certification

1. Facility Contact Name (who will be onsite) John Lallas					
2. Facility Contact Mailing Address (if different that	2. Facility Contact Mailing Address (if different than Company Mailing Address)				
100 Lee Street, Othello, WA 99344	1				
3. Facility Contact Phone Number	4. Facility Contact E-mail				
(509) 331-7734 john.lallas@mccain.com					
5. Billing Contact Name (who should receive billing information)					
John Lallas					
6. Billing Contact Mailing Address (if different than	Company Mailing Address)				
100 Lee Street, Othello, WA 99344					
7. Billing Contact Phone Number	8. Billing Contact E-mail				
(509) 331-7734 John.lallas@mccain.com					
9. Consultant Name (optional – if $3^{rd}$ party hired to complete application elements)					
Hui Cheng					
10. Consultant Organization/Company					
Trinity Consultants					
11. Consultant Mailing Address (street, city, state, zip)					
20819 72 <sup>nd</sup> Avenue S, Suite 610, Kent, WA 98032					
12. Consultant Phone Number	13.Consultant E-mail				
(253) 867-5600 x 1003 hcheng@trinityconsultants.com					
14. Responsible Official Name and Title (who is responsible for project policy or decision-making)					
Evan Buell, Vice President of Engineering					
15. Responsible Official Mailing Address					
One Tower Lane, Oakbrook Terrance, IL 60181					
16. Responsible Official Phone 17. Responsible Official E-mail					
(858) 699-6495 Evan.buell@mccain.com					
18. Responsible Official Certification and Signature					
I certify that the information on this application is acc	I certify that the information on this application is accurate and complete.				
Fac 15 M	April 20, 2022				
Signature Now Net	Date				



### Part 2: Technical Information

The Technical Information may be sent with this application form to the Cashiering Unit, or may be sent directly to the Ecology regional office with jurisdiction along with a copy of this application form.

For all sections, check the box next to each item as you complete it.

#### **III. Project Description**

Please attach the following to your application.

Written narrative describing your proposed project.

Projected construction start and completion dates.

Operating schedule and production rates.

⊠ List of all major process equipment with manufacturer and maximum rated capacity.

Process flow diagram with all emission points identified.

Plan view site map.

Manufacturer specification sheets for major process equipment components.

Manufacturer specification sheets for pollution control equipment.

Fuel specifications, including type, consumption (per hour & per year) and percent sulfur.

#### IV. State Environmental Policy Act (SEPA) Compliance

#### Check the appropriate box below.

SEPA review is complete:

Include a copy of the final SEPA checklist and SEPA determination (e.g., DNS, MDNS, EIS) with your application.

SEPA review has not been conducted:

If review will be conducted by another agency, list the agency. You must provide a copy of the final SEPA checklist and SEPA determination before Ecology will issue your permit. Agency Reviewing SEPA:

If the review will be conducted by Ecology, fill out a SEPA checklist and submit it with your application. You can find a SEPA checklist online at <a href="https://ecology.wa.gov/Regulations-Permits/SEPA/Environmental-review/SEPA-document-templates">https://ecology.wa.gov/Regulations-Permits/SEPA/Environmental-review/SEPA-document-templates</a>



### V. Emissions Estimations of Criteria Pollutants

### **Does your project generate criteria air pollutant emissions?** 🖂 Yes 🗌 No

If yes, please provide the following information regarding your criteria emissions in your application.

 $\boxtimes$  The names of the criteria air pollutants emitted (i.e., NO<sub>x</sub>, SO<sub>2</sub>, CO, PM<sub>2.5</sub>, PM<sub>10</sub>, TSP, VOC, and Pb)

 $\boxtimes$  Potential emissions of criteria air pollutants in tons per hour, tons per day, and tons per year (include calculations)

If there will be any fugitive criteria pollutant emissions, clearly identify the pollutant and quantity

### VI. Emissions Estimations of Toxic Air Pollutants

### **Does your project generate toxic air pollutant emissions?** 🖂 Yes 🗌 No

If yes, please provide the following information regarding your toxic air pollutant emissions in your application.

 $\boxtimes$  The names of the toxic air pollutants emitted (specified in <u>WAC 173-460-150</u><sup>1</sup>)

 $\boxtimes$  Potential emissions of toxic air pollutants in pounds per hour, pounds per day, and pounds per year (include calculations)

If there will be any fugitive toxic air pollutant emissions, clearly identify the pollutant and quantity

### **VII. Emission Standard Compliance**

Provide a list of all applicable new source performance standards, national emission standards for hazardous air pollutants, national emission standards for hazardous air pollutants for source categories, and emission standards adopted under Chapter 70.94 RCW.

**Does your project comply with all applicable standards identified?** Xes No

### VIII. Best Available Control Technology

Provide a complete evaluation of Best Available Control Technology (BACT) for your proposal.

<sup>&</sup>lt;sup>1</sup> <u>http://apps.leg.wa.gov/WAC/default.aspx?cite=173-460-150</u>



#### IX. Ambient Air Impacts Analyses

Please provide the following:

- Ambient air impacts analyses for Criteria Air Pollutants (including fugitive emissions)
- Ambient air impacts analyses for Toxic Air Pollutants (including fugitive emissions)

Discharge point data for each point included in air impacts analyses (include only if modeling is required)

- Exhaust height
- Exhaust inside dimensions (ex. diameter or length and width)
- Exhaust gas velocity or volumetric flow rate

Exhaust gas exit temperature

The volumetric flow rate

- Description of the discharges (i.e., vertically or horizontally) and whether there are any obstructions (ex., raincap)
- Identification of the emission unit(s) discharging from the point
- The distance from the stack to the nearest property line
- Emission unit building height, width, and length
- Height of tallest building on-site or in the vicinity and the nearest distance of that building to the exhaust
- Whether the facility is in an urban or rural location

## **Does your project cause or contribute to a violation of any ambient air quality standard or acceptable source impact level?** $\Box$ Yes $\bigotimes$ No

Table C-1a.	Potential	Emission	Summary

	Annual Emission Rate (tpy)							
Emission Point	PM <sub>10</sub>	PM <sub>2.5</sub>	SO <sub>2</sub>	NO <sub>x</sub>	VOC	СО	HAPs	CO <sub>2</sub> e
Line 1	35.29	35.29			15.76			
Line 2	30.64	30.64			7.88			
Line 3 <sup>a</sup>	7.81	7.81	6.18E-03	1.58	2.08	3.84	8.45E-04	1,231
Boiler 1 & 2, Lines 1-3 HVACs <sup>a</sup>	4.92	4.92	0.39	64.68	3.56	54.33	0.05	77,258
Boiler 3	3.19	3.19	5.87	15.57	2.31	15.78	0.04	50,058
Line 4	8.41	8.41			53.59			
Flare	1.54	1.54	5.68	4.04	0.56	4.73	0.48	11,977
Line 4 HVAC Systems	0.36	0.36	0.03	4.75	0.26	3.99	3.90E-03	5,673
Emergency Generators	0.32	0.32	0.48	4.39	0.31	1.47	6.12E-03	259
Facility-Wide Potential Emissions <sup>b</sup>	92.5	92.5	12.5	95.0	86.3	84.1	0.6	146,456
Title V Threshold <sup>c</sup>	100	100	100	100	100	100	25	
Title V Required?	No	No	No	No	No	No	No	

a Line 3 includes a natural gas-fired burner. The emissions from Line 3 burner, Boilers 1 & 2, and Lines 1-3 HVACs are estimated based on the natural gas usage limit from Approval Order 19AQ-E056 (listed below). Boiler 3, Line 4 and Flare emissions are shown as PTE assuming continous operation at the capacity. The proposed natural gas usage limit for Line 4 HVACs and the facility-wide limit are presented below.

