

APPENDIX A
COLD-START ADJUSTMENT FACTORS

DIESEL GENERATOR COLD-START ADJUSTMENT FACTORS

ICF INTERNATIONAL, APRIL-2011

Short-term concentration trends for VOC, CO and NOx immediately following a cold start by a large diesel backup generator were measured by the California Energy Commission for their document :Air Quality Implications of Backup Generators in California” dated July 2005. They used continuous monitors to measure the following trends, which are shown in the attached figure:

During the first 14 seconds after cold-start, the VOC concentration spiked up to a maximum value of 900 ppm before dropping back to the steady state value of 30 ppm. The area under the concentration-vs-time curve represents a “VOC spike” of 6,300 ppm-sec..

It took 8 seconds for the NOx concentration to ramp up to its steady state value of 38 ppm. The area under the concentration-vs-time curve represents the “NOx deficit” of 160 ppm-sec.

The Cold Start Adjustment Factor for DPM was estimated by assuming the concentration trend for DPM should be similar to the trend for VOC. In that case, for any generator operating period after a cold start, the adjustment factor is the area under the VOC Spike divided by the area under the 30 ppm steady state concentration profile.

Example: DPM emissions for 1-hour Generator Runtime After Cold Start

The steady state VOC concentration is 30 ppm. For a 1-hour runtime the VOC emission is the area under the concentration-vs-time curve, or 30 ppm x 3600 seconds = 108,000 ppm-sec.

The “cold start factor” is the VOC spike area divided by the steady state area:

$$(6300 \text{ ppm-sec}) / (108,000 \text{ ppm-sec}) = 0.058.$$

So during the 1-hour period following a cold start the overall DPM emission factor is adjusted by the “cold start factor” of 1.058.

Example: NOx Emissions During 1-Hour Runtime Following Cold Start

NOx Deficit = 160 ppm-sec

Steady-state NOx profile = 38 ppm x 3600 sec = 137,000 ppm-sec

NOx Cold Start Factor = $1 - (160/137,000) = 0.999 \times \text{Steady State Emission Factor}$

Table B-1. Emission Factor Adjustments for Cold Start

| Runtime Following Cold Start | DPM | NOx |
|------------------------------|-------|-------|
| 10-minutes | 1.35 | 0.999 |
| 30-minutes | 1.12 | 0.999 |
| 1-hour | 1.058 | 0.999 |
| 8-hours | 1.007 | 0.999 |

Cold Start Emissions for the Detroit 92 at VAF

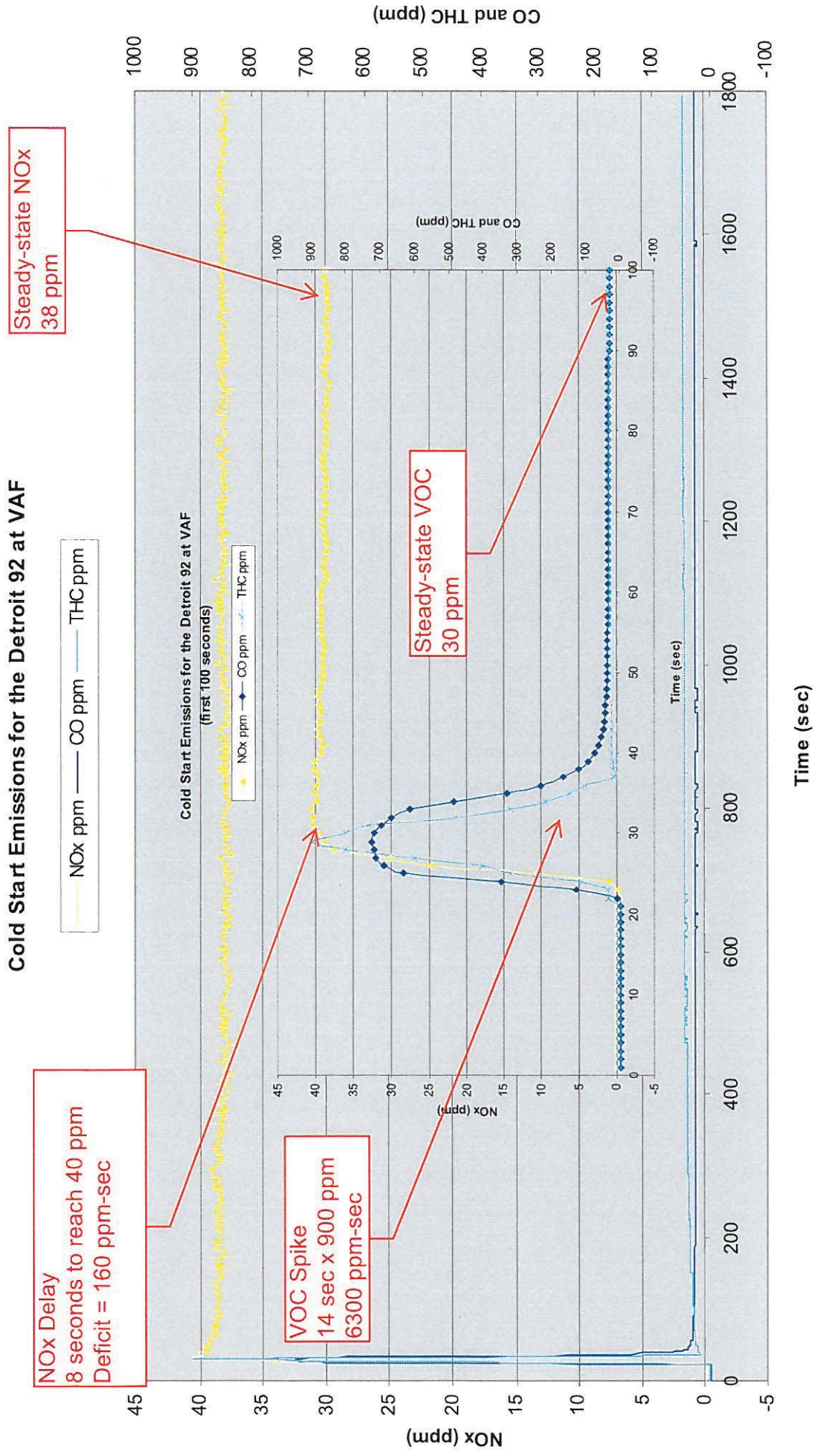
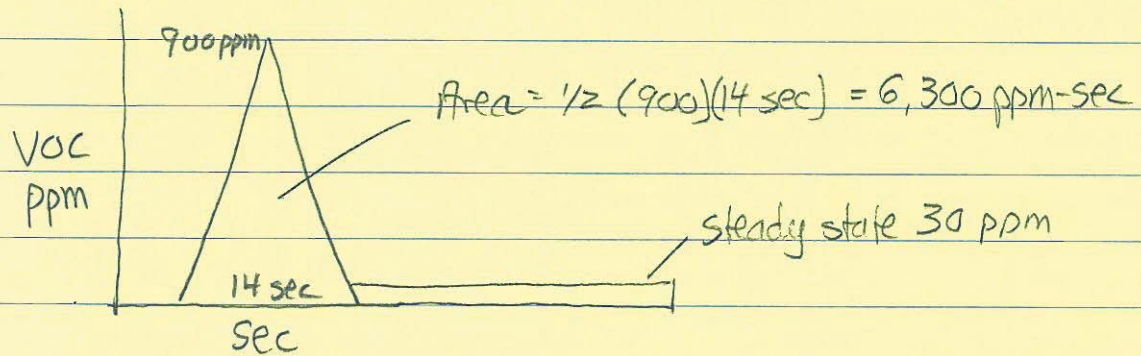


Figure 19. Cold-start emissions for CO and NO_x as a function of time

VOC Spike

$$\text{VOC Spike Area} = \frac{1}{2}(900 \text{ ppm})(14 \text{ sec}) = 6,300 \text{ ppm-sec}$$



Steady State VOC Areas @ 30 ppm

$$10\text{-minutes Area} = 30 \text{ ppm} \times 600 \text{ sec} = 18,000 \text{ ppm-sec}$$

$$\text{Cold-Start Factor} = 6,300 / 18,000 = 0.35$$

So DPM in 1st 10 minutes = 1.35 * steady state

$$30\text{-min Area} = 30 \text{ ppm} \times 30 \text{ min} \times 60 = 54,000 \text{ ppm-sec}$$

$$\text{Cold Start Factor} = 6300 / 54,000 = 0.12$$

So DPM in 1st 30 min = 1.12 * steady state

$$60\text{-minutes} = 30 \text{ ppm} \times 60 \text{ min} \times 60 \text{ sec/min} = 108,000 \text{ ppm-sec}$$

$$\text{Cold start factor} = 6300 / 108,000 = 0.058$$

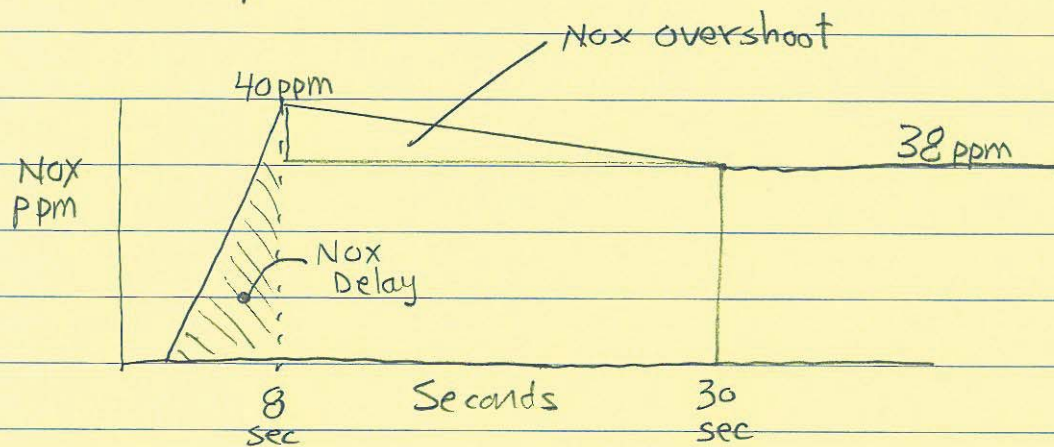
So DPM in 1st 60 min = 1.058 * steady state

$$8\text{-hours: } 30 \text{ ppm} \times 8 \text{ hrs} \times 3600 \text{ sec/hr} = 864,000 \text{ ppm-sec}$$

$$\text{Cold Start factor} = 6300 / 864,000 = 0.0073$$

So DPM in 8-hrs = 1.0073 * steady state

NOx Delay



Nox Delay: 8 secs to reach 40 ppm

$$\text{Area} = \frac{1}{2} (8 \text{ sec}) (40) = 160 \text{ ppm} \cdot \text{sec}$$

Nox Overshoot: 22 secs to drop to 38 ppm

$$\text{Area} = \frac{1}{2} (22 \text{ sec}) (2 \text{ ppm}) = 22 \text{ ppm} \cdot \text{sec}$$

$$\text{Net Deficit} = 22 \text{ ppm} \cdot \text{sec} - 160 \text{ ppm} \cdot \text{sec} = -138 \text{ ppm} \cdot \text{sec}$$

1-hour Nox Cold-Start Factor @ 38 ppm steady state

$$\text{Steady state 1-hr} = 3600 \text{ sec} \times 38 \text{ ppm} = 137,000 \text{ ppm} \cdot \text{sec}$$

$$\text{Cold start factor} = -138 \text{ ppm} \cdot \text{sec} / 137,000 \text{ ppm} \cdot \text{sec}$$

So Cold start adjustment = 0.999 * Steady state

APPENDIX B
EMISSION CALCULATIONS AND AERMOD
DISPERSION FACTORS

Table B-1. Per-Generator Emission Rates in lbs/hour

| MTU's Stable Condition Not-to-Exceed (Stack Test Limits), lbs/hour | | | | | |
|---|-----------|------------|--------------------|-----------|------------|
| Electrical Load | PM | Nox | Primary NO2 | CO | VOC |
| 100% (3,000 kWe) | 0.484 | 10.3 | 0.4 | 1.35 | 0.22 |
| 93% | 0.444 | 9.3 | 0.4 | 1.24 | 0.22 |
| 90% | 0.425 | 8.83 | 0.4 | 1.19 | 0.22 |
| 81% | 0.374 | 7.58 | 0.4 | 1.05 | 0.22 |
| 10% | 0.4 | 2.6 | 1.5 | 0.6 | 0.25 |
| Controlled, Cold-Start, Catalyst-Delayed Emissions Used for AERMOD, lbs/hour | | | | | |
| Electrical Load | PM | Nox | Primary NO2 | CO | VOC |
| 100% | 0.512 | 17.2 | 1.22 | 2.39 | 0.39 |
| 93% | 0.47 | 15.4 | 1.1 | 2.17 | 0.39 |
| 90% | 0.45 | 14.6 | 1.06 | 2.11 | 0.39 |
| 81% | 0.396 | 12.5 | 0.95 | 1.93 | 0.39 |
| 10% | 0.422 | 3.12 | 0.88 | 1.41 | 0.61 |
| Nominal Uncontrolled Emissions, lbs/hour | | | | | |
| Electrical Load | PM | Nox | Primary NO2 | CO | VOC |
| 100% | 3.23 | 51.7 | 5.17 | 6.8 | 1.1 |
| 93% | 2.96 | 46.1 | 4.61 | 6.3 | 1.1 |
| 90% | 2.83 | 43.6 | 4.36 | 6 | 1.1 |
| 81% | 2.49 | 37.2 | 3.72 | 5.3 | 1.1 |
| 10% | 2.67 | 5.7 | 0.57 | 2.8 | 1.2 |

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Table B-2a. Fuel Usage and Emissions During Startup/Commissioning Testing

| Activity | Hours | Load | Per-Gen Fuel, gal/hr | Per-Generator lbs/hr | | | | Per-Generator Startup Emissions, lbs | | | | Per-Gen Fuel, gal |
|--|-------|------|----------------------|----------------------|-------|------|------|--------------------------------------|--------|--------|--------|-------------------|
| | | | | PM | NOX | VOC | CO | PM | NOX | VOC | CO | |
| Level 3 Testing | 8 | 100% | 232 | 0.512 | 17.2 | 0.39 | 2.39 | 4.10 | 138 | 3.1 | 19.1 | 1,856 |
| Level 4 Testing | 12 | 75% | 183 | 0.357 | 11.02 | 0.39 | 1.69 | 4.28 | 132 | 4.7 | 20.3 | 2,196 |
| Level 5 Testing | 20 | 100% | 232 | 0.512 | 17.2 | 0.39 | 2.39 | 10.2 | 344 | 7.8 | 47.8 | 4,640 |
| Combined Startup/Commissioning Each Generator | | | | | | | | 18.6 | 614 | 16 | 87.2 | 8,692 |
| Number of Generators Tested 70-year period | | | | | | | | 17 | 17 | 17 | 17 | 17 |
| Facility-Wide Startup/Commissioning, Combined 17 Generators (lbs) | | | | | | | | 317 | 10,435 | 265 | 1,482 | 147,764 |
| Annualized 70-yr Average Startup emissions (tons/yr) | | | | | | | | 0.0023 | 0.0745 | 0.0019 | 0.0106 | |
| Number of Generators Commissioned Mx Year of Full buildout | | | | | | | | 5 | 5 | 5 | 5 | 5 |
| 5-Genset Max Buildout Peak Year (lbs) | | | | | | | | 93 | 3,069 | 78 | 436 | 43,460 |
| Facility-Wide DEEP Emissions from Startup Testing (tons) | | | | | | | | 0.158 | 5.218 | 0.133 | 0.741 | |
| Facility-Wide DEEP Emissions from Routine Operations (tons) | | | | | | | | 0.221 | 5.83 | 0.36 | 1.22 | |
| 70-Year DEEP Emissions from Routine Operations (tons) | | | | | | | | 15.47 | 408.1 | 25.2 | 85.4 | |
| Fraction of 70-Year Emissions Contributed by Initial Startup Testing and Commissioning | | | | | | | | 1.0% | 1.3% | 0.5% | 0.9% | |

Table B-2B. Fuel Usage and Emissions During Triennial Stack Testing

| Activity | Hours | Load | Per-Gen Fuel, gal/hr | Warmed Up Per-Generator lbs/hr | | | | Per-Generator Startup Emissions, lbs | | | | Per-Gen Fuel, gal |
|--|-------|------|----------------------|--------------------------------|------|------|------|--------------------------------------|---------|---------|---------|-------------------|
| | | | | PM | NOX | VOC | CO | PM | NOX | VOC | CO | |
| Stack Testing | 10 | 100% | 232 | 0.484 | 10.3 | 0.22 | 1.35 | 4.84 | 103 | 2.2 | 13.5 | 2,320 |
| Combined Stack Testing Each Generator | | | | | | | | 4.8 | 103 | 2 | 13.5 | 2,320 |
| Number of Generators Tested any one year | | | | | | | | 7 | 7 | 7 | 7 | 7 |
| Max-year stack testing of Generators (lbs) | | | | | | | | 34 | 721 | 15 | 95 | 16,240 |
| 3-yr Annualized Stack Testing, tons/yr (5.7 gens each year) | | | | | | | | 0.01379 | 0.29355 | 0.00627 | 0.03848 | |
| Facility-Wide DEEP Emissions from Routine Operations (tons) | | | | | | | | 0.221 | 5.83 | 0.36 | 1.22 | |
| Fraction of Routine Operational Emissions Contributed by Triennial Stack Testing | | | | | | | | 6.2% | 5.0% | 1.7% | 3.2% | |
| Fraction of Routine Operational Emissions Contributed by Triennial Stack Testing and Initial Startup/Commissioning | | | | | | | | 7.3% | 6.3% | 2.3% | 4.0% | |