Approval Order 19AQ-E056 Natural Gas Usage Limit for Lines 1-3:	1,314.28	million cf/yr =	1,340,566	MMBtu/yr
Line 4 Proposed Natural Gas Usage Limit (including Boiler 3 and Line 4 HVACs):	933.21	million cf/yr =	951,876	MMBtu/yr
Boiler 3:	838.21	million cf/yr =	854,976	MMBtu/yr
Line 4 HVACs:	95.00	million cf/yr =	96,900	MMBtu/yr
Facility-wide Natural Gas Usage Limit:	2,247.49	million cf/yr =	2,292,442	MMBtu/yr

<sup>b</sup> Facility-wide SO<sub>2</sub> emissions take the maximum of biogas firing at the boiler or the flare. HVACs are for comfort air conditioning purposes only and emissions from the HVAC systems are included for the facility-wide emissions.

<sup>c</sup> Per 40 CFR 70.2 and 70.3, a Title V Permit is required for any major source which is defined as the potential to emit emissions greater or equal to 100 tpy for any air pollutant subject to regulation, 10 tpy of an individual HAP, or 25 tpy of combined HAPs. Fugitives sources do not need to be considered in determining the potential to emit for the facility since the source is not one of the listed 28 source categories. As the Othello facility is not categorized as a listed source category, fugitive emissions are not required to be included. The EPA definition of "fugitive emissions" is "those emissions which could not reasonable pass through a stack, chimney, vent, or other functionally-equivalent opening" per the February 10, 1999 memorandum *Interpretation of the Definition of Fugitive Emissions in Parts 70 and 71*, from Thomas C. Current, Director Information Transfer and Program Integration Division. All fugitive emissions of HAP must be included when determining major source status. Fugitive emissions in this case would include truck traffic for products/raw materials transportation, which does not emit any HAP.

		1		
Averaging	Project Emission Rate <sup>a</sup>	De Minimis	SQER <sup>b</sup>	Modeling
Period	(lb/	averaging pe	riod)	Required?
Year	57.29	1.0E+00	2.1E+01	Yes
Year	392.05	1.4E+00	2.7E+01	Yes
Year	3.87	2.4E-01	4.8E+00	No
Year	16.96	3.0E+00	6.0E+01	No
24-hr	0.02	1.3E-03	2.6E-02	No
24-hr	4.45	1.1E+01	2.2E+02	De Minimis
24-hr	0.14	1.9E+01	3.7E+02	De Minimis
24-hr	0.09	8.2E-01	1.6E+01	De Minimis
Year	476.31	3.2E+00	6.5E+01	Yes
24-hr	0.05	2.6E+00	5.2E+01	De Minimis
24-hr	0.93	7.4E-03	1.5E-01	Yes
1-hr	3.60	4.6E-01	1.2E+00	Yes
1-hr	0.48	4.6E-01	8.7E-01	No
1-hr	5.08	1.1E+00	4.3E+01	No
	Averaging Period Year Year Year 24-hr 24-hr 24-hr 24-hr 24-hr 24-hr 24-hr 24-hr 24-hr 1-hr 1-hr 1-hr	Project Emission           Averaging Period         Project Emission           Year         Rate <sup>a</sup> Year         57.29           Year         392.05           Year         3.87           Year         16.96           24-hr         0.02           24-hr         0.14           24-hr         0.09           Year         476.31           24-hr         0.93           1-hr         3.60           1-hr         0.48           1-hr         5.08	Project Emission Rate <sup>a</sup> De Minimis b           Period         (lb/averaging period)           Year         57.29         1.0E+00           Year         392.05         1.4E+00           Year         3.87         2.4E-01           Year         16.96         3.0E+00           24-hr         0.02         1.3E-03           24-hr         0.14         1.9E+01           24-hr         0.14         1.9E+01           24-hr         0.09         8.2E-01           Year         476.31         3.2E+00           24-hr         0.93         7.4E-03           1-hr         3.60         4.6E-01           1-hr         5.08         1.1E+00	Project Emission Period         Project Emission Rate <sup>a</sup> De Minimis b         SQER b           Year         57.29         1.0E+00         2.1E+01           Year         392.05         1.4E+00         2.7E+01           Year         387         2.4E-01         4.8E+00           Year         16.96         3.0E+00         6.0E+01           24-hr         0.02         1.3E-03         2.6E-02           24-hr         0.14         1.9E+01         3.7E+02           24-hr         0.09         8.2E-01         1.6E+01           Year         476.31         3.2E+00         6.5E+01           24-hr         0.05         2.6E+00         5.2E+01           24-hr         0.93         7.4E-03         1.5E-01           1-hr         3.60         4.6E-01         8.7E-01           1-hr         0.48         4.6E-01         8.7E-01           1-hr         5.08         1

#### Table C-1b. Updated Line 4 Project TAP Emissions

<sup>a</sup> Project emissions are conservatively determined to be the sum of the dual fuel scenario for the new boiler and the projected biogas emissions for the flare for all TAPs.

<sup>b</sup> De Minimis and SQER are updated to use WAC 173-460-150 (effective 12/31/2019).

#### Table C-2a. Potential Emissions from the New Boiler 3 - Natural Gas Combustion

Maximum Operating Hours		8,760	hr/year		
Maximum Heat Input Capacity <sup>b</sup>		97.6 MMBtu/hr			
Estimated Heat Input	by Natural Gas <sup>a</sup>	854,976	MMBtu/yr		
	Natural Gas	Exhaust Gas	Emission Factor		
	<b>Emission Factor</b>	Emission Factor	а	Emissio	n Rate
Pollutant	(lb/MMscf)	(lb/dry 10 <sup>6</sup> scf)	(lb/MMBtu)	(lb/hr)	(tpy)
PM <sub>10</sub> c	7.6		7.45E-03	0.73	3.19
PM <sub>2.5</sub> c	7.6		7.45E-03	0.73	3.19
SO <sub>2</sub> c	0.6		5.88E-04	0.06	0.25
NO <sub>X</sub> d		4.18	3.64E-02	3.56	15.57
VOC <sup>c</sup>	5.5		5.39E-03	0.53	2.31
CO <sup>c</sup>		4.24	3.69E-02	3.60	15.78
<u>CO₂e</u> e				11,428.76	50,057.97
CO <sub>2</sub> e			116.98	11,416.97	50,006.32
N <sub>2</sub> O <sup>e</sup>			2.20E-04	0.02	0.09
CH <sub>4</sub> e			2.20E-03	0.22	0.94

<sup>a</sup> The natural gas heating value below is used to convert the AP-42 emission factors in lb/MMscf to lb/MMBtu, in accordance with footnotes in Chapter 1.4. The boiler can fire all of the biogas generated and supplement the remaining heat input by natural gas, or fire 100% natural gas.

Natural gas heating value 1,020 Btu/scf

<sup>b</sup> The maximum heat input is based on vendor provided burner heat input.

<sup>c</sup> Emission factors for small boilers (<100 MMBtu/hr) are obtained from Table 1.4.1 and Table 1.4.2, AP-42 Chapter 1.4, Natural Gas Combustion. Here it assumes that these emissions are not affected by the type of gas fired (natural gas or biogas). Note that the annual SO<sub>2</sub> emissions listed in this table only represents natural gas combustion at the estimated annual natural gas usage listed here.

 $^{\rm d}$  Emission factors for NO<sub>x</sub> and CO are obtained from emission limits of 30 ppm and 50 ppm corrected to 3% oxygen, respectively. The emission factors are converted from ppm to lb/MMscf using EPA Method 19 using the equations below. A conversion fuel factor of 8,710 dscf/MMBtu is used to determine the emission factor in lb/MMBtu.