Table B-3

CATALYST-DELAY EMISSION FACTORS

| NOX-NO2 AFTER DISCUSSIONS WITH JAMES RICHMOND AND TODD SNARR, 9-13-2012 | | | | | | | | | | | | | | | | | | |
|---|---------------------|-----------------|----------------------------|---------------------------|---|--------------------------|---------------------------|---------------------------------|--|------|---------------------|-----------------|----------------------------|---------------------------|---------------------|--------------------------|---------------------------|---------------------------------|
| Elm-Approved Increases-Decreases NO2 Emissions (lbs/hr) Accounting For Catalyst Delay Time | | | | | Elm-Approved Increases-Decreases NOX Emissions (lbs/hr) Accounting For Catalyst Delay Time | | | | | | | | | | | | | |
| Load | Tot Run Time Min | Warm Up time | Untreated NO2 lbs/hr | Subtotal Time x NO2 | Treated Time Min | Treated NO2 lbs/hr | Subtotal Time x NO2 | Wt. Average NO2 lbs/hr | | Load | Tot Run Time Min | Warm Up time | Untreated NOX lbs/hr | Subtotal Time x NOX | Treated Time Min | Treated NOX lbs/hr | Subtotal Time x NOX | Wt. Average NOX lbs/hr |
| 81 | 60 | 10 | 3.72 | 0.62 | 50 | 0.4 | 0.333333 | 0.95 | | 81 | 60 | 10 | 37.2 | 6.2 | 50 | 7.58 | 6.316667 | 12.52 |
| 90 | 60 | 10 | 4.36 | 0.727 | 50 | 0.4 | 0.333333 | 1.06 | | 90 | 60 | 10 | 43.6 | 7.267 | 50 | 8.83 | 7.358333 | 14.63 |
| 93 | 60 | 10 | 4.61 | 0.768 | 50 | 0.4 | 0.333333 | 1.10 | | 93 | 60 | 10 | 46.1 | 7.683 | 50 | 9.3 | 7.75 | 15.43 |
| Idle | 60 | 20 | 0.57 | 0.19 | 40 | 1.5 | 1 | 1.190 | | Idle | 60 | 20 | 6 | 2 | 40 | 2.6 | 1.733333 | 3.733 |
| Idle | 30 | 20 | 0.57 | 0.38 | 10 | 1.5 | 0.5 | 0.880 | | Idle | 30 | 20 | 6 | 4 | 10 | 2.6 | 0.866667 | 4.867 |

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Controlled PM Emission Rates

| Load | PM lbs/hr |
|------|-----------|
| 100 | 0.484 |
| 81 | 0.374 |
| 90 | 0.425 |
| 93 | 0.444 |
| Idle | 0.40 |

| Elm-Approved Increases-Decreases CO Emissions (lbs/hr) Accounting For Catalyst Delay Time | | | | | | | | |
|--|---------------------|-----------------|------------------------|--------------------------|---------------------|----------------------|--------------------------|-----------------------------|
| Load | Tot Run Time Min | Warm Up time | Untreated CO lbs/hr | Subtotal Time x CO | Treated Time Min | Treated CO lbs/hr | Subtotal Time x CO | Wt. Average CO lbs/hr |
| 81 | 60 | 10 | 5.3 | 0.883333 | 50 | 1.05 | 0.875 | 1.76 |
| 90 | 60 | 10 | 6 | 1.000 | 50 | 1.19 | 0.991667 | 1.99 |
| 93 | 60 | 10 | 6.3 | 1.050 | 50 | 1.24 | 1.033333 | 2.08 |
| Idle | 60 | 20 | 2.8 | 0.933333 | 40 | 0.6 | 0.4 | 1.333 |
| 50 | 60 | 10 | 4.2 | 0.7 | 50 | 0.84 | 0.7 | 1.40 |
| 60 | 60 | 10 | 4.4 | 0.733333 | 50 | 0.87 | 0.725 | 1.46 |
| 70 | 60 | 10 | 4.6 | 0.766667 | 50 | 0.91 | 0.758333 | 1.53 |
| Idle | 30 | 20 | 2.8 | 1.866667 | 10 | 0.6 | 0.2 | 2.067 |

| Elm-Approved Increases-Decreases VOC Emissions (lbs/hr) Accounting For Catalyst Delay Time | | | | | | | | |
|---|---------------------|-----------------|---------------------|----------------------------|---------------------|-------------------|----------------------------|---------------------------------|
| Load | Tot Run Time Min | Warm Up time | Untreated lbs/hr | Subtotal Time x conc | Treated Time Min | Treated lbs/hr | Subtotal Time x conc | Wt. Average VOC lbs/hr |
| 81 | 60 | 10 | 1.1 | 0.183333 | 50 | 0.22 | 0.183333 | 0.37 |
| 90 | 60 | 10 | 1.1 | 0.183 | 50 | 0.22 | 0.183333 | 0.37 |
| 93 | 60 | 10 | 1.1 | 0.183 | 50 | 0.22 | 0.183333 | 0.37 |
| Idle | 60 | 20 | 1.23 | 0.41 | 40 | 0.25 | 0.166667 | 0.577 |
| 50 | 60 | 10 | 1.1 | 0.183333 | 50 | 0.22 | 0.183333 | 0.37 |
| 60 | 60 | 10 | 1.1 | 0.183333 | 50 | 0.22 | 0.183333 | 0.37 |
| 70 | 60 | 10 | 1.1 | 0.183333 | 50 | 0.22 | 0.183333 | 0.37 |
| Idle | 30 | 20 | 1.23 | 0.82 | 10 | 0.25 | 0.083333 | 0.903 |

Table B-4

ANNUAL EMISSIONS_ Oct-2012-INCREASED IDLE RATE_ Riker Data Center (10-11-2012)

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DAYIME-MASKED TABLE AA. Annual DPM - Scheduled Diagnostic Testing, Power Outage + Storm Avoidance, Corrective Maintenance, and De-energized Building Maintenance,

| Hours at Each Runtime Mode | | | | | | | | | | | | | | AERMOD Hrs/day | Each Genset DPM lbs/hr | Each Genset Fuel Gal/Hr | Each Genset NOX lbs/hr | Each Genset DPM lbs/yr | Facility Wide DPM Tons/yr | Facility- Wide Fuel Gal/Year | Facility Wide NOX Tons/yr | Each Genset CO lbs/hr | Facility- Wide CO Tons/yr | Each Genset HC lbs/hr | Facility- Wide HC Tons/yr | Each Genset NO2 lbs/hr | Facility- Wide NO2 Tons/yr |
|---|----------|----------------|-------------|--------------|-------------------------|---|-----|--------|------|-------|--------|------|--------------|-------------------|---|----------------------------------|---------------------------------|---------------------------------|------------------------------------|------------------------------------|---------------------------------|-----------------------------|---------------------------------|-----------------------------|---------------------------------|---------------------------------|----------------------------------|
| Gen # | Gen Area | Engine Load | No. Gens | W | M | Q | A-F | A-Step | Corr | De-En | Outage | Cool | Total hrs/yr | | | | | | | | | | | | | | |
| A - Unplanned Outage + Storm Avoidance (24 hrs/day) | | | | | | | | | | | | | | | Unplanned Outage + Storm Avoidance | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | | | | | | 24 | | 24 | 24 | 0.396 | 195 | 12.5 | 9.5 | 0.02376 | 23,400 | 0.75 | 1.76 | 0.1056 | 0.37 | 0.0222 | 0.95 | 0.057 |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | | | | | | 24 | | 24 | 24 | 0.45 | 213 | 14.6 | 10.8 | 0.0162 | 15,336 | 0.5256 | 1.99 | 0.07164 | 0.37 | 0.01332 | 1.06 | 0.038 |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | | | | | | 24 | | 24 | 24 | 0.45 | 213 | 14.6 | 10.8 | 0.0162 | 15,336 | 0.5256 | 1.99 | 0.07164 | 0.37 | 0.01332 | 1.06 | 0.038 |
| ETC-1 | ETC | 93% | 1 | | | | | | | | 24 | | 24 | 24 | 0.47 | 220 | 15.4 | 11.3 | 0.00564 | 5,280 | 0.1848 | 2.08 | 0.02496 | 0.37 | 0.00444 | 1.1 | 0.013 |
| Group B - Testing at Full Outage Loads | | | | | | | | | | | | | | | Testing at Full Outage Loads | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | | | 3 | 6 | | | | 17 | 12 | 0.396 | 195 | 12.5 | 6.7 | 0.01683 | 16,575 | 0.53125 | 1.76 | 0.0748 | 0.37 | 0.015725 | 0.95 | 0.040 |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | | | 3 | 6 | | | | 17 | 12 | 0.45 | 213 | 14.6 | 7.7 | 0.01475 | 10,863 | 0.3723 | 1.99 | 0.050745 | 0.37 | 0.009435 | 1.06 | 0.027 |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | | | 3 | 6 | | | | 17 | 12 | 0.45 | 213 | 14.6 | 7.7 | 0.01475 | 10,863 | 0.3723 | 1.99 | 0.050745 | 0.37 | 0.009435 | 1.06 | 0.027 |
| ETC-1 | ETC | 93% | 1 | | | | | | | | 8 | | 17 | 12 | 0.47 | 220 | 15.4 | 8.0 | 0.003995 | 3,740 | 0.1309 | 2.08 | 0.01768 | 0.37 | 0.003145 | 1.1 | 0.009 |
| Group C - 100% Load During Testing (Daytime) | | | | | | | | | | | | | | | Testing at 100% Load | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 100% | 5 | | | | | | 0.5 | 8 | | | 8.5 | 12 | 0.512 | 232 | 17.2 | 4.4 | 0.01088 | 9,860 | 0.3655 | 2.39 | 0.050788 | 0.37 | 0.007863 | 1.22 | 0.026 |
| 2-1 to 2-3 | Bldg 2 | 100% | 3 | | | | | | 0.5 | 8 | | | 8.5 | 12 | 0.512 | 232 | 17.2 | 4.4 | 0.006528 | 5,916 | 0.2193 | 2.39 | 0.030473 | 0.37 | 0.004718 | 1.22 | 0.016 |
| 3-1 to 3-3 | Bldg 3 | 100% | 3 | | | | | | 0.5 | 8 | | | 8.5 | 12 | 0.512 | 232 | 17.2 | 4.4 | 0.006528 | 5,916 | 0.2193 | 2.39 | 0.030473 | 0.37 | 0.004718 | 1.22 | 0.016 |
| ETC-1 | ETC | 100% | 1 | | | | | | 0.5 | 8 | | | 8.5 | 12 | 0.512 | 232 | 17.2 | 4.4 | 0.002176 | 1,972 | 0.0731 | 2.39 | 0.010158 | 0.37 | 0.001573 | 1.22 | 0.005 |
| 1-6 and 1-7 Reserve | Bldg 1 | 100% | 2 | | | | | | 0.5 | 8 | | | 8.5 | 12 | 0.512 | 232 | 17.2 | 4.4 | 0.004352 | 3,944 | 0.1462 | 2.39 | 0.020315 | 0.37 | 0.003145 | 1.22 | 0.010 |
| 2-4 Reserve | Bldg 2 | 100% | 1 | | | | | | 0.5 | 8 | | | 8.5 | 12 | 0.512 | 232 | 17.2 | 4.4 | 0.002176 | 1,972 | 0.0731 | 2.39 | 0.010158 | 0.37 | 0.001573 | 1.22 | 0.005 |
| 3-4 Reserve | Bldg 3 | 100% | 1 | | | | | | 0.5 | 8 | | | 8.5 | 12 | 0.512 | 232 | 17.2 | 4.4 | 0.002176 | 1,972 | 0.0731 | 2.39 | 0.010158 | 0.37 | 0.001573 | 1.22 | 0.005 |
| ETC-2 Reserve | ETC | 100% | 1 | | | | | | 0.5 | 8 | | | 8.5 | 12 | 0.512 | 232 | 17.2 | 4.4 | 0.002176 | 1,972 | 0.0731 | 2.39 | 0.010158 | 0.37 | 0.001573 | 1.22 | 0.005 |
| D1 - Idle During Emergency Outages (24 hrs/day) | | | | | | | | | | | | | | | Idle During Outages (24 hrs/day) | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 10% | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 24 | 0.4224 | 45 | 3.73 | 1.7 | 0.004224 | 900 | 0.0373 | 1.333 | 0.01333 | 0.577 | 0.00577 | 1.19 | 0.012 |
| 2-1 to 2-3 | Bldg 2 | 10% | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 24 | 0.4224 | 45 | 3.73 | 1.7 | 0.002534 | 540 | 0.02238 | 1.333 | 0.007998 | 0.577 | 0.003462 | 1.19 | 0.007 |
| 3-1 to 3-3 | Bldg 3 | 10% | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 24 | 0.4224 | 45 | 3.73 | 1.7 | 0.002534 | 540 | 0.02238 | 1.333 | 0.007998 | 0.577 | 0.003462 | 1.19 | 0.007 |
| ETC-1 | ETC | 10% | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 24 | 0.4224 | 45 | 3.73 | 1.7 | 0.000845 | 180 | 0.00746 | 1.333 | 0.002666 | 0.577 | 0.001154 | 1.19 | 0.002 |
| 1-6 and 1-7 Reserve | Bldg 1 | 10% | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 1 | 13 | 24 | 0.4224 | 45 | 3.73 | 5.5 | 0.005491 | 1,170 | 0.04849 | 1.333 | 0.017329 | 0.577 | 0.007501 | 1.19 | 0.015 |
| 2-4 Reserve | Bldg 2 | 10% | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 1 | 25 | 24 | 0.4224 | 45 | 3.73 | 10.6 | 0.00528 | 1,125 | 0.046625 | 1.333 | 0.016663 | 0.577 | 0.007213 | 1.19 | 0.015 |
| 3-4 Reserve | Bldg 3 | 10% | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 1 | 25 | 24 | 0.4224 | 45 | 3.73 | 10.6 | 0.00528 | 1,125 | 0.046625 | 1.333 | 0.016663 | 0.577 | 0.007213 | 1.19 | 0.015 |
| ETC-2 Reserve | ETC | 10% | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 1 | 25 | 24 | 0.4224 | 45 | 3.73 | 10.6 | 0.00528 | 1,125 | 0.046625 | 1.333 | 0.016663 | 0.577 | 0.007213 | 1.19 | 0.015 |
| D2 - Idle During Testing (Daytime Only) | | | | | | | | | | | | | | | Idle During Testing (Daytime Only) | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 10% | 5 | 20 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 5.5 | 28.5 | 12 | 0.4224 | 45 | 3.73 | 12.0 | 0.030096 | 6,413 | 0.265763 | 2.07 | 0.147488 | 0.903 | 0.064339 | 0.88 | 0.063 |
| 2-1 to 2-3 | Bldg 2 | 10% | 3 | 20 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 5.5 | 28.5 | 12 | 0.4224 | 45 | 3.73 | 12.0 | 0.018058 | 3,848 | 0.159458 | 2.07 | 0.088493 | 0.903 | 0.038603 | 0.88 | 0.038 |
| 3-1 to 3-3 | Bldg 3 | 10% | 3 | 20 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 5.5 | 28.5 | 12 | 0.4224 | 45 | 3.73 | 12.0 | 0.018058 | 3,848 | 0.159458 | 2.07 | 0.088493 | 0.903 | 0.038603 | 0.88 | 0.038 |
| ETC-1 | ETC | 10% | 1 | 20 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 5.5 | 28.5 | 12 | 0.4224 | 45 | 3.73 | 12.0 | 0.006019 | 1,283 | 0.053153 | 2.07 | 0.029498 | 0.903 | 0.012868 | 0.88 | 0.013 |
| 1-6 and 1-7 Reserve | Bldg 1 | 10% | 2 | 20 | 3 | 3 | 6 | | | 8 | 0 | 0.5 | 40.5 | 12 | 0.4224 | 45 | 3.73 | 17.1 | 0.017107 | 3,645 | 0.151065 | 2.07 | 0.083835 | 0.903 | 0.036572 | 0.88 | 0.036 |
| 2-4 Reserve | Bldg 2 | 10% | 1 | 20 | 3 | 3 | 6 | | | 8 | 0 | 0.5 | 40.5 | 12 | 0.4224 | 45 | 3.73 | 17.1 | 0.008554 | 1,823 | 0.075533 | 2.07 | 0.041918 | 0.903 | 0.018286 | 0.88 | 0.018 |
| 3-4 Reserve | Bldg 3 | 10% | 1 | 20 | 3 | 3 | 6 | | | 8 | 0 | 0.5 | 40.5 | 12 | 0.4224 | 45 | 3.73 | 17.1 | 0.008554 | 1,823 | 0.075533 | 2.07 | 0.041918 | 0.903 | 0.018286 | 0.88 | 0.018 |
| ETC-2 Reserve | ETC | 10% | 1 | 20 | 3 | 3 | 6 | | | 8 | 0 | 0.5 | 40.5 | 12 | 0.4224 | 45 | 3.73 | 17.1 | 0.008554 | 1,823 | 0.075533 | 2.07 | 0.041918 | 0.903 | 0.018286 | 0.88 | 0.018 |
| New Group E - 100% Load During Stack Testing + Commissioning (Daytime Only) | | | | | | | | | | | | | | | 100% Load During Stack Testing + Commissioning (Daytime Only) | | | | | | | | | | | | |
| Gen # | Gen Area | Engine Load | No. Gens | 1/70 Comm | 1/3 Stack Testing | Q | A-F | A-Step | Corr | De-En | Outage | Cool | Total hrs/yr | AERMOD Hrs/day | Each Genset DPM lbs/hr | Each Genset Fuel Gal/Hr | Each Genset NOX lbs/hr | Each Genset DPM lbs/yr | Facility Wide DPM Tons/yr | Facility- Wide Fuel Gal/Year | Facility Wide NOX Tons/yr | Each Genset CO lbs/hr | Facility- Wide CO Tons/yr | Each Genset HC lbs/hr | Facility- Wide HC Tons/yr | Each Genset NO2 lbs/hr | Facility Wide NO2 Tons/yr |
| 1-1 to 1-5 | Bldg 1 | 100% | 5 | 0.519 | 3.33 | | | | | | | | 3,849 | 12 | 0.512 | 232 | 17.2 | 1.97 | 0.004927 | 4,465 | 0.165507 | 2.39 | 0.022998 | 0.37 | 0.00356 | 1.22 | 0.012 |
| 2-1 to 2-3 | Bldg 2 | 100% | 3 | 0.519 | 3.33 | | | | | | | | 3,849 | 12 | 0.512 | 232 | 17.2 | 1.97 | 0.002956 | 2,679 | 0.099304 | 2.39 | 0.013799 | 0.37 | 0.002136 | 1.22 | 0.007 |
| 3-1 to 3-3 | Bldg 3 | 100% | 3 | 0.519 | 3.33 | | | | | | | | 3,849 | 12 | 0.512 | 232 | 17.2 | 1.97 | 0.002956 | 2,679 | 0.099304 | 2.39 | 0.013799 | 0.37 | 0.002136 | 1.22 | 0.007 |
| ETC-1 | ETC | 100% | 1 | 0.519 | 3.33 | | | | | | | | 3,849 | 12 | 0.512 | 232 | 17.2 | 1.97 | 0.000985 | 893 | 0.033101 | 2.39 | 0.0046 | 0.37 | 0.000712 | 1.22 | 0.002 |
| 1-6 and 1-7 Reserve | Bldg 1 | 100% | 2 | 0.519 | 3.33 | | | | | | | | 3,849 | 12 | 0.512 | 232 | 17.2 | 1.97 | 0.001971 | 1,786 | 0.066203 | 2.39 | 0.009199 | 0.37 | 0.001424 | 1.22 | 0.005 |
| 2-4 Reserve | Bldg 2 | 100% | 1 | 0.519 | 3.33 | | | | | | | | 3,849 | 12 | 0.512 | 232 | 17.2 | 1.97 | 0.000985 | 893 | 0.033101 | 2.39 | 0.0046 | 0.37 | 0.000712 | 1.22 | 0.002 |
| 3-4 Reserve | Bldg 3 | 100% | 1 | 0.519 | 3.33 | | | | | | | | 3,849 | 12 | 0.512 | 232 | 17.2 | 1.97 | 0.000985 | 893 | 0.033101 | 2.39 | 0.0046 | 0.37 | 0.000712 | 1.22 | 0.002 |
| ETC-2 Reserve | ETC | 100% | 1 | 0.519 | 3.33 | | | | | | | | 3,849 | 12 | 0.512 | 232 | 17.2 | 1.97 | 0.000985 | 893 | 0.033101 | 2.39 | 0.0046 | 0.37 | 0.000712 | 1.22 | 0.002 |
| | | | | | | | | | | | | | | | 70-yr Facility-Wide Incl. Startup and Stack Testing | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | 70-yr Facility-Wide Routine Annual | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | 0.306 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | 181,305 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | 6.49 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | 1.38 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | 0.419 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | 0.707 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | 0.289 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | 166,125 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | |

APPENDIX C
AERMOD STACK PARAMETERS

Vantage Data Center - Annual DEEP

KLK 09-20-2012

Revised NO2 Limit (Higher idle emissions during 30 min weekly testing)

AERMOD File: Vantage Annual DPM_S_Sep Rev

AERMOD File (full grid for 20080: Vantage Annual DPM_AA2_Oct2012)

AERMOD Output:

| Year | Maximum | | Max along property | | Max near SW home |
|------|---------|------------|--------------------|------------------------------|------------------|
| | Conc. | Location | Conc. | Location | Conc. |
| 2004 | 0.0417 | Building 1 | 0.028 | South Boundary | 0.020 |
| 2005 | 0.0438 | Building 1 | 0.030 | South Boundary | 0.020 |
| 2006 | 0.0381 | Office B | 0.027 | East Boundary next to Bldg 3 | 0.019 |
| 2007 | 0.0386 | Office B | 0.032 | East Boundary next to Bldg 3 | 0.022 |
| 2008 | 0.0475 | Building 1 | 0.042 | East Boundary next to Bldg 3 | 0.031 |

2008 AERMOD Output:

| Maximum | |
|---------|---|
| Conc. | Location |
| 0.047 | Point of max impact - rooftop of Building 1 |
| 0.047 | MICR - Building 1 |
| 0.042 | MIBR - along east property, approximately 360 meters from north fenceline |
| 0.031 | MIRR - at closest property line (SW home) |
| 0.018 | MIRR - at house structure (SW home) |
| 0.026 | Maximum off-site impacted bussiness/office (Sabey) |
| 0.009 | SE home |

TABLE BB2. Sep-2012; Increased Idle Emissions; 24-hr PM10 AERMOD Input for Full Power Outage

G:\Seattle\PNWProjects\PACLAND_11_Riker Data Center\03_Reports-Analyses\NO2 Requested Revised Emission Limits\AERMOD-Input_-Revised DEEP-NOX-NO2_jmw_10-11-2012.xls]BB2-Sep2012_24hr PM10 AERM

| Gen # | Gen Area | Engine Load | Exit Temp (K) | Exit Velocity (m/sec) | Stack Dia (m) | 24-Hr PM10 Rate per Engine (g/sec) | Hours/Day at Each Runtime Mode | | | | | | | | | | | | | | AERMOD Hrs/day | Each Genset PM10 lbs/hr | Each Genset Fuel Gal/Hr | Each Genset NOX lbs/hr | Each Genset PM10 lbs/DAY | Facility Wide PM10 lbs/DAY | Facility-Wide Fuel Gal/DAY | | | | | | | | | | | | | | | | |
|------------------------------------|----------|-------------|---------------|-----------------------|---------------|------------------------------------|--------------------------------|--------|-------|------------|----------|--------------|---|---|---|-----|--------|------|-------------------------|--------|----------------|------------------------------------|-------------------------|------------------------|--------------------------|----------------------------|----------------------------|--------|----------------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|
| | | | | | | | No. Gens | Temp F | ACFM | Dia Inches | Area ft2 | Velocity fps | W | M | Q | A-F | A-Step | Corr | De-En | Outage | | | | | | | | Cool | Total hrs in Max Day | | | | | | | | | | | | | | |
| Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | | | | | | | | | | Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 720 | 29.2 | 0.661 | 4.99E-02 | 5 | 836 | 21208 | 26 | 3.69 | 95.92 | | | | | | | 24 | | 24 | 24 | 0.396 | 195 | 12.5 | 9.5 | 47.5 | 23,400 | | | | | | | | | | | | | | | |
| 2-1 to 2-3 | Bldg 2 | 90% | 742 | 30.3 | 0.661 | 5.68E-02 | 3 | 877 | 22000 | 26 | 3.69 | 99.50 | | | | | | | 24 | | 24 | 24 | 0.45 | 213 | 14.6 | 10.8 | 32.4 | 15,336 | | | | | | | | | | | | | | | |
| 3-1 to 3-3 | Bldg 3 | 90% | 742 | 30.3 | 0.661 | 5.68E-02 | 3 | 877 | 22000 | 26 | 3.69 | 99.50 | | | | | | | 24 | | 24 | 24 | 0.45 | 213 | 14.6 | 10.8 | 32.4 | 15,336 | | | | | | | | | | | | | | | |
| ETC-1 | ETC | 93% | 750 | 30.7 | 0.661 | 5.93E-02 | 1 | 891 | 22273 | 26 | 3.69 | 100.73 | | | | | | | 24 | | 24 | 24 | 0.47 | 220 | 15.4 | 11.3 | 11.3 | 5,280 | | | | | | | | | | | | | | | |
| 10% Idle | | | | | | | | | | | | | | | | | | | | | | Zero Idle | | | | | | | | | | | | | | | | | | | | | |
| 1-6 and 1-7 Reserve | Bldg 1 | 10% | 584 | 7.9 | 0.661 | 5.08E-02 | 2 | 592 | 5741 | 26 | 3.69 | 25.96 | | | | | | | 24 | | 24 | 24 | 0.4028 | 45 | 3.12 | 9.7 | 19.3 | 2,160 | | | | | | | | | | | | | | | |
| 2-4 Reserve | Bldg 2 | 10% | 584 | 7.9 | 0.661 | 5.08E-02 | 1 | 592 | 5741 | 26 | 3.69 | 25.96 | | | | | | | 24 | | 24 | 24 | 0.4028 | 45 | 3.12 | 9.7 | 9.7 | 1,080 | | | | | | | | | | | | | | | |
| 3-4 Reserve | Bldg 3 | 10% | 584 | 7.9 | 0.661 | 5.08E-02 | 1 | 592 | 5741 | 26 | 3.69 | 25.96 | | | | | | | 24 | | 24 | 24 | 0.4028 | 45 | 3.12 | 9.7 | 9.7 | 1,080 | | | | | | | | | | | | | | | |
| ETC-2 Reserve | ETC | 10% | 584 | 7.9 | 0.661 | 5.08E-02 | 1 | 592 | 5741 | 26 | 3.69 | 25.96 | | | | | | | 24 | | 24 | 24 | 0.4028 | 45 | 3.12 | 9.7 | 9.7 | 1,080 | | | | | | | | | | | | | | | |
| Changed by Belle | | | | | | | | | | | | | | | | | | | Facility-Wide Emissions | | 172 | 64,752 | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | lbs/DAY | gal/DAY | | | | | | | | | | | | | | | | | | | | | |

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Vantage Data Center - 24hr PM10 NAAQS

KLK 10-14-2012

24-hr PM10 during Full Power Outage (Increased Idle Emissions)

AERMOD File: Vantage 24hr PM10 Outage_BB2_Oct2012

AERMOD Output:

| Average | Conc/Dep. | East(X) | North(Y) | Year | |
|-------------------|-----------|---------|----------|------|-----------------------|
| 1ST-HIGHEST 24-HR | 20.78 | 287077 | 5236748 | 2005 | |
| 1ST-HIGHEST 24-HR | 18.71 | 287068 | 5236742 | 2005 | |
| 1ST-HIGHEST 24-HR | 17.90 | 287068 | 5236742 | 2006 | |
| 1ST-HIGHEST 24-HR | 23.64 | 287068 | 5236742 | 2007 | |
| 1ST-HIGHEST 24-HR | 28.38 | 287068 | 5236742 | 2008 | Rooftop of Building 1 |

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PM2.5-NAAQS Modeling for Scheduled Maintenance: De-Energized Full-Building Maintenance

Changed by Belle, 12/3

G:\Seattle\PNWProjects\PACLAND_11_Riker Data Center\03_Reports-Analyses\NO2 Requested Revised Emission Limits\AERMOD-Input_-Revised DEEP-NOX-NO2_jmw_10-11-2012.xls)CC2 Sep2012 PM2.5-Maint

TABLE CC2 - SEP 2012, INCRTERASED PER-GENSET IDLE LOAD EMISSIONS, BUT SHUTTING DOWN ONE RESERVE GENSET AFTER 15 MINUTES

Maximum 24-Hour PM2.5 Emission Rates and Stack Parameters for De-energized Full-Building Maintenance at Data Center 1 (Riker Data Center)

| Gen # | Gen Area | Engine Load | Exit Temp (K) | Exit Velocity (m/sec) | Stack Dia (m) | 1st-Highest 24-hr PM2.5 Rate per Engine (g/sec) | No. Gens | Temp F | ACFM | Dia Inches | Area ft2 | Velocity fps | Hours/Year at Each Runtime Mode | | | | | | | | Worst Case Emission Hours on One Day | AERMOD Hrs/day | Each Genset DPM lbs/hr | Facility Wide DPM lbs/day | | | | |
|---|----------|-------------|---------------|-----------------------|---------------|---|----------|--------|-------|------------|----------|--------------|---|---|-------|-----|---------------|------|--------|--------|--------------------------------------|----------------|------------------------|---------------------------|--------|---------------|--|--|
| | | | | | | | | | | | | | W | M | Q | A-F | A-Step | Corr | De-En | Outage | | | | | Cool | Total hrs/day | | |
| De-energized Maintenance at Full Outage Loads | | | | | | | | | | | | | De-energized Maintenance at Full Outage Loads | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 720 | 29.2 | 0.661 | 0.0333 | 5 | 836 | 21208 | 26 | 3.69 | 95.92 | | | 0 | 0 | | | 8 | | 8 | 8 | 12 | | 0.396 | 3.168 | | |
| Zero Idle | | | | | | | | | | | | | Zero Idle | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 10% | 584 | 7.9 | 0.661 | 0.0021 | 5 | 592 | 5741 | 26 | 3.69 | 25.96 | | | | | 0 | | 0.5 | 0.5 | 0.5 | 0.5 | 12 | | 0.4028 | 0.2014 | | |
| 1-6 and 1-7 Reserve | Bldg 1 | 10% | 584 | 7.9 | 0.661 | 0.0339 | 2 | 592 | 5741 | 26 | 3.69 | 25.96 | | | | | 4 | | 0 | 4 | 8 | 8 | 12 | | 0.4028 | 3.224 | | |
| Annual Days Per Year at Data Center 1 | | | | | | | | | | | | | 4 | 1 | | | | | | | 1 | | | | | | | |
| | | | | | | | | | | | | | Idle Emissions | | 6.592 | | lbs/day PM2.5 | | 0.0346 | | g/sec | | | | | | | |

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Vantage Data Center - 24hr PM2.5 NAAQS

KLK 10-14-2012

24-hr PM2.5 for Scheduled Maintenance: De-Energized Full-Building Maintenance

AERMOD File: Bldg1 24hr PM25 Maintain_CC2_Oct2012

AERMOD Output:

| Average | Conc/Dep. | East(X) | North(Y) | Year | |
|-------------------|-----------|---------|----------|------|------------------------|
| 1ST-HIGHEST 24-HR | 6.65 | 287102 | 5236766 | 2005 | Roof top of Building 1 |
| 1ST-HIGHEST 24-HR | 5.02 | 287068 | 5236742 | 2005 | |
| 1ST-HIGHEST 24-HR | 4.90 | 287068 | 5236742 | 2006 | |
| 1ST-HIGHEST 24-HR | 5.15 | 287068 | 5236742 | 2007 | |
| 1ST-HIGHEST 24-HR | 6.60 | 287068 | 5236742 | 2008 | |

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DD2 - SEP-2012_NO2-ASIL DURING POWER OUTAGE, RESERVE GENSETS AT IDLE WITH INCREASE NOX AND NO2
 Revised NO2 Limit (Higher idle emissions - Lower emissions at high loads) - Aug 2012

AERMOD File: Vantage 1hr NO2 Outage_Rev Limit v2

PVMRM: NO2/NOx Ratio = see table below; Equilibrium Ratio = 0.9.