NO<sub>X</sub> EF (lb/MMscf) = NO<sub>X</sub> concentration (ppm) ×  $1.194 \times 10^{-7}$  (lb/scf)/(ppm-NO<sub>X</sub>) ×  $20.9\%/(20.9\%-3\%) \times 10^{6}$ CO EF (lb/MMscf) = CO concentration (ppm) ×  $1.660 \times 10^{-7}$  (lb/scf)/(ppm-SO<sub>2</sub>) × 28.0101 (g/mol SO<sub>2</sub>) / 64.066 (g/mol CO) ×  $20.9\%/(20.9\%-3\%) \times 10^{6}$ 

<sup>e</sup> The emission factors for each GHG are obtained from 40 CFR 98 Subpart C, Tables C-1 and C-2 for natural gas combustion, and converted to values in lb/MMBtu. The GHGs emissions are calculated based on the Global Warming Potentials (GWP) provided in Table A-1 of 40 CFR 98.

CO <sub>2</sub>	1
N <sub>2</sub> O	298
CH <sub>4</sub>	25

#### Table C-2b. Potential Emissions from the New Boiler 3 - Biogas and Natural Gas Combustion

Maximum Hoat Input	Capacity	97.6	MMBtu/hr	
Maximum neat input	Capacity	854,976	MMBtu/yr	
Diagon consumption <sup>a</sup>		0.051	MMscf/hr	
Biogas consumption		325	MMscf/yr	
Estimated Heat Input	by Piogos <sup>a</sup>	32.44	MMBtu/hr	
Estimated near input	Dy Diogas	206,674	MMBtu/yr	
	H <sub>2</sub> S Content	Destruction	Emissio	on Rate
Pollutant	(molar fraction)	Efficiency	(lb/hr)	(tpy)
SO <sub>2</sub> from Biogas b	0.02%	98%	1.78	5.68
H <sub>2</sub> S <sup>b</sup>	0.02%	98%	0.02	0.06
	<b>Biogas Emission</b>	Natural Gas		
	Factor	Emission Factor	Emissio	on Rate
Pollutant	(lb/MMBtu)	(lb/MMBtu)	(lb/hr)	(tpy)
PM <sub>10</sub> c	7.45E-03	7.45E-03	0.73	3.19
PM <sub>2.5</sub> c	7.45E-03	7.45E-03	0.73	3.19
SO <sub>2</sub> from Natural Gas		5.88E-04	0.04	0.19
NO <sub>X</sub> c	0.04	0.04	3.56	15.57
VOC <sup>c</sup>	5.39E-03	5.39E-03	0.53	2.31
CO <sup>c</sup>	0.04	0.04	3.60	15.78
<u>CO₂e</u> d			11,373.20	49,880.95
CO <sub>2</sub> d	114.79	116.98	11,346.18	49,780.80
N <sub>2</sub> O <sup>d</sup>	1.39E-03	2.20E-04	0.06	0.21
CH <sub>4</sub> d	7.05E-03	2.20E-03	0.37	1.44

<sup>a</sup> Biogas consumption rate is from permit No. 19AQ-E056. Here assumes that the new Boiler 3 can fire up to 100% of biogas generated. Hourly biogas consumption is based on McCain's design, which is 850 scfm. Biogas heating value is based on McCain's design information.

Biogas heating value: 636 Btu/scf

 $^{b}$  H<sub>2</sub>S content is based on McCain's design information, consistently with other sites operating a wastewater treatment plant. Based on the sulfothane scrubber quote, the outlet H<sub>2</sub>S concentration will be less than 200 ppm. It assumes that 98% of the H<sub>2</sub>S will be combusted to SO<sub>2</sub>. The following parameters are used to convert the sulfur content from H<sub>2</sub>S to SO<sub>2</sub>:

> gas constant, J/K-mol: 8.314 Standard air temperature, K: 273.15 Standard pressure, Pa: 101325 MW of SO<sub>2</sub>, g/mol: 64 MW of H<sub>2</sub>S, g/mol: 34.1

<sup>c</sup> The same emission factors for natural gas combustion are used here for biogas combustion.

<sup>d</sup> The emission factors for each GHG are obtained from 40 CFR 98 Subpart C, Tables C-1 and C-2 for other biomass gaseous fuels, and converted to values in Ib/MMBtu. The GHGs emissions are calculated based on the Global Warming Potentials (GWP) provided in Table A-1 of 40 CFR 98.

#### Table C-2c. Potential Emissions from the New Boiler 3

		Hourly Emission	Annual
		Rate	Emission Rate
Pollutant		(lb/hr)	(tpy)
PM <sub>10</sub>		0.73	3.19
PM <sub>2.5</sub>		0.73	3.19
SO <sub>2</sub>	а	1.82	5.87
NO <sub>X</sub>		3.56	15.57
VOC		0.53	2.31
СО		3.60	15.78
H <sub>2</sub> S	b	0.02	0.06
HAPs		9.42E-03	0.04
CO <sub>2</sub> e		11,429	50,058

<sup>a</sup> Emissions are the worst of combustion of natural gas only or dual fuel.

<sup>b</sup> H<sub>2</sub>S emissions are from uncombusted biogas.

#### Table C-2d. HAP Emissions from the New Boiler 3

Maximum Operati	ng H	lours	8760	hr/yr					
Estimated Heat In	put	by Natural Gas <sup>a</sup>	854,976	MMBtu/yr					
Estimated Annual	Hea	t Input by Biogas <sup>b</sup>	206,674	MMBtu/yr					
Estimated Hourly	Heat	: Input by Biogas <sup>b</sup>	32	MMBtu/hr					
			<b>Emission Factor</b>	Natural Gas	Emissio	on Rate	Biogas	Dual Fuel Em	nission Rate
Pollutant		HAP?	(lb/MMscf)	(lb/MMBtu)	(lb/hr)	(tpy)	(lb/MMBtu)	(lb/hr)	(tpy)
Benzene	с	Yes	0.0058	5.69E-06	5.55E-04	2.43E-03	9.12E-06	6.66E-04	2.79E-03
Formaldehyde	с	Yes	0.0123	1.21E-05	1.18E-03	5.16E-03	1.93E-05	1.41E-03	5.91E-03
PAH's (including Naphthalene)	с	Yes	0.0004	3.92E-07	3.83E-05	1.68E-04	6.29E-07	4.60E-05	1.92E-04
Naphthalene	с	Yes - included above	0.0003	2.94E-07	2.87E-05	1.26E-04	4.72E-07	3.45E-05	1.44E-04
Acetaldehyde	с	Yes	0.0031	3.04E-06	2.97E-04	1.30E-03	4.87E-06	3.56E-04	1.49E-03
Acrolein	с	Yes	0.0027	2.65E-06	2.58E-04	1.13E-03	4.25E-06	3.10E-04	1.30E-03
Propylene	с	No	0.5300	5.20E-04	0.05	0.22	8.33E-04	0.06	0.25
Toluene	с	Yes	0.0265	2.60E-05	2.54E-03	1.11E-02	4.17E-05	3.04E-03	1.27E-02
Xylenes	с	Yes	0.0197	1.93E-05	1.89E-03	8.26E-03	3.10E-05	2.26E-03	9.46E-03
Ethyl Benzene	с	Yes	0.0069	6.76E-06	6.60E-04	2.89E-03	1.08E-05	7.93E-04	3.31E-03
Hexane	с	Yes	0.0046	4.51E-06	4.40E-04	1.93E-03	7.23E-06	5.28E-04	2.21E-03

<sup>a</sup> The natural gas heating value below is used to convert the AP-42 emission factors in lb/MMscf to lb/MMBtu, in accordance with footnotes in Chapter 1.4. The boiler can fire all of the biogas generated and supplement the remaining heat input by natural gas, or fire 100% natural gas.

> Natural gas heating value 1,020 Btu/scf

<sup>b</sup> Biogas consumption rate is based on McCain's estimates on annual basis. Here assumes that the new alpha boiler can fire up to 100% of biogas generated. Hourly biogas consumption assumes the 30% combustion is contributed by biogas based on vendor info. Biogas heating value is based on McCain's design information.

> Biogas heating value: 636 Btu/scf

<sup>c</sup> Emissions factors for HAPs are taken from the Ventura County Air Pollution Control District AB 2588 Combustion Emission Factors. http://www.aqmd.gov/docs/defaultsource/permitting/toxics-emission-factors-from-combustion-process-.pdf. The emission factors provided are in the unit of lb/MMscf for natural gas external combustion sources in the size of 10-100 MMBtu/hr. The emission factor document does not specify the heating value to convert the factors from lb/MMStt to lb/MMBtu. For biogas it is assumed that the natural gas external combustion factors are representative, even though the heating value of biogas is much lower than that of natural gas. In this case, the lb/MMscf natural gas factors were applied to biogas combustion rate in scfm directly, which is conservative in estimating speciated HAP/TAP emissions from biogas combustion.

#### Table C-3a. Potential Emissions from the Flare - Pilot Gas

Maximum Operating	imum Operating Hours 8,760 hr/year		hr/year	
Propane Usage <sup>a</sup>		8,400	gal/yr	
Estimated Heat Inp	ut <sup>a</sup>	768.60	MMBtu/yr	
	Propane Emission	Propane Emission		
	Factor <sup>b</sup>	Factor <sup>c</sup>	Emissi	on Rate
Pollutant	(lb/1000 gal)	(lb/MMBtu)	(lb/hr)	(tpy)
PM <sub>10</sub>	0.7		6.71E-04	2.94E-03
PM <sub>2.5</sub>	0.7		6.71E-04	2.94E-03
SO <sub>2</sub>	0.054		5.18E-05	2.27E-04
NO <sub>X</sub>	13		1.25E-02	0.05
VOC	1		9.59E-04	4.20E-03
со	7.5		7.19E-03	0.03
<u>CO₂e</u> <sup>c</sup>			12.21	53.48
CO <sub>2</sub> c		138.60	12.16	53.27
N <sub>2</sub> O <sup>c</sup>		1.32E-03	1.16E-04	5.08E-04
CH <sub>4</sub> c		6.61E-03	5.80E-04	2.54E-03

Propane usage is estimated based on limited plant operations data from November 2021 to now, and adding a safety factor for conservatism. Propane heating value from AP-42 Chapter 1.5 is used to determine the heat input. Propane heating value 91.5 MMBtu/1000 gal

<sup>b</sup> Emission factors for propane combustion are obtained from Table 1.5-1, AP-42 Chapter 1.5. According to an EPA study (https://www3.epa.gov/ttnchie1/conference/ei12/area/haneke.pdf), a national average sulfur content in LPG is 0.54 gr/1000 gal, which is used to determine the SO2 emission factor.

<sup>c</sup> The emission factors for each GHG are obtained from 40 CFR 98 Subpart C, Tables C-1 and C-2 for propane combustion, and converted to values in Ib/MMBtu. The GHGs emissions are calculated based on the Global Warming Potentials (GWP) provided in Table A-1 of 40 CFR 98.

-		
	CO <sub>2</sub>	1
	N <sub>2</sub> O	298
	CH₄	25

#### Table C-3b. Potential Emissions from the Flare - Biogas Combustion

Biogas consumption <sup>a</sup>		5.10E-02	MMscf/hr		
		325	MMscf/yr		
Estimated Heat	Inpu	t by Biogas <sup>a</sup>	206,674	MMBtu/yr	
		H <sub>2</sub> S Content	Destruction	Emiss	ion Rate
Pollutant		(molar fraction)	Efficiency	(lb/hr)	(tpy)
SO <sub>2</sub>	b	0.02%	98%	1.78	5.68
H₂S	b	0.02%	98%	0.02	0.06
				Emiss	ion Rate
Pollutant		Emissior	n Factor	(lb/hr)	(tpy)
PM <sub>10</sub>	с	1.48E-02	lb/MMBtu	0.48	1.53
PM <sub>2.5</sub>	с	1.48E-02	lb/MMBtu	0.48	1.53
NO <sub>X</sub>	c	0.039	lb/MMBtu	1.25	3.99
со	с	0.045	lb/MMBtu	1.48	4.70
VOC	d	5.39E-03	lb/MMBtu	0.17	0.56
<u>CO₂e</u>	e			3,742.63	11,923.51
CO <sub>2</sub>	e	114.79	lb/MMBtu	3,723.48	11,862.51
N <sub>2</sub> O	e	1.39E-03	lb/MMBtu	0.05	0.14
CH <sub>4</sub>	e	7.05E-03	lb/MMBtu	0.23	0.73

Biogas consumption rate is based on permit No. 19AQ-E056. The maximum hourly biogas generation rate is expected to be 850 scfm. Biogas heating value is based on McCain's design information.

Biogas heating value: 636 Btu/scf

 $^{\rm b}$  H<sub>2</sub>S content is based on McCain's design information, consistently with other sites operating a wastewater treatment plant. The outlet H<sub>2</sub>S concentration is based on permit limit of 200 ppm. It assumes that 98% of the H<sub>2</sub>S will be combusted to SO<sub>2</sub>. The following parameters are used to convert the sulfur content from H<sub>2</sub>S to SO<sub>2</sub>:

gas constant, J/K-mol: 8.314 Standard air temperature, K: 273.15

Standard pressure, Pa: 101325

MW of SO2, g/mol: 64

MW of H<sub>2</sub>S, g/mol: 34.1

<sup>c</sup> The PM<sub>10</sub>, PM<sub>2.5</sub>, NO<sub>x</sub> and CO emission factors are obtained from AP-42 Chapter 2.4 (Draft version, October 2008). The factors for landfill flares are assumed to be representative of biogas combustion, because the landfill gas' heating value is close to biogas' heating value (about half of natural gas' heating value). Additionally, these factors are on the per scf CH<sub>4</sub> burned, which should provide a representative estimate for biogas combustion using biogas' heating value. The lb/million dscf CH<sub>4</sub> factor is converted to lb/MMBtu using CH<sub>4</sub>'s HHV of 1011 Btu/scf.

<sup>d</sup> The biogas stream contains mainly methane and other inert gases, which does contain small amount of VOC. The VOCs are usually destroyed during combustion. The same VOC emission factor for natural gas combustion is conservatively used here for biogas combustion (AP-42 Chapter 1.4 factors in lb/MMscf converted to lb/MMBtu using the default natural gas heating value of 1,020 Btu/scf).

<sup>e</sup> The emission factors for each GHG are obtained from 40 CFR 98 Subpart C, Tables C-1 and C-2 for other biomass gaseous fuels, and converted to values in Ib/MMBtu. The GHGs emissions are calculated based on the Global Warming Potentials (GWP) provided in Table A-1 of 40 CFR 98.

#### Table C-3c. Potential Emissions from the Flare

	Hourly Emission Rate	Annual Emission Rate
Pollutant	(lb/hr)	(tpy)
PM <sub>10</sub>	0.48	1.54
PM <sub>2.5</sub>	0.48	1.54
SO <sub>2</sub>	<sup>a</sup> 1.78	5.68
NO <sub>X</sub>	1.26	4.04
VOC	0.18	0.56
CO	1.48	4.73
H <sub>2</sub> S	<sup>b</sup> 0.02	0.06
HAPs	0.15	0.48
CO <sub>2</sub> e	3,755	11,977

<sup>a</sup> Emissions are the sum from pilot gas combustion and biogas combustion.

 $^{\rm b}~{\rm H_2S}$  emissions are from uncombusted biogas.