Stack Input:

| | | | | | | | | | | Jim's notes 9-18-2012 | | |
|-----------|--------------------|--------------------|---------------------|-----------------------|---------------------|--------------------|------------------------|-----------------------|----------------|------------------------|-----------------------------|-------|
| Source ID | Source Description | Easting (X) (m) | Northing (Y) (m) | Base Elevation (m) | Stack Height (m) | Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | NOX (lb/hr) | Primary NO2 (lb/hr) | Stack NO2:NOx Mass Ratio | |
| 1 | 1_1 | 81% Load | 287054.05 | 5236880.14 | 402.336 | 12.4968 | 720 | 29.2 | 0.6604 | 12.5 | 0.95 | 7.6% |
| 2 | 1_2 | 81% Load | 287057.12 | 5236875.48 | 402.336 | 12.4968 | 720 | 29.2 | 0.6604 | 12.5 | 0.95 | 7.6% |
| 3 | 1_3 | 81% Load | 287061.43 | 5236868.98 | 402.336 | 12.4968 | 720 | 29.2 | 0.6604 | 12.5 | 0.95 | 7.6% |
| 4 | 1_4 | 81% Load | 287065.53 | 5236862.87 | 402.336 | 12.4968 | 720 | 29.2 | 0.6604 | 12.5 | 0.95 | 7.6% |
| 5 | 1_5 | 81% Load | 287069.59 | 5236856.78 | 402.336 | 12.4968 | 720 | 29.2 | 0.6604 | 12.5 | 0.95 | 7.6% |
| 6 | 1_6R | 10% Load | 287073.68 | 5236850.63 | 402.336 | 12.4968 | 584 | 7.9 | 0.6604 | 3.73 | 1.19 | 31.9% |
| 7 | 1_7R | 10% Load | 287077.74 | 5236844.57 | 402.336 | 12.4968 | 584 | 7.9 | 0.6604 | 3.73 | 1.19 | 31.9% |
| 8 | 2_1 | 90% Load | 287173.92 | 5237286.15 | 406.2984 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 9 | 2_2 | 90% Load | 287165.37 | 5237280.84 | 406.2984 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 10 | 2_3 | 90% Load | 287156.44 | 5237275.28 | 406.2984 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 11 | 2_4R | 10% Load | 287147.9 | 5237269.94 | 406.2984 | 12.4968 | 584 | 7.9 | 0.6604 | 3.73 | 1.19 | 31.9% |
| 12 | 3_1 | 90% Load | 287136.21 | 5237037.04 | 403.86 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 13 | 3_2 | 90% Load | 287144.21 | 5237030.91 | 403.86 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 14 | 3_3 | 90% Load | 287152.15 | 5237024.82 | 403.86 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 15 | 3_4R | 10% Load | 287160.17 | 5237018.74 | 403.86 | 12.4968 | 584 | 7.9 | 0.6604 | 3.73 | 1.19 | 31.9% |
| 16 | ETC_1 | 93% Load | 287063.11 | 5237220.51 | 406.6032 | 13.3502 | 750 | 30.7 | 0.6604 | 15.4 | 1.1 | 7.1% |
| 17 | ETC_2R | 10% Load | 287056.99 | 5237227.29 | 406.6032 | 13.3502 | 584 | 7.9 | 0.6604 | 3.73 | 1.19 | 31.9% |

184.15

18.16

Vantage Data Center - 1hr NO2 ASIL

KLK 10-14-2012

Revised NO2 Limit (Higher idle emissions - Lower emissions at high loads)

AERMOD File: Vantage 1hr NO2 Outage_DD2_Oct2012

PVMRM: NO2/NOx Ratio = 0.1; Equilibrium Ratio = 0.9.

Stack Input:

| Source ID | Source Description | Easting (X) (m) | Northing (Y) (m) | Base Elevation (m) | Stack Height (m) | Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | Jim's notes 9-18-2012 | | |
|-----------|--------------------|--------------------|---------------------|-----------------------|---------------------|--------------------|------------------------|-----------------------|-----------------------|------------------------|---------------|
| | | | | | | | | | NOX (lb/hr) | Primary NO2 (lb/hr) | NO2:NOx Ratio |
| 1_1 | 81% Load | 287054.05 | 5236880.14 | 402.34 | 12.4968 | 720 | 29.2 | 0.6604 | 12.5 | 0.95 | 7.6% |
| 1_2 | 81% Load | 287057.12 | 5236875.48 | 402.34 | 12.4968 | 720 | 29.2 | 0.6604 | 12.5 | 0.95 | 7.6% |
| 1_3 | 81% Load | 287061.43 | 5236868.98 | 402.34 | 12.4968 | 720 | 29.2 | 0.6604 | 12.5 | 0.95 | 7.6% |
| 1_4 | 81% Load | 287065.53 | 5236862.87 | 402.34 | 12.4968 | 720 | 29.2 | 0.6604 | 12.5 | 0.95 | 7.6% |
| 1_5 | 81% Load | 287069.59 | 5236856.78 | 402.34 | 12.4968 | 720 | 29.2 | 0.6604 | 12.5 | 0.95 | 7.6% |
| 1_6R | 10% Load | 287073.68 | 5236850.63 | 402.34 | 12.4968 | 584 | 7.9 | 0.6604 | 3.73 | 1.19 | 31.9% |
| 1_7R | 10% Load | 287077.74 | 5236844.57 | 402.34 | 12.4968 | 584 | 7.9 | 0.6604 | 3.73 | 1.19 | 31.9% |
| 2_1 | 90% Load | 287173.92 | 5237286.15 | 406.30 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 2_2 | 90% Load | 287165.37 | 5237280.84 | 406.30 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 2_3 | 90% Load | 287156.44 | 5237275.28 | 406.30 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 2_4R | 10% Load | 287147.9 | 5237269.94 | 406.30 | 12.4968 | 584 | 7.9 | 0.6604 | 3.73 | 1.19 | 31.9% |
| 3_1 | 90% Load | 287136.21 | 5237037.04 | 403.86 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 3_2 | 90% Load | 287144.21 | 5237030.91 | 403.86 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 3_3 | 90% Load | 287152.15 | 5237024.82 | 403.86 | 12.4968 | 742 | 30.3 | 0.6604 | 14.6 | 1.06 | 7.3% |
| 3_4R | 10% Load | 287160.17 | 5237018.74 | 403.86 | 12.4968 | 584 | 7.9 | 0.6604 | 3.73 | 1.19 | 31.9% |
| ETC_1 | 93% Load | 287063.11 | 5237220.51 | 406.60 | 13.3502 | 750 | 30.7 | 0.6604 | 15.4 | 1.1 | 7.1% |
| ETC_2R | 10% Load | 287056.99 | 5237227.29 | 406.60 | 13.3502 | 584 | 7.9 | 0.6604 | 3.73 | 1.19 | 31.9% |

AERMOD Output:

| Average | Conc/Dep. | East(X) | North(Y) | Year |
|----------------------------|-----------|---------|----------|------|
| 1ST-HIGHEST MAX DAILY 1-HR | 336 | 287096 | 5236775 | 2004 |
| 1ST-HIGHEST MAX DAILY 1-HR | 351 | 286999 | 5236686 | 2005 |
| 1ST-HIGHEST MAX DAILY 1-HR | 342 | 286994 | 5236693 | 2006 |
| 1ST-HIGHEST MAX DAILY 1-HR | 335 | 287090 | 5236784 | 2007 |
| 1ST-HIGHEST MAX DAILY 1-HR | 345 | 287004 | 5236678 | 2008 |

Along SW fenceline

**FF2-Vantage Data Center - Sep-2012, NO2 NAAQS, Bldg 3 with 30-minute test and Elm's Nox/NO2 limits
Revised NO2 Limit (Higher idle emissions during 30 min weekly testing) - Sep 2012**

Stack Run Time: 7 am to 6 pm

Stack Input:

| Stack Input: | | | | | | | | | Jim's notes 9-18-12 (30 minute test) | | |
|--------------|-------------------------|--------------------|---------------------|--------------------|--------------------|------------------|-----------------------|-------------------|--------------------------------------|---------------------|---------------|
| Source ID | Source Description | Easting (X) (m) | Northing (Y) (m) | Base Elevat (m) | Stack Heigh (m) | Temperatu (K) | Exit Velocit (m/s) | Stack Diam (m) | Prim NOX (lb/hr) | Prim NO2 (lb/hr) | NO2:NOX Ratio |
| 3_1 | weekly testing 10% load | 287136.2 | 5237037 | 403.86 | 12.5 | 584 | 7.9 | 0.6604 | 4.87 | 0.88 | 18.1% |
| 3_2 | weekly testing 10% load | 287144.2 | 5237031 | 403.86 | 12.5 | 584 | 7.9 | 0.6604 | 4.87 | 0.88 | 18.1% |
| 3_3 | weekly testing 10% load | 287152.2 | 5237025 | 403.86 | 12.5 | 584 | 7.9 | 0.6604 | 4.87 | 0.88 | 18.1% |
| | | | | | | | | | 14.61 | 2.64 | |

G:\Seattle\PNWProjects\PACLAND__-11_Riker Data Center\03_Reports-Analyses\NO2 Requested Revised Emission Limits\[AERMOD-Input_-Revised DEEP-NOX-NO2_jmw_10-11-2012.xls]FF2-Sep12_NO2 Bldg3
Test 30 min

AERMOD File: Bldg3 1hr NO2 30min Test_FF2_Oct2012
 PVMRM: NO2/NOx Ratio = 0.181; Equilibrium Ratio = 0.9.
 Stack Run Time: 7 am to 6 pm

Stack Input:

| Source ID | Source Description | Easting (X) (m) | Northing (Y) (m) | Base Elevation (m) | Stack Height (m) | Temperature (K) | Exit Velocity (m/s) | Stack Diameter (m) | Jim's notes 9-18-12 (30 minute test) | | |
|-----------|-------------------------|--------------------|---------------------|-----------------------|---------------------|--------------------|------------------------|-----------------------|--------------------------------------|---------------------|---------------|
| | | | | | | | | | Prim NOX (lb/hr) | Prim NO2 (lb/hr) | NO2:NOX Ratio |
| 3_1 | weekly testing 10% load | 287136.2 | 5237037.0 | 403.9 | 12.5 | 584 | 7.9 | 0.6604 | 4.87 | 0.88 | 18.1% |
| 3_2 | weekly testing 10% load | 287144.2 | 5237030.9 | 403.9 | 12.5 | 584 | 7.9 | 0.6604 | 4.87 | 0.88 | 18.1% |
| 3_3 | weekly testing 10% load | 287152.2 | 5237024.8 | 403.9 | 12.5 | 584 | 7.9 | 0.6604 | 4.87 | 0.88 | 18.1% |

3-Year Average

| Rank | Ave. Conc. | East(X) | North(Y) | Years | |
|------|------------|---------|----------|-----------|--|
| 1st | 243 | 287303 | 5237047 | 2005-2007 | Along east fenceline, next to building 3 |
| 2nd | 229 | 287303 | 5237047 | 2005-2007 | |
| 3rd | 222 | 287303 | 5237047 | 2005-2007 | |

**1-hr NO2 impact for 30-minute test:
 243 ug/m3 x (30 min / 60 min) = 122 ug/m3**

AERMOD Output:

| Average | Conc./Dep. | East(X) | North(Y) | Year |
|-----------------------------|------------|---------|----------|------|
| 1ST-HIGHEST MAX DAILY 1-HR | 263 | 287303 | 5237037 | 2004 |
| 2ND-HIGHEST MAX DAILY 1-HR | 246 | 287303 | 5237037 | 2004 |
| 3RD-HIGHEST MAX DAILY 1-HR | 220 | 287303 | 5237047 | 2004 |
| 4TH-HIGHEST MAX DAILY 1-HR | 212 | 287303 | 5237047 | 2004 |
| 5TH-HIGHEST MAX DAILY 1-HR | 209 | 287303 | 5237047 | 2004 |
| 6TH-HIGHEST MAX DAILY 1-HR | 194 | 287303 | 5237057 | 2004 |
| 7TH-HIGHEST MAX DAILY 1-HR | 192 | 287303 | 5237057 | 2004 |
| 8TH-HIGHEST MAX DAILY 1-HR | 191 | 287303 | 5237057 | 2004 |
| 9TH-HIGHEST MAX DAILY 1-HR | 180 | 287303 | 5237057 | 2004 |
| 10TH-HIGHEST MAX DAILY 1-HR | 177 | 287303 | 5237057 | 2004 |
| 1ST-HIGHEST MAX DAILY 1-HR | 257 | 287303 | 5237047 | 2005 |
| 2ND-HIGHEST MAX DAILY 1-HR | 250 | 287303 | 5237037 | 2005 |
| 3RD-HIGHEST MAX DAILY 1-HR | 231 | 287303 | 5237047 | 2005 |
| 4TH-HIGHEST MAX DAILY 1-HR | 229 | 287303 | 5237037 | 2005 |
| 5TH-HIGHEST MAX DAILY 1-HR | 223 | 287303 | 5237047 | 2005 |
| 6TH-HIGHEST MAX DAILY 1-HR | 222 | 287303 | 5237047 | 2005 |
| 7TH-HIGHEST MAX DAILY 1-HR | 197 | 287303 | 5237047 | 2005 |
| 8TH-HIGHEST MAX DAILY 1-HR | 189 | 287303 | 5237047 | 2005 |
| 9TH-HIGHEST MAX DAILY 1-HR | 188 | 287303 | 5237047 | 2005 |
| 10TH-HIGHEST MAX DAILY 1-HR | 183 | 287303 | 5237047 | 2005 |
| 1ST-HIGHEST MAX DAILY 1-HR | 232 | 287303 | 5237047 | 2006 |
| 2ND-HIGHEST MAX DAILY 1-HR | 224 | 287303 | 5237047 | 2006 |
| 3RD-HIGHEST MAX DAILY 1-HR | 217 | 287303 | 5237047 | 2006 |
| 4TH-HIGHEST MAX DAILY 1-HR | 201 | 287303 | 5237047 | 2006 |
| 5TH-HIGHEST MAX DAILY 1-HR | 196 | 287303 | 5237047 | 2006 |
| 6TH-HIGHEST MAX DAILY 1-HR | 193 | 287303 | 5237047 | 2006 |
| 7TH-HIGHEST MAX DAILY 1-HR | 187 | 287303 | 5237047 | 2006 |
| 8TH-HIGHEST MAX DAILY 1-HR | 180 | 287303 | 5237047 | 2006 |
| 9TH-HIGHEST MAX DAILY 1-HR | 179 | 287303 | 5237047 | 2006 |
| 10TH-HIGHEST MAX DAILY 1-HR | 173 | 287303 | 5237047 | 2006 |
| 1ST-HIGHEST MAX DAILY 1-HR | 241 | 287303 | 5237047 | 2007 |
| 2ND-HIGHEST MAX DAILY 1-HR | 232 | 287303 | 5237047 | 2007 |
| 3RD-HIGHEST MAX DAILY 1-HR | 227 | 287303 | 5237047 | 2007 |
| 4TH-HIGHEST MAX DAILY 1-HR | 216 | 287303 | 5237047 | 2007 |
| 5TH-HIGHEST MAX DAILY 1-HR | 207 | 287303 | 5237037 | 2007 |
| 6TH-HIGHEST MAX DAILY 1-HR | 200 | 287303 | 5237047 | 2007 |
| 7TH-HIGHEST MAX DAILY 1-HR | 191 | 287303 | 5237047 | 2007 |
| 8TH-HIGHEST MAX DAILY 1-HR | 190 | 287303 | 5237047 | 2007 |
| 9TH-HIGHEST MAX DAILY 1-HR | 189 | 287303 | 5237047 | 2007 |
| 10TH-HIGHEST MAX DAILY 1-HR | 185 | 287303 | 5237047 | 2007 |
| 1ST-HIGHEST MAX DAILY 1-HR | 233 | 287303 | 5237047 | 2008 |
| 2ND-HIGHEST MAX DAILY 1-HR | 226 | 287303 | 5237047 | 2008 |
| 3RD-HIGHEST MAX DAILY 1-HR | 221 | 287303 | 5237047 | 2008 |
| 4TH-HIGHEST MAX DAILY 1-HR | 218 | 287303 | 5237047 | 2008 |
| 5TH-HIGHEST MAX DAILY 1-HR | 206 | 287303 | 5237047 | 2008 |
| 6TH-HIGHEST MAX DAILY 1-HR | 205 | 287303 | 5237047 | 2008 |
| 7TH-HIGHEST MAX DAILY 1-HR | 203 | 287303 | 5237047 | 2008 |
| 8TH-HIGHEST MAX DAILY 1-HR | 201 | 287303 | 5237047 | 2008 |
| 9TH-HIGHEST MAX DAILY 1-HR | 200 | 287303 | 5237047 | 2008 |
| 10TH-HIGHEST MAX DAILY 1-HR | 197 | 287303 | 5237047 | 2008 |