#### Table C-3d. HAP Emissions - Flare

Maximum Operating Hours		8760	hr/yr				
Estimated Heat Inp	out	t by Propane <sup>a</sup>	769	MMBtu/yr			
Estimated Heat Inp	out	t by Biogas <sup>b</sup>	206,674	MMBtu/yr			
Estimated Hourly H	lea	at Input by Biogas <sup>b</sup>	32	MMBtu/hr			
Pollutant		HAP?	Emission Factor (lb/MMscf)	Propane (lb/MMBtu)	Biogas (lb/MMBtu)	Total Emis (lb/hr)	sion Rate (tpy)
Benzene	с	Yes	0.159	6.33E-05	2.50E-04	8.11E-03	0.03
Formaldehyde	с	Yes	1.169	4.65E-04	1.84E-03	0.06	0.19
PAH's (including , Naphthalene)	с	Yes	0.014	5.57E-06	2.20E-05	7.14E-04	2.28E-03
Naphthalene	c	Yes - included above	0.011	4.38E-06	1.73E-05	5.61E-04	1.79E-03
Acetaldehyde	с	Yes	0.043	1.71E-05	6.76E-05	2.19E-03	6.99E-03
Acrolein	с	Yes	0.010	3.98E-06	1.57E-05	5.10E-04	1.63E-03
Propylene	с	No	2.440	9.71E-04	3.84E-03	0.12	0.40
Toluene	с	Yes	0.058	2.31E-05	9.12E-05	2.96E-03	9.43E-03
Xylenes	с	Yes	0.029	1.15E-05	4.56E-05	1.48E-03	4.72E-03
Ethyl Benzene	с	Yes	1.444	5.74E-04	2.27E-03	0.07	0.23
Hexane	с	Yes	0.029	1.15E-05	4.56E-05	1.48E-03	4.72E-03

Propane usage is estimated based on a similar plant's actual usage, and scaled to the maximum amount usage for PTE purposes. Propane based on a similar plant's actual usage, and scaled to the maximum amount usage for PTE purposes.

heating value from AP-42 Chapter 1.5 is used to determine the heat input.

Propane heating value 91.5 MMBtu/1000 gal

Propane liquid to gas 36.4 cf/gal

<sup>b</sup> Biogas consumption rate is based on McCain's estimates on annual basis. Here assumes that the new alpha boiler can fire up to 100% of biogas generated. Hourly biogas consumption assumes the heat input capacity is reached by biogas combustion. Biogas heating value is based on Biogas heating value:
 636 Btu/scf

<sup>c</sup> Emissions factors for HAPs are taken from the Ventura County Air Pollution Control District AB 2588 Combustion Emission Factors. http://www.aqmd.gov/docs/default-source/permitting/toxics-emission-factors-from-combustion-process-.pdf. The emission factors provided are in the unit of Ib/MMscf for natural gas external combustion sources in the size of 10-100 MMBtu/hr. The emission factor document does not specify the heating value to convert the factors from Ib/MMscf to Ib/MMBtu. For biogas it is assumed that the natural gas external combustion factors are representative, even though the heating value of biogas is much lower than that of natural gas. In this case, the Ib/MMscf natural gas factors were applied to biogas combustion rate in scfm directly, which is conservative in estimating speciated HAP/TAP emissions from biogas combustion.

#### Table C-4a. Potential Emissions from Line 4

Operating Hours	8,760	hr/year				
Line 4 Capacity	59,270	lb finished pro	oduct/hr			
	Emission Factors (lb/finished ton)		Emission Rate (lb/hr)		Emission Rate (tpy)	
Stage	PM <sub>10</sub> / PM <sub>2.5</sub>	VOC	PM <sub>10</sub> / PM <sub>2.5</sub>	VOC	PM <sub>10</sub> / PM <sub>2.5</sub>	VOC
Line 4 Dryer and Two-Stage a Fryer - Wet ESP	0.065	0.413	1.92	12.23	8.41	53.59
	1.92	12.23	8.41	53.59		

<sup>a</sup> Line 4 dryer/fryer will be steam heated. Emissions from Line 4 dryer/fryer will be controlled by a new wet ESP. The PM emissions are based on vendor guarantee. VOC emissions from the wet ESP are based on recent McCain's Burley, ID plant source test results for a production line with a dryer and a two-stage fryer, accouting for a safety factor of 20%. The emission factor from the test report in lb/hr is converted to a lb/finished ton value using the production rate during the test. It is conservatively assumed all THC is VOC.

#### Table C-5a. Potential Emissions from the Existing Boilers 1, 2 and Lines 1-3 HVACs - Natural Gas

Natural Gas H	leating	Value <sup>a</sup>	1,020	Btu/scf		
Maximum He	at Inpu	t Capacity <sup>b</sup>	210.40	MMBtu/hr		
Maximum An	nual He	at Input <sup>b</sup>	1,319,541.6	MMBtu/yr		
		Natural Gas Emission Factor	Emission Factor	Emiss	ion Rate	
Pollutant		(lb/MMscf)	(lb/MMBtu)	(lb/hr)	(tpy)	
PM <sub>10</sub>	с	7.6	7.45E-03	1.57	4.92	
PM <sub>2.5</sub>	с	7.6	7.45E-03	1.57	4.92	
SO <sub>2</sub>	с	0.6	5.88E-04	0.12	0.39	
NO <sub>X</sub>	с	100	0.10	20.63	64.68	
VOC	c	5.5	5.39E-03	1.13	3.56	
СО	с	84	8.24E-02	17.33	54.33	
<u>CO<sub>2</sub>e</u>	d			24,636.82	77,257.81	
CO <sub>2</sub>	e		116.98	24,611.40	77,178.10	
N <sub>2</sub> O	e		2.20E-04	0.05	0.15	
CH <sub>4</sub>	e		2.20E-03	0.46	1.45	

<sup>a</sup> The natural gas heating value uses a typical heating value from AP-42.

<sup>b</sup> The maximum heat input capacity is based on vendor provided emission data at 100% firing rate for the two boilers, and as-built specifications for HVACs located at Lines 1-3. The maximum annual heat input is based on the natural gas usage limit from Approval Order 19AQ-E056, minus the maximum usage from Line 3 burner.

<sup>c</sup> Emission factors for small boilers (<100 MMBtu/hr) are obtained from Table 1.4.1 and Table 1.4.2, AP-42 Chapter 1.4, Natural Gas Combustion.

<sup>d</sup> The GHGs emissions are calculated based on the Global Warming Potentials (GWP) provided in Table A-1 of 40 CFR 98.

CO <sub>2</sub>	1
N <sub>2</sub> O	298
CH <sub>4</sub>	25

<sup>e</sup> The emission factors are obtained from 40 CFR 98 Subpart C, Tables C-1 and C-2, and converted to values in Ib/MMBtu.

#### Table C-5b. HAP Emissions - Boilers 1, 2 and Lines 1-3 HVACs

Estimated Heat Input by Natural Gas "		1,319,542	MMBtu/yr		
		Emission			
		Factor <sup>®</sup>	Natural Gas	Emissio	on Rate
Pollutant	HAP?	(lb/MMscf)	(lb/MMBtu)	(lb/hr)	(tpy)
Benzene	Yes	0.0058	5.69E-06	1.20E-03	3.75E-03
Formaldehyde	Yes	0.0123	1.21E-05	2.54E-03	7.96E-03
PAH's (including Naphthalene)	Yes	0.0004	3.92E-07	8.25E-05	2.59E-04
Naphthalene	Yes - included above	0.0003	2.94E-07	6.19E-05	1.94E-04
Acetaldehyde	Yes	0.0031	3.04E-06	6.39E-04	2.01E-03
Acrolein	Yes	0.0027	2.65E-06	5.57E-04	1.75E-03
Propylene	No	0.5300	5.20E-04	0.11	0.34
Toluene	Yes	0.0265	2.60E-05	5.47E-03	0.02
Xylenes	Yes	0.0197	1.93E-05	4.06E-03	1.27E-02
Ethyl Benzene	Yes	0.0069	6.76E-06	1.42E-03	4.46E-03
Hexane	Yes	0.0046	4.51E-06	9.49E-04	2.98E-03
TOTAL HAPs				0.02	0.05

<sup>a</sup> The natural gas heating value below is used to convert the AP-42 emission factors in lb/MMscf to lb/MMBtu, in accordance with footnotes in Chapter 1.4. The boiler can fire all of the biogas generated and supplement the remaining heat input by natural gas, or fire 100% natural gas.

Natural gas heating value 1,020 Btu/scf

<sup>b</sup> Emissions factors for HAPs are taken from the Ventura County Air Pollution Control District AB 2588 Combustion Emission Factors. http://www.aqmd.gov/docs/default-source/permitting/toxics-emission-factors-from-combustion-process-.pdf. The emission factors provided are in the unit of Ib/MMscf for natural gas external combustion sources in the size of 10-100 MMBtu/hr. The emission factor document does not specify the heating value to convert the factors from Ib/MMscf to Ib/MMBtu. For biogas it is assumed that the natural gas external combustion factors are representative, even though the heating value of biogas is much lower than that of natural gas. In this case, the Ib/MMscf natural gas factors were applied to biogas combustion rate in scfm directly, which is conservative in estimating speciated HAP/TAP emissions from biogas combustion.

#### Table C-6a. Potential Emissions from Line 1

Operating Hours	8,760	hr/year				
Line 1 Capacity	39,000	lb finished pr	oduct/hr			
Emission Factors (lb/finished ton)		Emission Rate (lb/hr)		Emission Rate (tpy)		
Stage	PM <sub>10</sub> / PM <sub>2.</sub>	, VOC	PM <sub>10</sub> / PM <sub>2.5</sub>	VOC	PM <sub>10</sub> / PM <sub>2.5</sub>	VOC
Line 1 Dryer	0.25		4.88		21.35	
Line 1 Fryer Stage A - Batter	0.107	0.092	2.08	1.80	9.12	7.88
Line 1 Fryer Stage B - Batter	0.0564	0.092	1.10	1.80	4.82	7.88
Conventional	0.1087	0.092	2.12	1.80	9.29	7.88
	т	DTAL Line 1 <sup>d</sup>	8.06	3.60	35.29	15.76

<sup>a</sup> Line 1 dryer is steam heated. The PM emissions are based on Othello's dryer emission factor.

<sup>b</sup> Line 1 fryer stage A is for battered products only, and is controlled by the existing Wet ESP. PM emission factor is based on Wet ESP permit limit of 0.0262 gr/dscf per NOC No. DE 98AQ-E121, but scaled to a lb/finished ton factor using 2011 test result. VOC emissions are based on Othello's emission factor for fryers (test data applying 20% safety factor).

<sup>c</sup> Line 1 fryer stage B is for battered products and conventional products, and is controlled by the existing air washer. PM emission factor is based on source test based on air washer outlet for the corresponding product type (batter or conventional), accounting for 20% safety factor. VOC emissions are based on Othello's emission factor for fryers.

<sup>d</sup> Line 1 total emissions include dryer and fryer emissions. Fryer emissions are based on the batter products emissions for conservatism, because emissions are higher for manufacturing batter products than conventional products.

#### Table C-6b. Potential Emissions from Line 2

Operating Hours		8,760	hr/year				
Line 2 Capacity		39,000	lb finished pro	oduct/hr			
		Emission Factors (lb/finished ton)		Emission Rate (lb/hr)		Emission Rate (tpy)	
Stage	F	PM <sub>10</sub> / PM <sub>2.</sub>	5 VOC	PM <sub>10</sub> / PM <sub>2.5</sub>	VOC	PM <sub>10</sub> / PM <sub>2.5</sub>	VOC
Line 2 Dryer	а	0.25		4.88		21.35	
Line 2 Fryer - Conventional	b	0.1087	0.092	2.12	1.80	9.29	7.88
			TOTAL Line 2	7.00	1.80	30.64	7.88

<sup>a</sup> Line 2 dryer is steam heated. The PM emissions are based on Othello's dryer emission factor.

<sup>b</sup> Line 2 fryer is only for conventional products, and is controlled by the existing air washer. PM emission factor is based on source test based on air washer outlet for the corresponding product. VOC emissions are based on Othello's emission factor for fryers.

#### Table C-7a. Potential Emissions from the Line 3 Dryer

Operating Hour	rs		8,760	hr/year	
Line 3 Capacity			10,000	lb finished product/hr	
Natural Gas He	ating \	√alue ª	1,020	Btu/scf	
Maximum Heat	Input	Capacity <sup>b</sup>	2.40	MMBtu/hr	
		Natural Gas	Exhaust Gas		
		Emission	Emission		
		Factor	Factor	Emissio	n Rate
Pollutant		(lb/MMscf)	(lb/MMBtu)	(lb/hr)	(tpy)
SO <sub>2</sub>	с	0.6	5.88E-04	1.41E-03	6.18E-03
NO <sub>X</sub>	с	153	0.15	0.36	1.58
VOC	с	5.5	0.01	1.29E-02	0.06
CO	с	373	0.37	0.88	3.84
<u>CO₂e</u>	d			281.04	1,230.93
CO <sub>2</sub>	d		116.98	280.75	1,229.66
N <sub>2</sub> O	d		2.20E-04	5.29E-04	2.32E-03
CH <sub>4</sub>	d		2.20E-03	5.29E-03	0.02
PM <sub>10</sub> / PM <sub>2.5</sub>	e	0.25	lb/ton finished product	1.25	5.48

<sup>a</sup> The natural gas heating value below is used to convert the AP-42 emission factors in lb/MMscf to lb/MMBtu, in accordance with footnotes in Chapter 1.4.

<sup>b</sup> Line 3 dryer is a direct-fired dryer. The burner was retrofitted in 2011 with two 1.2 MMBtu/hr burners.
<sup>c</sup> Emission factors from natural gas combustion are obtained from Table 1.4.1 and Table 1.4.2, AP-42 Chapter 1.4, Natural Gas Combustion. NO<sub>X</sub> and CO emission factors are based on April 1994 Ore-Ida source test for Ontario, OR facility, which are the best available source of factors from a direct-fired dryer using natural gas.

<sup>d</sup> The emission factors for each GHG are obtained from 40 CFR 98 Subpart C, Tables C-1 and C-2 for natural gas combustion, and converted to values in lb/MMBtu. The GHGs emissions are calculated based on the Global Warming Potentials (GWP) provided in Table A-1 of 40 CFR 98.

CO <sub>2</sub>	1
N <sub>2</sub> O	298
CH <sub>4</sub>	25

<sup>e</sup> PM emissions are determined based on Othello's dryer emission factor.

#### Table C-7b. Potential Emissions from Line 3 Fryer

Operating Hours	8,760	hr/year				
Line 3 Capacity	10,000	lb finished produ	ct/hr			
	Emission Factors (lb/finished ton)		Emission Rate (lb/hr)		Emission Rate (tpy)	
Stage	PM <sub>10</sub> / PM <sub>2.5</sub>	VOC	PM <sub>10</sub> / PM <sub>2.5</sub>	VOC	PM <sub>10</sub> / PM <sub>2.5</sub>	VOC
Line 3 Fryer - Co- a product	0.107	0.092	0.53	0.46	2.34	2.02

<sup>a</sup> Line 3 fryer is only for co-product only, and is controlled by the existing wet ESP. PM emission factor is based on Wet ESP permit limit of 0.0262 gr/dscf per NOC No. DE 98AQ-E121, but scaled to a lb/finished ton factor using 2011 test result. VOC emissions are based on Othello's emission factor for fryers.