APPENDIX D
GENERATOR SPECIFICATIONS AND EMISSION
CONTROLS

Table D-1. BACT Capital Cost for MTU AirClarity System (SCR and Catalyzed DPF) Vantage Data Center

| Cost Category | Cost Factor | Source of Cost Factor | Quant. | Unit Cost | Subtotal Cost |
|---|------------------------|------------------------|--------|-----------|--------------------|
| Direct Costs | | | | | |
| Purchased Equipment Costs | | | | | |
| FOB Purchase Price | As quoted by MTU | MTU | 17 | \$400,000 | \$6,800,000 |
| Instrumentation | Assume no cost | | 0 | 0 | 0 |
| Sales Tax | WA state tax | WA state tax | 6.5% | -- | \$442,000 |
| Shipping | 0.05A | EPA Cost Manual | 5.0% | -- | \$340,000 |
| Subtotal Purchased Equipment Cost, PEC | | | | | \$7,582,000 |
| Direct Installation Costs | | | | | |
| Enclosure structural supports | Assume no cost | Assume no cost | 0 | \$0 | \$0 |
| Installation | 1/2 of EPA Cost Manual | 1/2 of EPA Cost Manual | 2.5% | -- | \$189,550 |
| Electrical | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Piping | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Insulation | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Painting | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Subtotal Direct Installation Costs | | | | | \$189,550 |
| Site Preparation and Buildings (SP) | | | | | |
| | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Total Direct Costs, DC (PEC + Direct Installation + Site Prep) | | | | | \$7,771,550 |
| Indirect Costs (Installation) | | | | | |
| Engineering | 0.025*PEC | 1/4 of EPA Cost Manual | 2.5% | -- | \$189,550 |
| Construction and field expenses | 0.025*PEC | 1/2 of EPA Cost Manual | 2.5% | -- | \$189,550 |
| Contractor Fees | From DIS data center | From DIS data center | 6.8% | -- | \$532,645 |
| Startup | 0.02*PEC | EPA Cost Manual | 2.0% | -- | \$151,640 |
| Performance Test (Tech support) | 0.01*PEC | EPA Cost Manual | 1.0% | -- | \$75,820 |
| Contingencies | 0.03*PEC | EPA Cost Manual | 3.0% | -- | \$227,460 |
| Subtotal Indirect Costs, IC | | | | | \$1,366,665 |
| Total Capital Investment (TCI = DC+IC) | | | | | \$9,138,215 |

TCI/PEC
1.21

TCI per gen
\$537,542

Table D-2. Vantage Data Center Annualized BACT Cost-Effectiveness for MTU AirClarity System

| Item | Quantity | Units | Unit cost | Subtotal |
|--|------------------------|-------|-----------|------------------|
| Annualized Capital Recovery | | | | |
| Total Capital Cost | | | | \$9,138,215 |
| Capital Recovery Factor, 25 yrs, 4% discount rate | | | | 0.06401 |
| Subtotal Annualized 25-year Capital Recovery Cost | | | | \$584,937 |
| Direct Annual Costs | | | | |
| Annual Admin charges | 2% of TCI (EPA Manual) | | 0.02 | \$182,764 |
| Annual Property tax | 1% of TCI (EPA Manual) | | 0.01 | \$91,382 |
| Annual Insurance | 1% of TCI (EPA Manual) | | 0.01 | \$91,382 |
| Annual operation/labor/maintenance costs: Upperbound estimate would assume CARB's value of \$3.00/hp/year and would result in \$206,000/year. Lower bound estimate would assume zero annual O&M. Mid-range value would account for urea, fuel for pressure drop, increased inspections, periodic OEM visits, and the costs for Ecology's increased emission testing requirements. For this screening-level analysis we assumed the lower-bound annual O&M cost of zero. | | | | |
| Subtotal Direct Annual Costs | | | | \$365,529 |
| Total Annual Cost (Capital Recovery + Direct Annual Costs) | | | | \$950,466 |
| Uncontrolled emissions | | | | 27.6 |
| Assumed Control Efficiency | | | | Varies |
| Annual Tons Removed | | | | 19.92 |
| Cost Effectiveness (\$ per tons combined pollutant destroyed) | | | | \$47,714 |

TCI/gen \$537,542

Combined Pollutants

| Pollutant | DEEP | CO | VOC | NOX |
|-----------------------|------|------|------|-------|
| Uncontrolled TPY | 1.48 | 5.67 | 1.14 | 19.3 |
| Controlled TPY | 0.22 | 1.22 | 0.36 | 5.83 |
| Tons Removed/Year | 1.26 | 4.45 | 0.78 | 13.43 |
| Overall Removal Effcy | 85% | 78% | 68% | 70% |

"Reasonableness Cost-Effectiveness" of Acceptable Control Cost vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Acceptable Annual Cost (\$/year) |
|---|---------------------------------------|----------------------------|---|
| NOX | \$9,473 | 13.43 | \$127,222 per year |
| CO | \$5,000 | 4.45 | \$22,250 per year |
| VOC | \$9,473 | 0.78 | \$7,389 per year |
| PM | \$23,200 | 1.26 | \$29,232 per year |
| Total Acceptable Annual Control Cost for Combined Pollutants | | | \$186,093 per year |
| Actual Annual Control Cost | | | \$950,466 per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Acceptable) |

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DIESEL ENGINE-GENERATOR SET

3000-XC6DT2

3000 kWe / 60 Hz / Standby
480 - 13.8kV

(Reference 2800-XC6DT2 for Prime Rating Technical Data)



SYSTEM RATINGS

Standby

| Voltage (L-L) | 480V | 600V | 4160V | 12470V | 13200V | 13800V |
|------------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Phase | 3 | 3 | 3 | 3 | 3 | 3 |
| PF | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 |
| Hz | 60 | 60 | 60 | 60 | 60 | 60 |
| kW | 3000 | 3000 | 3000 | 3000 | 3000 | 3000 |
| kVA | 3750 | 3750 | 3750 | 3750 | 3750 | 3750 |
| AMPS | 4511 | 3609 | 520 | 174 | 164 | 157 |
| skVA@30% | | | | | | |
| Voltage Dip | 6400 | 6800 | 5250 | C/F | C/F | C/F |
| Generator Model* | 1030FDL1005 | 1030FDS1015 | 1020FDM1204 | 1030FDH1429 | 1030FDH1429 | 1030FDH1429 |
| Temp Rise | 130 °C/27 °C | 125 °C/40 °C | 130 °C/27 °C | 130 °C/27 °C | 130 °C/27 °C | 130 °C/27 °C |
| Connection | 6 LEAD WYE | 6 LEAD WYE | 6 LEAD WYE | 6 LEAD WYE | 6 LEAD WYE | 6 LEAD WYE |

CERTIFICATIONS AND STANDARDS

Emissions –

Engine-generator set is designed and manufactured

UL 2200 / CSA – Optional

– UL 2200 Listed

Performance Assurance Certification (PAC)

– Engine-Generator set ISO 8528-5 f
Transient Response
– Verified product design, quality and performance

Power Rating

– Accepts Rated Load in One Step Per NFPA 110
– Verified product design, quality and performance
operation is approved up to 85%.

STANDARD FEATURES*

MTU Onsit
Global Product Support

20V 4000 Diesel Engine
- 95.4 Liter Displacement
- Common Rail Fuel Injection
- 4-Cy

Generator
- Br
- PMG (P
- 300% Shor
- 2/3 Pitch Windings
- S or 5
- Op
Digital Control Panel(s)
- UL Recognized, CS
- Comple
- L

- Integral Set-Mounted
- Engine Driven Fan

STANDARD EQUIPMENT*

Engine

Air Cleaners
Oil Pump
Oil Drain Extension & S/O Valve
Full Flow Oil Filter
Closed Crankcase Ventilation
Jacket Water Pump
Inter Cooler Water Pump
Thermostats
Blower Fan & Fan Drive
Radiator - Unit Mounted
Electric Starting Motor - 24V
Governor - Electronic Isochronous
Base - Structural Steel
AE Flywheel & Bell Housing
Charging Alternator - 24V
Battery Bo
Flexible Fuel Connectors
Flexible Exhaust Connection

Generator

and motor starting

up to 10 seconds
Self-Ventilated and Drip-Proof
Superior Voltage Regulation
Voltage Regulation, Volts-per-Hertz R

No Load to Full Load Regulation
Brushless Alternator with Brushless Pilot Exciter

2 Bearing, Sealed
Flexible Coupling
Full Amortisseur Windings
125% Rotor Balancing
3-Phase Voltage Sensing
±0.25% Voltage Regulation
Full Load - One S
3% Maximum Harmonic Content

Digital Control Panel(s)

Digital Metering
Engine Parameters
Generator Protection Functions
Engine Protection
CAN Bus ECU Communications
s-Based Sof

Remote Communications to RDP-110 Remote Annunciator
16 Programmable Contact Inputs
Up to 11 Contact Outputs
Recognized, CS
Event Recording
IP 54 Front Panel Rating with Integrated Gasket
NFPA 110 Compatible

APPLICATION DATA

| Engine | |
|------------------------------------|-----------------------------|
| Model | 20V 4000 G83L 6 ECT 4-Cy |
| Arrangement | 20V |
| Displacement: L (in ³) | 95.4 (5,822) |
| Bore: cm (in) | 17 (6.69) |
| Stroke: cm (in) | 21 (8.27) |
| Compression Ratio | 16.5:1 |

| | |
|------------------|-------------------------------|
| Engine Governor | Electronic Isochronous (ADEC) |
| Speed Regulation | ±0.25% |

| Liquid Capacity (Lubrication) | |
|-------------------------------|------------|
| Oil Capacity | 205 (54.2) |
| | 55 (14.5) |
| | 5 |

| Electrical | |
|-----------------------------|----|
| Electric Volts DC | 24 |
| Cold Cranking Amps Under -1 | |

| Fuel System | |
|-----------------------------|-----------|
| Fuel Supply Connection Size | |
| Inlet Connection Size | |
| Recommended Fuel | Diesel #2 |

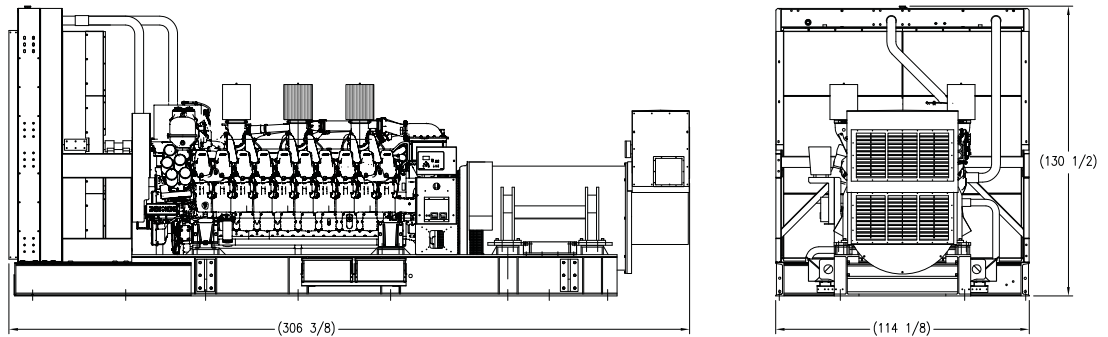
| Fuel Consumption | | |
|------------------|---|---------|
| | | STANDBY |
| 5% of P | 5 | 5 |
| at 50% of P | | |

| Cooling - Radiator System | | |
|---|------------|---------|
| | | STANDBY |
| Maximum Allowable Static Pressure on Rad. Exhaust: kPa (in. H ₂ O) | 0.12 (0.5) | |
| | 56 | |
| | 5 | 50) |
| o Coolant: kW (BTUM) | | |
| o : kW (BTUM) | 70 | (55, |
| o Ambient: kW (BTUM) | | |

| Air Requirements | | |
|--|-------|----------|
| | | STANDBY |
| Aspirating: *m ³ | | |
| Required for | | |
| Cooled Unit: *m ³ | 35,36 | |
| Remote Cooled Applications; Required for | | |
| Used Gen-set | | |
| Max of 25 °F Rise: *m ³ | 40 | (29,500) |

| Exhaust System | | |
|---|-----|---------|
| | | STANDBY |
| Gas Temp. (Stack): °C (°F) | 525 | (977) |
| Gas Volume at Stack Temp: m ³ | | |
| Maximum Allowable Back Pressure: kPa (in. H ₂ O) | 8.5 | (34.1) |

WEIGHTS AND DIMENSIONS



Drawing above for illustration purposes only, based on standard open power 480 volt engine-generator set. Lengths may vary with other voltages. Do not use for installation design. See website for unit specific template drawings.

| System | Dimensions (LxWxH) | Weight (less tank) |
|--------|---|-----------------------|
| OPU | 7,780 x 2,900 x 3,310 mm (306.38 x 114.13 x 130.5 in) | 27,466 kg (60,553 lb) |

Weights and dimensions are based on open power units and are estimates only. Consult the factory for accurate weights and dimensions for your specific engine-generator set.

SOUND DATA

| Unit Type | Standby Full Load |
|--------------------------------|-------------------|
| Level 0: Open Power Unit (dBA) | 107 |

Sound data is provided at 7 m (23 ft). Engine-generator set tested in accordance with ISO 8528-10 and with infinite exhaust.

EMISSIONS DATA

| NO _x + NMHC | CO | PM |
|------------------------|------|------|
| 4.21 | 0.52 | 0.06 |

All units are in g/hp-hr and are EPA D2 cycle values.

Emission levels of the engine may vary as a function of ambient temperature, barometric pressure, humidity, fuel type and quality, installation parameters, measuring instrumentation, etc. The data provided are laboratory results from one engine representing this rating. The data was obtained under controlled environmental conditions with calibrated instrumentation traceable to the United States National Bureau of Standards and in compliance with US EPA regulations found within 40 CFR Part 89. The weighted cycle value from each engine is guaranteed to be below the US EPA Standards at the US EPA defined conditions.

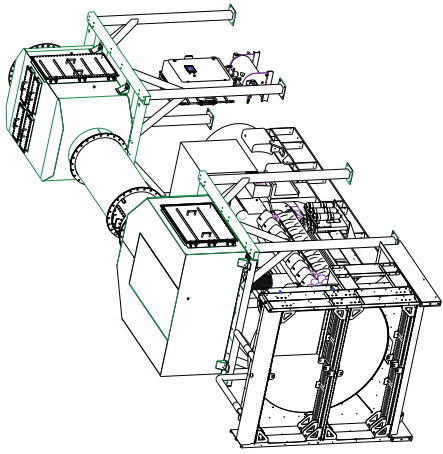
RATING DEFINITIONS AND CONDITIONS

- // Standby ratings apply to installations served by a reliable utility source. The standby rating is applicable to varying loads for the duration of a power outage. No overload capability for this rating. Ratings are in accordance with ISO 8528-1, ISO 3046-1, BS 5514, AS 2789, and DIN 6271.
- // Deration Factor:
 - Altitude:** Consult your local MTU Onsite Energy Power Generation Distributor for altitude derations.
 - Temperature:** Consult your local MTU Onsite Energy Power Generation Distributor for temperature derations.

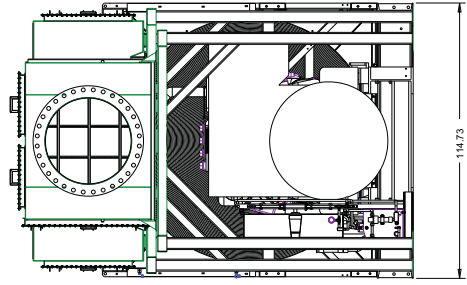
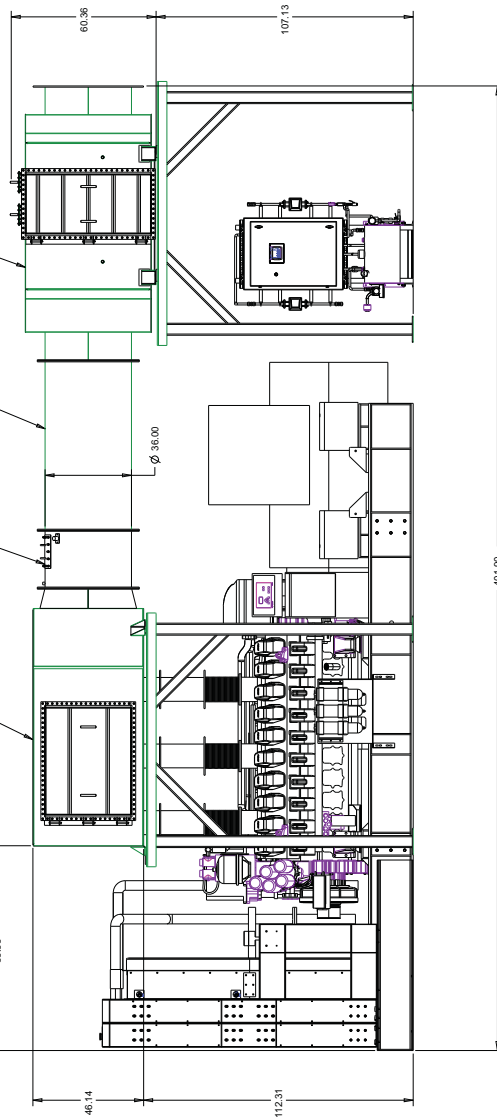
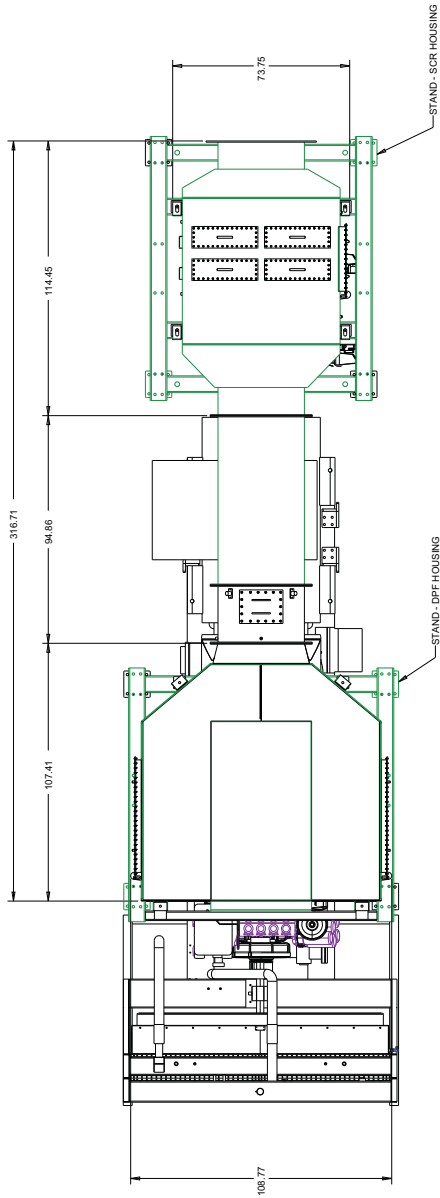
Materials and specifications subject to change without notice.