#### Table C-7c. Potential Emissions from Line 3

	Emission Rate	Annual Emission Rate
Pollutant	(lb/hr)	(tpy)
PM <sub>10</sub>	1.78	7.81
PM <sub>2.5</sub>	1.78	7.81
SO <sub>2</sub>	1.41E-03	6.18E-03
NO <sub>X</sub>	0.36	1.58
VOC	0.47	2.08
CO	0.88	3.84
HAPs	1.93E-04	8.45E-04
CO <sub>2</sub> e	281	1,231

#### Table C-7d. HAP Emissions - Line 3

Maximum Operating Hours		8760	hr/yr		
Estimated Heat Input	t by Natural Gas <sup>a</sup>	21,024	MMBtu/yr		
		Factor <sup>b</sup>	Natural Gas	Emission	Rate
Pollutant	HAP?	(lb/MMscf)	(lb/MMBtu)	(lb/hr)	(tpy)
Benzene	Yes	0.0058	5.69E-06	1.36E-05	5.98E-05
Formaldehyde	Yes	0.0123	1.21E-05	2.89E-05	1.27E-04
PAH's (including Naphthalene)	Yes	0.0004	3.92E-07	9.41E-07	4.12E-06
Naphthalene	Yes - included above	0.0003	2.94E-07	7.06E-07	3.09E-06
Acetaldehyde	Yes	0.0031	3.04E-06	7.29E-06	3.19E-05
Acrolein	Yes	0.0027	2.65E-06	6.35E-06	2.78E-05
Propylene	No	0.5300	5.20E-04	1.25E-03	5.46E-03
Toluene	Yes	0.0265	2.60E-05	6.24E-05	2.73E-04
Xylenes	Yes	0.0197	1.93E-05	4.64E-05	2.03E-04
Ethyl Benzene	Yes	0.0069	6.76E-06	1.62E-05	7.11E-05
Hexane	Yes	0.0046	4.51E-06	1.08E-05	4.74E-05

<sup>a</sup> The natural gas heating value below is used to convert the AP-42 emission factors in lb/MMscf to lb/MMBtu, in accordance with footnotes in Chapter 1.4. The boiler can fire all of the biogas generated and supplement the remaining heat input by Natural gas heating value 1,020 Btu/scf

<sup>b</sup> Emissions factors for HAPs are taken from the Ventura County Air Pollution Control District AB 2588 Combustion Emission Factors. http://www.aqmd.gov/docs/default-source/permitting/toxics-emission-factors-from-combustion-process-.pdf

#### Table C-8a. Potential Emissions from Line 4 HVAC Systems

Natural Gas H	leating	Value <sup>a</sup>	1,020	Btu/scf	Ī		
Line 4 HVAC	Units H	eat Input Capacity <sup>b</sup>	65.35	MMBtu/hr			
Annual Heat	Input <sup>b</sup>		96,900	MMBtu/yr			
		Natural Gas	Emission				
		Emission Factor	Factor	on Rate			
Pollutant		(lb/MMscf)	(lb/MMBtu)	(lb/hr)	(tpy)		
PM <sub>10</sub>	c	7.6	7.45E-03	0.49	0.36		
PM <sub>2.5</sub>	с	7.6	7.45E-03	0.49	0.36		
SO <sub>2</sub>	с	0.6	5.88E-04	0.04	0.03		
NO <sub>X</sub>	с	100	0.10	6.41	4.75		
VOC	с	5.5	5.39E-03	0.35	0.26		
CO	с	84	8.24E-02	5.38	3.99		
<u>CO<sub>2</sub>e</u>	d			7,652.84	5,673.40		
CO <sub>2</sub>	e		116.98	7,644.94	5,667.54		
N <sub>2</sub> O	e		2.20E-04	1.44E-02	1.07E-02		
CH <sub>4</sub>	e		2.20E-03	0.14	0.11		

<sup>a</sup> The natural gas heating value uses a typical heating value from AP-42.

<sup>b</sup> The maximum heat input is the sum of all Line 4 HVAC systems. Annual heat input is based on the proposed natural gas usage. <sup>c</sup> Emission factors for small boilers (<100 MMBtu/hr) are obtained from Table 1.4.1 and Table 1.4.2, AP-42 Chapter 1.4, Natural Gas

Combustion.

<sup>d</sup> The GHGs emissions are calculated based on the Global Warming Potentials (GWP) provided in Table A-1 of 40 CFR 98.

CO <sub>2</sub>	1
N <sub>2</sub> O	298
CH <sub>4</sub>	25

<sup>e</sup> The emission factors are obtained from 40 CFR 98 Subpart C, Tables C-1 and C-2, and converted to values in lb/MMBtu.

#### Table C-8b. TAP and HAP Emissions - HVAC Systems

Estimated Heat Input by Natural Gas <sup>a</sup>		96,900	MMBtu/yr		
		Emission			
		Factor <sup>b</sup>	Natural Gas	Emissio	on Rate
Pollutant	HAP?	(lb/MMscf)	(lb/MMBtu)	(lb/hr)	(tpy)
Benzene	Yes	0.0058	5.69E-06	3.72E-04	2.76E-04
Formaldehyde	Yes	0.0123	1.21E-05	7.88E-04	5.84E-04
PAH's (including Naphthalene)	Yes	0.0004	3.92E-07	2.56E-05	1.90E-05
Naphthalene	Yes - included above	0.0003	2.94E-07	1.92E-05	1.43E-05
Acetaldehyde	Yes	0.0031	3.04E-06	1.99E-04	1.47E-04
Acrolein	Yes	0.0027	2.65E-06	1.73E-04	1.28E-04
Propylene	No	0.5300	5.20E-04	0.03	0.03
Toluene	Yes	0.0265	2.60E-05	1.70E-03	1.26E-03
Xylenes	Yes	0.0197	1.93E-05	1.26E-03	9.36E-04
Ethyl Benzene	Yes	0.0069	6.76E-06	4.42E-04	3.28E-04
Hexane	Yes	0.0046	4.51E-06	2.95E-04	2.19E-04
	TOTAL H	IAPs		5.25E-03	3.90E-03

<sup>a</sup> The natural gas heating value below is used to convert the AP-42 emission factors in lb/MMscf to lb/MMBtu, in accordance with footnotes in Chapter 1.4. The boiler can fire all of the biogas generated and supplement the remaining heat input by natural gas, or Natural gas heating value 1,020 Btu/scf

<sup>b</sup> Emissions factors for HAPs are taken from the Ventura County Air Pollution Control District AB 2588 Combustion Emission Factors. http://www.aqmd.gov/docs/default-source/permitting/toxics-emission-factors-from-combustion-process-.pdf

Table C-9a. Emission Summary For Generat	or 1					
Fuel:	Diesel		Generator M	lanufacturer	: Cummins Onan	
Maximum Hours of Operation (hr/yr):	500		Generator M	lodel:	300DFCB	
Maximum Engine Rating (hp):	465		Engine Manu	ufacturer:	Cummins	
Estimated Fuel Use (gal/hr) <sup>a</sup> :	23.8 Engine Mor			el:	NTA855-G2	
Pollutant	Emissions (lb/hr)	Emissions (tpy)	Emission Factor	Emission Factor Units	Emission Factor Source <sup>b</sup>	Notes
<u>Criteria:</u>						
Particulate Matter (PM)	1.02	0.26	2.20E-03	lb/hp-hr	AP-42 Table 3.3-1	
Particulate Matter <10 microns (PM <sub>10</sub> )	1.02	0.26	2.20E-03	lb/hp-hr	AP-42 Table 3.3-1	Assumed equal to PM.
Particulate Matter < 2.5 microns ( $PM_{2.5}$ )	1.02	0.26	2.20E-03	lb/hp-hr	AP-42 Table 3.3-1	Assumed equal to PM.
Sulfur Dioxide (SO <sub>2</sub> )	0.95	0.24	2.05E-03	lb/hp-hr	AP-42 Table 3.3-1	
Carbon Monoxide (CO)	3.11	0.78	6.68E-03	lb/hp-hr	AP-42 Table 3.3-1	
Nitrogen Oxides (NO <sub>x</sub> )	14.42	3.60	0.031	lb/hp-hr	AP-42 Table 3.3-1	Assumed to be uncontrolled.
Volatile Organic Compounds (VOC)	1.17	0.29	2.51E-03	lb/hp-hr	AP-42 Table 3.3-1	Assume all Organic Compounds are VOC.
<u>GHG:</u>						
Carbon Dioxide (CO <sub>2</sub> )		132.68	73.96	kg/MMBtu	40 CFR 98, Table C-1	
Methane (CH <sub>4</sub> )		0.01	0.003	kg/MMBtu	40 CFR 98, Table C-2	
Nitrous Oxide (N <sub>2</sub> O)		0.00	0.0006	kg/MMBtu	40 CFR 98, Table C-2	
Total Carbon Dioxide Equivalent (CO <sub>2</sub> e) <sup>a,c</sup>		133.14				

<sup>a</sup> Esimated fuel use is converted based on the average brake-specific fuel consumption of 7,000 Btu/hp-hr and the diesel fuel heating value per AP-42 (Btu/gal) of 137000.