C/F = Consult Factory/MTU Onsite Energy Distributor

PRELIMINARY



PICTORIAL VIEW



| COMPONENT WEIGHT CHART | |
|------------------------|--------------|
| COMPONENT | WEIGHT (LBS) |
| DPF HOUSING | 3200 |
| MIXING SPOOL | 300 |
| DPF HOUSING | 2700 |
| SCR HOUSING | 2700 |
| STAND-DPF HSG | 1300 |
| STAND-SCR HSG | 1400 |
| DOSING CONTROLLER | 450 |

| | |
|---|------------|
| MATERIAL: | |
| UNIT OF MEASURE: | INCH |
| 3250030002800/2500 BKW MTU TIER IV SYSTEM | |
| AirClarity 3250 | |
| DATE: | 18/23/2011 |
| DRAWN BY: | ESD |
| SCALE: | 1:20 |
| DWG SIZE: | E |
| CHANGE LEVEL: | 01 |
| SHEET: | 1 OF 1 |

GenAcc Products

ELM Permitting Information

9. Narrative of Tier-4 emission control equipment, including vendor-guaranteed removal efficiencies.

The diesel emission control strategy the AirClarity utilizes highly oxidizing precious metal particulate matter filters to control PM, HC, and CO reductions, as well as a Selective Catalytic Reducer coupled with an airless DEF injection system.

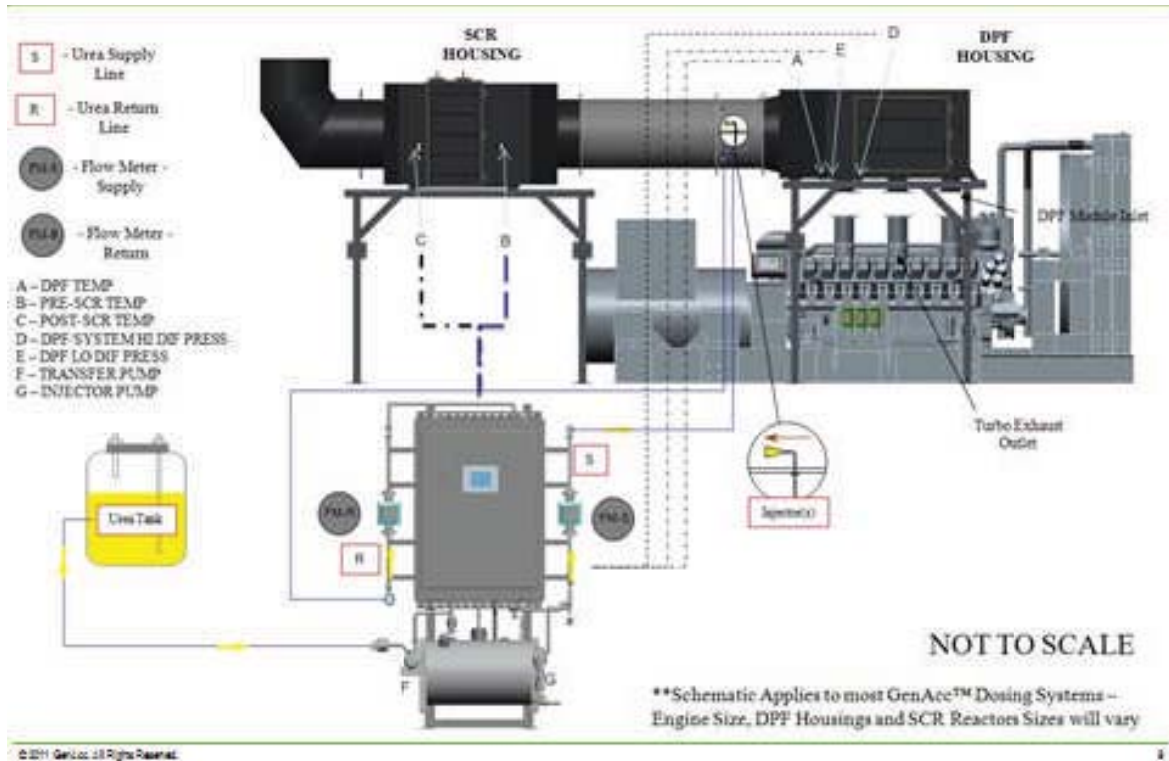
The injection system includes reductant tank level monitoring, return and supply flow metering, DPF temperature, SCR temperature (pre and post), DPF backpressure, system backpressure, and SCR outlet NO_x sensor; all parameters are logged and will produce alarms should the system operate out of spec. A relative humidity sensor will also be utilized in the system, as humidity has been known to affect engine-out NO_x by as much as 15% depending on ambient conditions.

The EnviCat[®] 2055 DPF is a wall flow ceramic Diesel Particulate Filter coated with a Süd-Chemie proprietary precious metal based coating on a cordierite ceramic substrate. The device is designed to filter and passively reduce >95% diesel particulate matter mass found in diesel engine exhaust. Furthermore, carbon monoxide and hydrocarbon emissions in the exhaust are reduced by means of catalytic oxidation. This device does not employ zone coating. The catalyzed DPF is also responsible for reducing hydrocarbons by almost 96%, as well as carbon monoxide reductions of greater than 99% (reductions based on engine baseline and emissions testing at 5-mode average).

The EnviCat[®] 20019 SCR is a flow through ceramic substrate coated with a Süd-Chemie proprietary SCR coating. The SCR is designed to reduce engine out NO_x emissions across a broad range of engine operating conditions.

Vendor-guaranteed removal efficiencies are as follows:

NO_x >90%
CO >90%
HC >90%
PM >87%



10. Has the Tier-4 generator achieved CARB certification? If so, provide the certification data.

No. In process.

11. Vendor-estimated purchase price of emission control equipment compared to Tier-2 generators

Estimated \$400,000 increase per Tier-2 generator.

12. Vendor's "Not-to-Exceed" and "Nominal" emission data.

See attached spreadsheets for both "Not-to-Exceed" (NTE) and nominal controlled emissions information.

13. Narrative of cold-start delay time before catalysts reach activation temperature and perform at vendor-guaranteed removal efficiency

The SCR is designed to operate nominally at 900 degrees Fahrenheit, however NOx conversion can be achieved from 300 to 1000 degrees Fahrenheit. Due to the possibility of forming ammonia salts at lower temperatures, DEF will only be injected at 425 degrees Fahrenheit or higher. Should the temperatures exceed 1000 degrees, the system will alarm as temperatures higher than this can result in catalyst degradation and possible destruction of the honeycomb material. Testing on the 20v4000 indicates

we can run at 10% load and dose Urea to reduce NOx. We believe this would happen in under 20 minutes with most conditions having dosing start in less than 15 minutes.

The DPF will reduce PM at all times but should be regenerated when one of the following conditions is met:

- After back pressure readings have reached the maximum allowable backpressure per manufacturers specifications (27" W.C.)
- After 24 idle cold starts of 30-minutes or less and no regeneration has been performed between the cold starts.
- After operation below the recommended regeneration temperature of 300°C for a consecutive period of 720-minutes

Regeneration is accomplished by bringing the engine load level required to achieve a minimum 300°C exhaust gas temperature at the filter inlet and holding for a minimum period of 30-minutes. In testing with the 20v4000 the filters should regen at 10% load unless ambient temperatures are extremely low.

Should the soot loading reach a high level before cold start maximum is reached, the DPF differential pressure sensor will read a high backpressure and the system will alarm. Should the system reach 24 cold starts without reaching the maximum backpressure, the system will alarm and alert the user for the need to regenerate the DPF elements.

14. Can the vendor provide a document of stack test data?

Stack test data (except for particulate and ammonia) are attached for NOx, CO, & HC at 100%, 75%, 50%, 25%, and 10% loads. Final stack test results for ammonia and particulate are expected to be available next week and completed results will be forwarded as soon as they are received.



Memorandum

Date: July 11, 2012

To: Greg Flibbert and Robert Koster, Dept. of Ecology Eastern Regional Office

cc: Mike Duffy, Vantage Data Centers

From: Jim Wilder, P.E.

Subject: **Top-Down BACT Assessment
Vantage-Quincy Data Center, Quincy, WA**

Introduction

This top-down Best Available Control Technology (BACT) assessment for the Vantage-Quincy Data Center was conducted at the request of Department of Ecology, to supplement the BACT calculations that were submitted with the May 29, 2012 Notice of Construction permit application package. The BACT calculations in the permit application package were limited to evaluating only Vantage's proposed AirClarity emission control system that includes a catalyzed diesel particulate filter (DPF) and a urea-based selective catalytic reduction system (SCR). Ecology requested the supplemental top-down BACT assessment to evaluate the full range of commercially available control technologies. Note, Vantage's proposed AirClarity emission control system is more efficient than any other emission control technology that has been considered for use on data centers in Washington state.

Summary and Conclusion

The proposed diesel engines will emit the following regulated pollutants which are subject to BACT review: nitrogen oxides (NO_x), carbon monoxide (CO), volatile organic compounds (VOCs), particulate matter (PM, PM₁₀ and PM_{2.5}) and sulfur dioxide.

Generators equipped with EPA Tier-2 certified engines were considered the base case for the BACT assessment. The following add-on technologies were considered for the top-down BACT assessment:

- AirClarity System (Catalyzed DPF and SCR) proposed by Vantage
- Catalyzed Diesel Particulate Filter
- Urea-Selective Catalytic Reduction
- Three-Way Catalyst

- Diesel Oxidation Catalyst

All of the add-on technologies are technically feasible. They are commercially available, and offer substantial pollutant removal efficiencies. None of them would pose unreasonable operational difficulties.

However, all of the add-on technologies failed the cost-effectiveness criteria, for the individual pollutants and for the multi-pollutant reasonableness test. The cost-effectiveness values for each technology are listed in Table 1.

Table 1. Comparison of Cost-Effectiveness Evaluations

| Control Device | Cost-Effectiveness (\$/ton) | | | | |
|---|-----------------------------|-------------|-----------|-------------|---------------------|
| | NOX | Total PM | CO | VOC | Combined Pollutants |
| MTU AirClarity System (Catalyzed DPF + SCR) proposed by Vantage | \$81,000 | \$700,000 | \$434,000 | \$1,645,000 | \$60,000 |
| Catalyzed DPF Alone | Ineffective | \$252,000 | \$152,000 | \$578,000 | \$81,000 |
| SCR Alone | \$40,300 | \$1,519,000 | \$216,000 | \$820,000 | \$32,000 |
| 3-Way Catalyst | \$37,500 | \$125,000 | \$71,000 | \$296,000 | \$19,200 |
| Diesel Oxidation Catalyst | Ineffective | \$310,000 | \$55,000 | \$314,000 | \$41,000 |
| Ecology Cost-Effectiveness Criterion | \$10,000 | \$23,200 | \$5,000 | \$10,000 | N/A |

Because all of the add-on technologies failed the cost-effectiveness criterion, ICF recommends that none of them should be defined as BACT. Instead, ICF recommends that BACT for each pollutant should be defined as use of EPA Tier-2 certified engines, with diligent annual operation and maintenance requirements required under New Source Performance Standards Subpart IIII.

Methodology

Emission Estimation Methods (Nominal-Controlled Emission Rates)

The AERMOD modeling used for NAAQS compliance and risk assessments for Vantage’s permit application used the vendor-guaranteed, “not-to-exceed” (NTE) load-specific controlled emission rates as the starting point for the emission calculations. Vantage’s equipment contractor is ELM Energy, LLC. ELM’s vendor guaranteed NTE controlled emission rates apply to each individual engine at each load.

However, for this BACT assessment Ecology directed ICF to use emission rates that are fundamentally different from ELM’s vendor-guaranteed controlled rates used for Vantage’s AERMOD modeling. For this BACT assessment Ecology directed ICF to forecast the uncontrolled emissions by using ELM’s “nominal uncontrolled” rates. These estimated uncontrolled rates, which were provided by ELM, represent ELM’s judgment of the likely overall average emission rates for the overall population of generators manufactured by MTU. They do not apply to any individual generator, and they are called “nominal” because they are not guaranteed by ELM or MTU. ELM’s “nominal-uncontrolled” emission rates are listed in Table 1. Note, the listed values for particulate matter include ICF’s adjustment factors to account for the total particulate including both the “front half” and the “back half” (FH+BH).

Table 1. ELM Energy Nominal Uncontrolled Emission Rates (lbs/hr)

| Load | NOX | Total PM (FH+BH) | CO | VOC |
|-------|------|------------------|-----|-----|
| 10% | 6.0 | 1.45 | 2.8 | 1.2 |
| 81.3% | 37.2 | 2.55 | 5.3 | 1.1 |
| 90% | 43.6 | 2.92 | 6.0 | 1.1 |
| 93.3% | 46.1 | 3.04 | 6.3 | 1.1 |
| 100% | 51.5 | 3.24 | 6.8 | 1.1 |

The load-specific “nominal-uncontrolled” rates were adjusted upward by applying the cold-start factors that were also used for Vantage’s permit application package. The overall cold-start adjusted uncontrolled emission rates, expressed as pounds per hour at each generator load, are presented in Attachment A.

To forecast the hourly controlled emission rates at each generator load, Ecology directed ICF to calculate the “nominal-controlled” rates by multiplying the “nominal uncontrolled” rate times the removal efficiency provided by the control device being considered. The vendor-supplied removal efficiencies for each of the control devices considered are listed in Table 2.

Table 2. Vendor-Provided Steady-State Pollutant Removal Efficiencies for Commercially Available Control Devices

| Pollutant | MTU AirClarity System Proposed by Vantage (Catalyzed DPF + Urea SCR) | Clean Air Systems Catalyzed DPF | Clean Air Systems Urea SCR NOX System Incl. DOC | Clean Emission Products 3-Way Catalyst | MiraTech Diesel Oxidation Catalyst |
|------------|--|---------------------------------|---|--|------------------------------------|
| NOx | 90% | 0% | 90% | 35% | 0% |
| PM (FH+BH) | 87% | 85% | 20% | 88% | 25% |
| CO | 90% | 90% | 90% | 99% | 90% |
| VOC | 90% | 90% | 90% | 90% | 60% |

Most of the control devices considered for this BACT assessment use a metal catalyst to destroy the pollutants. After a cold start, these catalysts temporarily remain inactive until the hot flue gas heats the catalyst up to its minimum operating temperature. To account for this temporary cold-start delay, an additional cold-start catalyst delay factor was applied to each control device. The cold-start catalyst delay factors for each control device are calculated in Attachments B-F.

After the load-specific, cold-start “nominal-controlled” emission rates were calculated for each control device, the facility-wide “nominal-uncontrolled” and “nominal-controlled” emission rates were calculated by applying the hourly emission rates to the runtime hours presented in Vantage’s permit application. The runtime hours considered for the BACT assessment included scheduled testing, corrective maintenance, storm avoidance, and unplanned power outages. The annual-average runtime hours for initial commissioning tests and for periodic stack emission testing were not included in the BACT assessment. The facility-wide “nominal-uncontrolled” emission rates are calculated in Attachment A. The facility-wide “nominal-controlled” emission rates for each control device are calculated in Attachments B-F.

Cost Estimating Methods

Cost spreadsheets for each category of control device considered for this BACT assessment are provided in Attachments B-F. The methods used to calculate the total capital investment (TCI) for each type of control device were as follows:

- For each control device other than DOCs, the purchase price listed as “Freight on Board (FOB)” at the manufacturer’s facility was provided. For DOCs, the Department of Information Services (DIS) provided a tally of the total installed cost at their Olympia data center.
- In some cases ICF used FOB purchase price information for control devices designed for either 2,000 kWe or 2,500 kWe generators at other data centers, rather than the 3,000 kWe generators at the Vantage Data Center. In those cases, ICF adjusted the FOB purchase price upward using the “0.6 rule”.
- Cost factors for indirect installation costs (shipping, installation, design fees, etc.) were derived from EPA’s guidance manual [EPA Pollution Control Cost Manual](#), January 2002. The cost factors from Section 4.2 Chapter 1, Selective Catalytic Reduction, were used.
- Annual capital recovery cost was based on an assumed 25-year equipment life, with a conservatively low discount rate of 4%.
- Indirect annual costs (overhead, insurance, and taxes) were calculated by cost factors from EPA’s control cost guidance manual listed above.

- For this screening-level analysis it was assumed that none of the control devices would incur annual costs for operation and maintenance. This results in a conservatively low estimate of the control device capital cost, annual cost, and cost-effectiveness.
- The Total Annual Cost for each control device was calculated by summing the estimate annual costs for capital recovery, direct operation and maintenance, and indirect annual costs.

Cost-Effectiveness Criteria for Individual Pollutants

For the individual pollutants, the individual pollutant cost-effectiveness was calculated by dividing the total annual cost (\$/year) by the tons of facility-wide pollutant removed by the control device. The derived cost-effectiveness was then compared to the following cost-effectiveness criteria values, which were developed by Ecology for the Sabey-Intergate-Quincy data center's air quality permit:

NOx: \$10,000/ton

Total PM (FH+BH): \$23,200/ton

CO: \$5,000/ton

VOC: no value listed. Assumed to be \$10,000/ton (same as NOx)

Reasonableness Cost Effectiveness for Multi-Pollutant Analyses

All of the control devices considered for this BACT assessment are at least marginally effective at controlling the entire range of pollutants. The manufacturer-provided removal efficiencies range from a low of 25% for PM removed by DOCs, to as high as 99.9% for CO removed by 3-Way Catalysts.

To account for the variable reduction efficiencies for the various pollutants, for each control device the multi-pollutant cost effectiveness was evaluated by comparing two facility-wide cost parameters: the actual total annual cost to own and operate the control device being considered; and the "reasonable annual control cost for combined pollutants". The evaluation is done using a three-step process:

- The "reasonable annual cost" for each individual pollutant is calculated by multiplying the annual tons/year of that pollutant removed by the control device times the Ecology cost-effectiveness criterion for that pollutant.
- The facility-wide "total reasonable annual cost" is calculated by summing the calculated values for each individual pollutant.
- The "total reasonable annual cost" is then compared to the actual total annual cost. If the actual annual cost is less than the "total reasonable annual cost" then the cost for multi-pollutant treatment is considered "reasonable" and the control device satisfies the BACT cost-effectiveness criterion. However, if the actual annual cost exceeds the "total reasonable annual cost" then the cost for multi-pollutant treatment is considered "non-reasonable" and the control device fails the BACT cost-effectiveness criterion.

Identification of Technically Feasible Control Technologies

Since 2007 Ecology and other Washington state agencies have issued air quality permits for the following data centers that use large diesel emergency generators: Sabey-Intergate-Quincy; Dell-Quincy; Yahoo-Quincy; Microsoft-Quincy; Intuit-Quincy; Titan-Moses Lake; Dept. of Information Services (DIS) Data Center –Olympia; Sabey-Intergate-Wenatchee; and T-Mobile-Wenatchee. ICF reviewed Ecology’s BACT determinations for these existing data centers, and developed the following list of technically feasible emission controls applicable for diesel generators:

- EPA Tier-2 certified engines with combustion controls including timing retard, exhaust gas cooling, exhaust gas recirculation, and turbocharging. This technology is considered the base case for the BACT assessment.
- Vantage’s proposed AirClarity system (catalyzed Diesel Particulate Filter plus Urea-based Selective Catalytic Reduction). Technical information, emission estimates, cost data, and cost-effectiveness calculations are provided in Attachment B.
- Catalyzed Diesel Particulate Filter by itself (technical information in Attachment C).
- Urea-Selective Catalytic Reduction by itself (technical information in Attachment D).
- Three-Way Catalyst (also known as Two-Stage Catalyst). Technical information is provided in Attachment E.
- Diesel Oxidation Catalyst (see Attachment F).

BACT Analysis for NOx

Vantage’s Proposed AirClarity System (Urea-Based SCR Plus Catalyzed DPF)

ELM energy has contracted with Vantage to install MTU’s AirClarity emission control system on each generator. Technical information is provided in Attachment B. The AirClarity system consists of a modular system including a catalyzed DPF and a urea-based SCR.

The SCR system evaluated for this analysis is the Clean Air Systems package. Technical information is provided in Attachment C. The SCR system functions by injecting a liquid reducing agent, such as urea, through a catalyst into the exhaust stream of the diesel engine. The urea reacts with the exhaust stream converting nitrogen oxides into nitrogen and water. The use of a lean ultralow sulfur fuel is required to achieve good NOx destruction efficiencies. SCR can reduce NOx emissions by up to 90-95 percent while simultaneously reducing hydrocarbon (VOC), CO and PM emissions.

For SCR systems to function effectively, exhaust temperatures must be high enough (about 200 to 500 degrees C) to enable catalyst activation. For this reason, SCR control efficiencies are expected to be

relatively low during the first 10 to 20 minutes after engine start up, especially during maintenance, and testing loads. There are also complications of managing and controlling the excess ammonia (ammonia slip) from SCR use. However, Vantage accounted for ammonia slip in its permit application and demonstrated the small amount of ammonia emissions would not cause ambient concentrations beyond the facility boundary to exceed the ASIL for ammonia. Because backup engines typically experience long inactive periods between operations, the facility must conduct diligent inspection and maintenance of the urea storage and injection system to ensure that urea crystallization inside reagent distribution lines does not interfere with the SCR system.

ELM has provided vendor-guaranteed removal efficiencies for the AirClarity system as follows: NOx = 90%; CO and VOC = 90%; and total PM (front-half plus back-half) = 87%. The AirClarity system provides substantial removal efficiencies for all key pollutants. The system is reliable, and would pose not substantial operating constraints. Therefore, the AirClarity system is considered a technically feasible add-on technology.

However, Vantage’s proposed AirClarity system failed the cost-effectiveness evaluation. ICF evaluated the cost effectiveness of installing and operating AirClarity systems on the proposed Vantage diesel engines. Emission calculations and cost-effectiveness calculations for an AirClarity system installed on the Vantage generators are provided in Attachment B. The individual-pollutant cost-effectiveness for NOx, PM, CO and VOC is presented in Table AC-1 below. The analysis indicates that the use of the AirClarity systems would cost approximately \$700,000 per ton of PM removed from the exhaust stream based on Vantage’s permitted annual runtime scenario including power outage of eight (8) hours per year. A previous survey by Ecology found that the permitting agencies surveyed have required installation of NOx controls as BACT with expected operational costs ranging from \$143 to \$9,473 per ton of NOx removed, and Ecology has set the NOx cost-effectiveness criterion at \$10,000 per ton. Therefore, the AirClarity system fails the cost-effectiveness test on an individual pollutant basis.

Table AC-1. AirClarity System, Individual Pollutants Removal Tonnages (Nominal-Controlled)

| Pollutant | PM (FH+BH) | CO | VOC | NOX |
|--------------------------------------|------------|-----------|-------------|-----------|
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 0.203 | 0.958 | 0.293 | 4.38 |
| Tons Removed/Year | 1.36 | 2.19 | 0.578 | 11.8 |
| Overall Cold-Start Removal Effcy | 87% | 70% | 66% | 73% |
| Annualized Cost (\$/yr) | \$950,466 | \$950,466 | \$950,466 | \$950,466 |
| Individual Pollutant \$/Ton Removed | \$700,039 | \$433,611 | \$1,644,950 | \$80,819 |
| Ecology Cost-Effectiveness Threshold | \$23,200 | \$5,000 | \$10,000 | \$10,000 |
| Pass or Fail? | Fail | Fail | Fail | Fail |

The AirClarity system would also provide substantial removal efficiencies for PM, CO and VOC, as well as for NOx. However, the AirClarity system failed the multi-pollutant cost effectiveness evaluation. Table AC-2 below shows the multi-pollutant evaluation. The actual annual cost to own and operate the AirClarity system would be \$950,000 per year, which far exceeds the “Total

Reasonable Annual Cost” of \$166,000 per year based on Ecology’s cost criteria for the individual pollutants.

Table AC-2. AirClarity System: Multi-Pollutant Cost-Effectiveness for Reasonable Control Cost vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Reasonable Annual Cost (\$/year) | |
|---|---------------------------------------|----------------------------|---|-----------------|
| NOX | \$10,000 | 11.76 | \$117,604 | per year |
| CO | \$5,000 | 2.19 | \$10,960 | per year |
| VOC | \$9,999 | 0.58 | \$5,778 | per year |
| PM (FH+BH) | \$23,200 | 1.36 | \$31,499 | per year |
| Total Reasonable Annual Control Cost for Combined Pollutants | | | \$165,841 | per year |
| Actual Annual Control Cost | | | \$950,466 | per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Reasonable) | |

ICF concludes that while Vantage’s proposed AirClarity system is a potentially-feasible emission control technology for diesel engines, it is not economically feasible under BACT. Therefore, ICF recommends that Ecology should reject this control option as BACT.

Selective Catalytic Reduction (SCR) By Itself (See Attachment D for details)

The SCR system evaluated for this analysis is the Clean Air Systems package that was originally evaluated by Sabey for the BACT analysis for their Intergate-Quincy data center. Technical information is provided in Attachment D. The Clean Air Systems package includes a urea-based SCR and a diesel oxidation catalyst, to provide substantial removal efficiencies for NOx, CO and VOC. The Clean Air Systems package does not include a DPF, so it provides only marginal removal efficiency for PM (20% estimated efficiency).

The SCR system functions by injecting a liquid reducing agent, such as urea, through a catalyst into the exhaust stream of the diesel engine. The urea reacts with the exhaust stream converting nitrogen oxides into nitrogen and water. The use of a lean ultralow sulfur fuel is required to achieve good NOx destruction efficiencies. SCR can reduce NOx emissions by up to 90-95 percent while simultaneously reducing hydrocarbon (VOC), CO and PM emissions.

For SCR systems to function effectively, exhaust temperatures must be high enough (about 200 to 500 degrees C) to enable catalyst activation. For this reason, SCR control efficiencies are expected to be relatively low during the first 10 to 20 minutes after engine start up, especially during maintenance, and testing loads. There are also complications of managing and controlling the excess ammonia (ammonia slip) from SCR use. However, Vantage accounted for ammonia slip in its permit application and demonstrated the small amount of ammonia emissions would not cause ambient concentrations beyond the facility boundary to exceed the ASIL for ammonia. Because backup engines typically experience

long inactive periods between operations, the facility must conduct diligent inspection and maintenance of the urea storage and injection system to ensure that urea crystallization inside reagent distribution lines does not interfere with the SCR system.

Based on these considerations, ICF concludes SCR is a technically feasible add-on technology for NOx, PM, VOC and CO control.

However, SCR failed the cost-effectiveness evaluation. ICF evaluated the cost effectiveness of installing and operating SCR systems on the proposed diesel engines. Emission calculations and cost-effectiveness calculations for an SCR system installed on the Vantage generators are provided in Attachment D. The individual-pollutant cost-effectiveness for NOx, PM, CO and VOC is presented in Table SCR-1 below. The analysis indicates that the use of SCR systems would cost approximately \$40,300 per ton of NOx removed from the exhaust stream based on Vantage’s worst-case annual runtime scenario including power outage of eight (8) hours per year. A previous survey by Ecology found that the permitting agencies surveyed have required installation of NOx controls as BACT with expected operational costs ranging from \$143 to \$9,473 per ton of NOx removed, and Ecology has set the NOx cost-effectiveness criterion at \$10,000 per ton.

Table SCR-1. Urea-SCR, Individual Pollutant Removal Tonnages (Nominal-Controlled)

| Pollutant | PM (FH+BH) | CO | VOC | NOX |
|--------------------------------------|-------------------|-----------|------------|------------|
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 1.248 | 0.958 | 0.293 | 4.38 |
| Tons Removed/Year | 0.31 | 2.19 | 0.578 | 11.8 |
| Overall Cold-Start Removal Effcy | 20% | 70% | 66% | 73% |
| Annual Cost (\$/yr) | \$473,994 | \$473,994 | \$473,994 | \$473,994 |
| Individual Pollutant \$/Ton Removed | \$1,518,616 | \$216,240 | \$820,331 | \$40,304 |
| Ecology Cost-Effectiveness Threshold | \$23,200 | \$5,000 | \$10,000 | \$10,000 |
| Pass or Fail? | Fail | Fail | Fail | Fail |

A typical SCR system would also provide substantial removal efficiencies for PM, CO and VOC, as well as for NOx. However, the SCR failed the multi-pollutant cost effectiveness evaluation. Table SCR-2 below shows the multi-pollutant evaluation. The actual annual cost to own and operate the SCR would be \$473,000 per year, which far exceeds the “Total Reasonable Annual Cost” of \$142,000 per year based on Ecology’s cost criteria for the individual pollutants.

Table SCR-2. Urea-SCR Multi-Pollutant Cost-Effectiveness for "Reasonable Control Cost" vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Reasonable Annual Cost (\$/year) | |
|---|---------------------------------------|----------------------------|---|-----------------|
| NOX | \$10,000 | 11.76 | \$117,604 | per year |
| CO | \$5,000 | 2.19 | \$10,960 | per year |
| VOC | \$9,999 | 0.58 | \$5,778 | per year |
| PM (FH+BH) | \$23,200 | 0.31 | \$7,241 | per year |
| Total Reasonable Annual Control Cost for Combined Pollutants | | | \$141,583 | per year |
| Actual Annual Control Cost | | | \$473,994 | per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Reasonable) | |

ICF concludes that while SCR is a demonstrated emission control technology for emergency diesel generators, it is not economically feasible for this project. Therefore, ICF recommends that Ecology should reject this NOx control option as BACT.

3-Way Catalyst (Two-Stage Catalyst)

For this BACT assessment, ICF considered the Clean Emission Products 3-Way Catalyst system that was permitted for the Titan Data Center in Moses Lake, WA. Technical specifications, removal efficiency data, emission calculations, and cost-effectiveness calculations are provided in Attachment E.

Based on the experience at the Titan Data Center, ICF concludes it is possible that 2-stage oxidation catalysts ("3-way" catalysts) might be able to be designed to provide some marginal NOx emission reductions from modern emergency generators. The Clean Emission Products system proposed by R S Titan Lotus, LLC and approved by Ecology is specially designed to remove up to 35% of NOx emissions, as well as considerable quantities of diesel particulate, CO and VOC emissions. The system reviewed by Ecology is a single-pass system that can be installed without retrofitting closed-loop systems such as Exhaust Gas Recirculation. Each catalyst system uses a stainless steel honeycomb mesh catalyst element coated with three catalysts: cerium washcoat; platinum (Pt) and rhodium (Rh) catalyst coatings.

The 2-stage oxidation catalysts first oxidize CO and VOC while removing oxygen from the gas stream, then the remaining rich-burn environment reacts with the Rh catalyst to chemically convert the NO and NO2 in the exhaust stream to nitrogen. The system achieves the required low-oxygen environment by using a specialized catalyst coating and cell structure to remove oxygen molecules from the diesel exhaust stream. Exhaust temperature must be at least 250°C and not exceed 750°C for the system to be effective.

Although 2-stage oxidation catalyst systems appear to have been commercially deployed for standby diesel engine applications in Europe, Australia and Canada, Ecology is unaware of specific applications within the United States. The Titan Data Center (Moses Lake, Washington) has proposed to use two 35” diameter x 3.5” thick 3-way catalysts within one stainless steel housing for their planned expansion. The manufacturer of that catalyst system (Clean Emissions Products, Inc.) guaranteed a NOx reduction of not less than 35% although their website and a company salesman both claim that their 2-stage catalysts are capable of reducing up to 99% of CO, 70% of NOx and 90% of diesel particulate. The catalysts proposed by the Titan Data Center are also expected to reduce at least 90% of VOC. Clean Emission Products’ limited test data have reported about 43% NOx reduction and about 88% diesel particulate reduction. However, Clean Emission Products have been unable to provide any test data for a lean-burn Tier-2 diesel engine such as those proposed at Vantage. As of this writing, the diesel generators at the Titan Data Center have not been installed, so no compliance test data are available for that facility.

Regardless, based on Clean Emission Products’ vendor-guaranteed contract with Titan Data Center, ICF concludes 3-Way Catalysts appear to be a technically-feasible add-on technology to provide marginal NOx reduction on diesel generators.

However, 3-Way Catalysts failed the cost-effectiveness evaluation. ICF evaluated the cost effectiveness of installing and operating 3-Way Catalyst systems on the proposed Vantage diesel engines. Emission calculations and cost-effectiveness calculations for an SCR system installed on the Vantage generators are provided in Attachment E. The individual-pollutant cost-effectiveness for NOx, PM, CO and VOC is presented in Table 3WC-1 below. The analysis indicates that the use of 3-Way Catalyst systems would cost approximately \$37,457 per ton of NOx removed from the exhaust stream based on Vantage’s worst-case annual runtime scenario including power outage of eight (8) hours per year. A previous survey by Ecology found that the permitting agencies surveyed have required installation of NOx controls as BACT with expected operational costs ranging from \$143 to \$9,473 per ton of NOx removed, and Ecology has set the NOx cost-effectiveness criterion at \$10,000 per ton. Therefore, the 3-Way Catalyst fails the cost-effectiveness test on an individual pollutant basis.