<sup>b</sup> promulgation.

<sup>c</sup> The Global Warming Potential for  $CO_2$  is 1,  $CH_4$  is 25 and  $N_2O$  is 298 per 40 CFR 98 Table A-1.

Fuel:	Diesel		Generator M	lanufacturer	: Caterpillar	
Maximum Hours of Operation (hr/yr):	500		<b>Generator</b> M	lodel:	C9	
Maximum Engine Rating (kW):	358					
Maximum Engine Rating (hp):	480					
Maximum Fuel Use (gal/hr):	22.4					
Maximum Fuel Use (gal/yr):	11,200					
Pollutant	Emissions (lb/hr)	Emissions (tpy)	Emission Factor	Emission Factor Units	Emission Factor Source <sup>b</sup>	Notes
<u>Criteria:</u>						
Particulate Matter (PM)	0.16	0.04	0.20	g/kW-hr	NSPS IIII	Tier III limit for PM
Particulate Matter <10 microns ( $PM_{10}$ )	0.25	0.06	NA	lb/hr	Filterable PM +	Condensable PM is assumed to be the
Particulate Matter < 2.5 microns ( $PM_{2.5}$ )	0.25	0.06	NA	lb/hr	Condensable PM	same as HC
Sulfur Dioxide (SO <sub>2</sub> )	0.98	0.25	2.05E-03	lb/hp-hr	AP-42 Table 3.3-1	
Carbon Monoxide (CO)	2.76	0.69	3.50	g/kW-hr	NSPS IIII	Tier III limit for CO
Nitrogen Oxides (NO <sub>X</sub> )	3.16	0.79	4.00	g/kW-hr	NSPS IIII	Tier III limit for NOX + HC
Volatile Organic Compounds (VOC)	0.09	0.02	0.09	lb/hr	Engine Emissions Data	Assume all hydrocarbons are VOC; highest of all five load points
<u>GHG:</u>						
Carbon Dioxide (CO <sub>2</sub> )		125.09	73.96	kg/MMBtu	40 CFR 98, Table C-1	
Methane (CH <sub>4</sub> )		0.01	0.003	kg/MMBtu	40 CFR 98, Table C-2	
Nitrous Oxide (N <sub>2</sub> O)		0.00	0.0006	kg/MMBtu	40 CFR 98, Table C-2	
Total Carbon Dioxide Equivalent (CO <sub>2</sub> e)		125.52				

<sup>a</sup> Diesel fuel heating value per AP-42 (Btu/gal) 137,000

- .. . .. . . . .

<sup>b</sup> Emissions factors were obtained from AP-42, Section 3.3, 40 CFR 89 Subpart B, and 40 CFR 98 Subpart C, where manufacturer's data is not available.

<sup>c</sup> The Global Warming Potential for CO<sub>2</sub> is 1, CH<sub>4</sub> is 25 and N<sub>2</sub>O is 298 per 40 CFR 98 Table A-1.

- -

#### Table C-9c. Diesel Internal Combustion Engine HAP Emissions - For Both Generators

			Diesel Fired		
			Industrial	Emissions	HAP Emissions <sup>2</sup>
Pollutant	CAS		Engines <sup>1</sup>		
	Number	HAP?	(lb/MMBtu)	(lb/hr)	(tpy)
Benzene	71-43-2	Yes	9.33E-04	5.90E-03	1.48E-03
Toluene	108-88-3	Yes	4.09E-04	2.59E-03	6.47E-04
Xylenes	1330-20-7	Yes	2.85E-04	1.80E-03	4.51E-04
1,3-Butadiene	106-99-0	Yes	3.91E-05	2.47E-04	6.18E-05
Formaldehyde	50-00-0	Yes	1.18E-03	7.46E-03	1.87E-03
Acetaldehyde	75-07-0	Yes	7.67E-04	4.85E-03	1.21E-03
Acrolein	107-02-8	Yes	9.25E-05	5.85E-04	1.46E-04
Total Polycyclic Aromatic Hydrocarbons (PAH)		Yes	1.68E-04	1.06E-03	2.66E-04
Total HAP				0.02	6.12E-03

<sup>a</sup> Emission factors are from Table 3.3-2-4 AP-42.

<sup>b</sup> List of HAP established by 42 U.S.C. 7412(b)(1).





# AirHeat Burners

AH-MA Series Version 2.20

#### **Main Specifications**

Parameter	Description
Input (Btu/hr./ft.)	1,200,000 maximum
Combustion Airstream	0.2" to 1.4"w.c.
Pressure Drop/Velocity	
Ignition	Direct spark ignition (6000VAC).
Pilot	Interruptible pilot for natural gas, propane or butane.
Integral Pilot Capacities	20,000 Btu/hr.
Burner Bodies	Standard Aluminum
	Low Pressure Aluminum*
	Standard Cast Iron
	Corrosion Resistant, EN Plated Cast Iron
	Low Pressure Cast Iron*
Burner Section Sizes	<ul> <li>150mm (6") straight section</li> </ul>
	<ul> <li>300mm (12") straight section</li> </ul>
	<ul> <li>300mm (12") straight section with back inlet</li> </ul>
~	<ul> <li>300mm (12") straight section with pilot</li> </ul>
	<ul> <li>150mm (6") by 300mm (12") tee section</li> </ul>
	<ul> <li>150mm (6") by 300mm (12") tee section with pilot</li> </ul>
	<ul> <li>300mm (12") by 300mm (12") cross section</li> </ul>
Pipe Threads	N.P.T. or B.S.P.
Maximum Upstream Air Temp.	450°F (232°C)
Maximum Downstream Air Temp.	850°F (454°C)
Maximum Temperature Rise	750°F (400°C)
Minimum Inlet Air Oxygen (O2)	8%
Flame Detection**	Flame rod or scanner.
Fuels	Natural gas, propane or butane.

\* For use with Natural Gas only.

- Burners over 5 lineal feet include flame supervision at the far end. If pilot ignition is being used, two flame supervision units are required; one for the pilot and one for the far end. If using direct spark on the main flame, only flame supervision at the far end is required providing ignition can be accomplished within 15 seconds. (Reference NFPA Requirement 5-9.2.2)
- Eclipse reserves the right to change the construction and/or configurations of our products at any time without being obliged to adjust earlier supplies accordingly.
- All information is based on laboratory testing. Different chamber size and air flow conditions may affect the data.
- All information is based on standard conditions (70°F at sea level). Contact Eclipse for performance data above ambient temperature.
- All inputs based on gross caloric values.





**Operating Range & Duct Pressure Measurement** 

**Inlet Air Temperature Correction** 

Air Press. Drop @ Air Temp. = Air Press. Drop from "Oper. Range" Chart x Correction Factor										
Air Inlet Temp. (°F)	0	30	70	150	200	250	300	350	400	450
Correction Factor	0.87	0.92	1.00	1.15	1.25	1.34	1.43	1.53	1.62	1.72

#### **Air Velocity Calculation**

Air Velocity (fpm) = 1096.2

4

#### **Differential Pressure Measurement & Burner Gas Pressure Drops**



\*\* 2.4mm gas ports

#### **Flame Lengths**











Eclipse AH-MA AirHeat Burners v2.20, Data Sheet 160, 11/7/04



Eclipse Combustion
www.eclipsenet.com

\*

- '