Table 3WC-1. Three-Way Catalyst Individual Pollutant Removal Tonnages (Nominal-Controlled)

| Pollutant | PM (FH+BH) | CO | VOC | NOX |
|--------------------------------------|-------------------|-----------|------------|------------|
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 0.187 | 0.739 | 0.293 | 11.57 |
| Tons Removed/Year | 1.37 | 2.41 | 0.578 | 4.6 |
| Overall Cold-Start Removal Effic | 88% | 77% | 66% | 28% |
| Annual Cost (\$/year) | \$171,311 | \$171,311 | \$171,311 | \$171,311 |
| Individual Pollutant \$/Ton Removed | \$124,740 | \$71,049 | \$296,484 | \$37,457 |
| Ecology Cost-Effectiveness Threshold | \$23,200 | \$5,000 | \$10,000 | \$10,000 |
| Pass or Fail? | Fail | Fail | Fail | Fail |

A typical 3-Way Catalyst system would also provide substantial removal efficiencies for PM, CO and VOC, as well as for NOx. However, the 3-Way Catalyst failed the multi-pollutant cost effectiveness evaluation. Table 3WC-2 below shows the multi-pollutant evaluation. The actual annual cost to own

and operate the 3-Way Catalyst would be \$171,000 per year, which exceeds the “Total Reasonable Annual Cost” of \$95,000 per year based on Ecology’s cost criteria for the individual pollutants.

Table 3WC-2. Three-Way Catalyst, Multi-Pollutant Cost-Effectiveness for "Reasonable Control Cost" vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Reasonable Annual Cost (\$/year) | |
|---|--|-----------------------------------|--|-----------------|
| NOX | \$10,000 | 4.57 | \$45,735 | per year |
| CO | \$5,000 | 2.41 | \$12,056 | per year |
| VOC | \$9,999 | 0.58 | \$5,778 | per year |
| PM (FH+BH) | \$23,200 | 1.37 | \$31,861 | per year |
| Total Reasonable Annual Control Cost for Combined Pollutants | | | \$95,430 | per year |
| Actual Annual Control Cost | | | \$171,311 | per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Reasonable) | |

ICF concludes that while 3-Way Catalysts are a potentially-feasible emission control technology for diesel engines, it is not economically feasible for this project. Therefore, ICF recommends that Ecology should reject this NOx control option as BACT.

NOx Adsorbers (Experimental Technology)

The use of NOx adsorbers (sometimes called lean NOx traps) is a catalytic method being developed and tested by diesel engine manufacturers to reduce NOx emissions, primarily from mobile sources. The NOx adsorber contains a catalyst (e.g., zeolite or platinum) that is used to “trap” NOx (NO and NO2) molecules found in the exhaust. NOx adsorbers can achieve NOx reductions greater than 90% at typical steady-state exhaust gas temperatures.

However, as of this writing, NOx adsorbers are experimental technology and are, therefore, very expensive. Additionally, a literature search did not reveal any indication that this technology is commercially available for stationary backup generators. Thus, ICF recommends that Ecology should reject NOx adsorbers as BACT for the proposed diesel engines.

Combustion Controls and Tier-2 Compliance

Diesel engine manufacturers typically use proprietary combustion control methods to achieve the emission reductions needed to meet applicable EPA Tier-2 standards. Common controls include fuel injection timing retard and exhaust gas recirculation. Injection timing retard reduces the peak flame temperature and NOx emissions, but may lead to higher fuel consumption.

Vantage will install generators equipped with MTU engines that will use a combination of combustion control methods, including fuel injection timing retard, to comply with EPA Tier-2 emission limits.

This is the only technology that provides substantial emission reductions while also satisfying cost-effectiveness criteria. ICF recommends that Ecology should require this technology as BACT for NO_x.

BACT Analysis for Combined Particulate Matter, Carbon Monoxide, and Volatile Organic Compounds

Vantage's Proposed AirClarity System (Catalyzed DPF Plus SCR)

The MTU AirClarity emission control system proposed by Vantage consists of a modular system including a catalyzed DPF and a urea-based SCR. ELM energy has provided vendor guaranteed removal efficiencies of 87% for total PM (front-half plus back-half), and 90% for NO_x, CO and VOC. Technical specifications, emission estimates, and cost-effectiveness calculations are provided in Attachment B. The AirClarity system provides substantial removal efficiencies for all key pollutants. The system is reliable, and would pose not substantial operating constraints. Therefore, the AirClarity system is considered a technically feasible add-on technology.

However, Vantage's proposed AirClarity system failed the cost-effectiveness evaluation. ICF evaluated the cost effectiveness of installing and operating AirClarity systems on the proposed Vantage diesel engines. Emission calculations and cost-effectiveness calculations for an AirClarity system installed on the Vantage generators are provided in Attachment B. The individual-pollutant cost-effectiveness for NO_x, PM, CO and VOC is presented in Table AC-1 below. The analysis indicates that the use of the AirClarity systems would cost approximately \$700,000 per ton of PM removed from the exhaust stream based on Vantage's worst-case annual runtime scenario including power outage of eight (8) hours per year.

For PM, a previous survey by Ecology found that none of the permitting agencies surveyed had required installation of a particulate matter control device (as BACT) that was expected to cost more than \$23,200 per ton of particulate removed. Therefore, Ecology has specified the PM cost-effectiveness criterion of \$23,200 per ton.

For CO, a previous survey by Ecology found that the permitting agencies surveyed have required installation of carbon monoxide controls as BACT on other types of emission units, with expected operational costs ranging from \$300 to \$9,795 per ton of carbon monoxide removed. The upper level of that range is suspect and it is possible that that number actually reflects California BACT which is typically equivalent to a Lowest Achievable Emissions Rate (LAER) limit. In Washington, costs for controlling CO from combined cycle natural gas electric generating facilities are usually in the \$3,500 to \$5,000 range. Therefore, Ecology has specified a BACT cost-effectiveness criterion of \$5,000 per ton removed for CO.

A previous survey by Ecology found that the permitting agencies surveyed have required installation of NO_x controls as BACT with expected operational costs ranging from \$143 to \$9,473 per ton of NO_x removed, and Ecology has set the NO_x cost-effectiveness criterion at \$10,000 per ton.

Ecology has not set a BACT cost-effectiveness criterion for VOC. For this BACT assessment, ICF assumed the VOC cost-effectiveness threshold is the same as for NOx, because both pollutants are ozone precursors. Therefore, the VOC criterion was assumed to be \$10,000 per ton.

As listed in Table AC-1 below, the calculated cost-effectiveness values for each individual pollutant controlled by the AirClarity system far exceed their respective Ecology criteria. Therefore, the AirClarity system fails the cost-effectiveness test on an individual pollutant basis.

Table AC-1. AirClarity System, Individual Pollutants Removal Tonnages (Nominal-Controlled)

| Pollutant | PM (FH+BH) | CO | VOC | NOX |
|--------------------------------------|------------|-----------|-------------|-----------|
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 0.203 | 0.958 | 0.293 | 4.38 |
| Tons Removed/Year | 1.36 | 2.19 | 0.578 | 11.8 |
| Overall Cold-Start Removal Effcy | 87% | 70% | 66% | 73% |
| Annualized Cost (\$/yr) | \$950,466 | \$950,466 | \$950,466 | \$950,466 |
| Individual Pollutant \$/Ton Removed | \$700,039 | \$433,611 | \$1,644,950 | \$80,819 |
| Ecology Cost-Effectiveness Threshold | \$23,200 | \$5,000 | \$10,000 | \$10,000 |
| Pass or Fail? | Fail | Fail | Fail | Fail |

The AirClarity system would also provide substantial removal efficiencies for PM, CO and VOC, as well as for NOx. However, the AirClarity system failed the multi-pollutant cost effectiveness evaluation. Table AC-2 below shows the multi-pollutant evaluation. The actual annual cost to own and operate the AirClarity system would be \$950,000 per year, which far exceeds the “Total Reasonable Annual Cost” of \$166,000 per year based on Ecology’s cost criteria for the individual pollutants.

Table AC-2. AirClarity System: Multi-Pollutant Cost-Effectiveness for Reasonable Control Cost vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Reasonable Annual Cost (\$/year) |
|---|---------------------------------------|----------------------------|---|
| NOX | \$10,000 | 11.76 | \$117,604 per year |
| CO | \$5,000 | 2.19 | \$10,960 per year |
| VOC | \$9,999 | 0.58 | \$5,778 per year |
| PM (FH+BH) | \$23,200 | 1.36 | \$31,499 per year |
| Total Reasonable Annual Control Cost for Combined Pollutants | | | \$165,841 per year |
| Actual Annual Control Cost | | | \$950,466 per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Reasonable) |

ICF concludes that while Vantage’s proposed AirClarity system is a potentially-feasible emission control technology for diesel engines, it is not economically feasible under BACT. Therefore, ICF recommends that Ecology should reject this control option as BACT.

Catalyzed Diesel Particulate Filters (DPFs)

For this BACT assessment, ICF evaluated the Clean Air Systems catalyzed DPFs that were originally considered for the Sabey-Intergate-Quincy data center. Technical specifications, emission estimates, and cost-effectiveness calculations are provided in Attachment C.

The Clean Air Systems catalyzed DPF package includes their PERMIT DPF plus their ASSURE diesel oxidation catalyst. Clean Air Systems estimated 85% removal efficiency for PM, and 90% removal efficiency for CO and VOC. The DPF-DOC system would not remove any NOx.

The catalyzed DPF system would be reliable, and would pose no substantial operating constraints for the generators. There is one identified problem with the catalyzed DPF system. Field tests on a DOC conducted by Microsoft on one of their diesel generators showed that DOCs can convert some of the non-toxic nitric oxide (NO) in the exhaust stream to highly-toxic nitrogen dioxide (NO₂). At this time it is uncertain whether the increased emissions of toxic NO₂ might pose human health concerns at receptors beyond the facility.

Regardless of that potential issue, ICF concludes that catalyzed DPFs would be a reliable and efficient system to reduce the emissions of PM, CO and VOC. Therefore, ICF concludes that catalyzed DPFs, by themselves, would be a technically feasible add-on control technology.

However, catalyzed DPFs failed the cost-effectiveness evaluation. ICF evaluated the cost effectiveness of installing and operating 3-Way Catalyst systems on the proposed Vantage diesel engines. Emission calculations and cost-effectiveness calculations for a catalyzed DPF system installed on the Vantage generators are provided in Attachment C. The individual-pollutant cost-effectiveness for NOx, PM, CO and VOC is presented in Table DPF-1 below. The analysis indicates that the use of a catalyzed DPF systems would cost approximately \$252,000 per ton of PM removed from the exhaust stream based on Vantage's worst-case annual runtime scenario including power outage of eight (8) hours per year.

As described previously, Ecology has set BACT cost-effectiveness thresholds for the individual pollutants at the values listed below in Table DPF-1. For each individual pollutant the forecast actual cost far exceeds Ecology's BACT cost-effectiveness criterion. Therefore, the catalyzed DPFs fails the cost-effectiveness test on an individual pollutant basis.

Table DPF-1. Catalyzed DPF, Individual Pollutant Removal Tonnages (Nominal-Controlled)

| Pollutant | PM (FH+BH) | CO | VOC | NOX |
|--------------------------------------|------------|-----------|-----------|-----------|
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 0.234 | 0.958 | 0.293 | 16.14 |
| Tons Removed/Year | 1.33 | 2.19 | 0.578 | 0.0 |
| Overall Cold-Start Removal Effcy | 85% | 70% | 66% | 0% |
| Annual Cost (\$/year) | \$333,734 | \$333,734 | \$333,734 | \$333,734 |
| Individual Pollutant \$/Ton Removed | \$251,586 | \$152,252 | \$577,585 | N/A |
| Ecology Cost-Effectiveness Threshold | \$23,200 | \$5,000 | \$10,000 | \$10,000 |
| Pass or Fail? | Fail | Fail | Fail | Fail |

A typical catalyzed DPF system would also provide substantial removal efficiencies for CO and VOC, as well as for PM. However, the DPF failed the multi-pollutant cost effectiveness evaluation. Table DPF-2 below shows the multi-pollutant evaluation. The actual annual cost to own and operate the DPF would be \$333,000 per year, which far exceeds the "Total Reasonable Annual Cost" of \$47,000 per year based on Ecology's cost criteria for the individual pollutants.

Table DPF-2. Catalyzed DPF, Multi-Pollutant Cost-Effectiveness for "Reasonable Control Cost" vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Reasonable Annual Cost (\$/year) | |
|---|---------------------------------------|----------------------------|---|-----------------|
| NOX | \$10,000 | 0.00 | \$0 | per year |
| CO | \$5,000 | 2.19 | \$10,960 | per year |
| VOC | \$9,999 | 0.58 | \$5,778 | per year |
| PM (FH+BH) | \$23,200 | 1.33 | \$30,775 | per year |
| Total Reasonable Annual Control Cost for Combined Pollutants | | | \$47,513 | per year |
| Actual Annual Control Cost | | | \$333,734 | per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Reasonable) | |

ICF concludes that while DPFs are a potentially-feasible emission control technology for diesel engines, it is not economically feasible under BACT. Therefore, ICF recommends that Ecology should reject this control option as BACT.

Diesel Oxidation Catalysts (see Attachment F)

For this BACT assessment ICF considered installing DOCs by themselves. That control strategy was required for the Department of Information Services (DIS) Data Center in Olympia, WA. For this assessment ICF considered the MiraTech DOC system that was installed at the DIS Data Center. Technical specifications, emission estimates, installation cost information, and cost-effectiveness

calculations are provided in Attachment F.

This method utilizes metal catalysts to oxidize carbon monoxide, particulate matter, and hydrocarbons in the diesel exhaust. Diesel oxidation catalysts (DOCs) are commercially available and reliable for controlling particulate matter, carbon monoxide and hydrocarbon emissions from diesel engines. While the primary pollutant controlled by DOCs is carbon monoxide (approximately 90% reduction), DOCs have also been demonstrated to reduce up to 25% of diesel engine exhaust particulate emissions, and up to 60% of hydrocarbon emissions.

The DOC system would be reliable. It would provide high removal efficiencies for CO and VOC, while also providing a small amount of PM removal. In general it would pose no substantial operating constraints for the generators. There is one identified problem with the catalyzed DPF system. Field tests on a DOC conducted by Microsoft on one of their diesel generators showed that DOCs can convert some of the non-toxic nitric oxide (NO) in the exhaust stream to highly-toxic nitrogen dioxide (NO₂). At this time it is uncertain whether the increased emissions of toxic NO₂ might pose human health concerns at receptors beyond the facility.

Regardless of that potential issue, ICF concludes that DOCs would be a reliable and efficient system to reduce the emissions of PM, CO and VOC. Therefore, ICF concludes that catalyzed DPFs, by themselves, would be a technically feasible add-on control technology.

However, DOCs failed the cost-effectiveness evaluation on an individual-pollutant basis and on a multi-pollutant basis. ICF evaluated the cost effectiveness of installing and operating DOC systems on the proposed Vantage diesel engines. Emission calculations and cost-effectiveness calculations for the DOC system installed on the Vantage generators are provided in Attachment F. The individual-pollutant cost-effectiveness for NO_x, PM, CO and VOC is presented in Table DOC-1 below. For each pollutant the forecast actual control cost far exceeds Ecology's cost-effectiveness criterion. Therefore, the DOC fails the cost-effectiveness test on an individual pollutant basis.

Table DOC-1. DOC Individual Pollutant Removal Tonnages (Nominal-Controlled)

| Pollutant | PM (FH+BH) | CO | VOC | NOX |
|--------------------------------------|-------------------|-----------|------------|------------|
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 1.170 | 0.958 | 0.485 | 16.14 |
| Tons Removed/Year | 0.39 | 2.19 | 0.385 | 0.0 |
| Overall Cold-Start Removal Effcy | 25% | 70% | 44% | 0% |
| Total Annual Cost (\$/year) | \$120,766 | \$120,766 | \$120,766 | \$120,766 |
| Individual Pollutant \$/Ton Removed | \$309,535 | \$55,094 | \$313,511 | N/A |
| Ecology Cost-Effectiveness Threshold | \$23,200 | \$5,000 | \$10,000 | \$10,000 |
| Pass or Fail? | Fail | Fail | Fail | Fail |

A typical DOC system would also provide some marginal efficiencies for PM, as wells as substantial removal for CO and VOC. However, the DOC failed the multi-pollutant cost effectiveness evaluation. Table DOC-2 below shows the multi-pollutant evaluation. The actual annual cost to own and operate

the DOC would be \$121,000 per year, which far exceeds the “Total Reasonable Annual Cost” of \$24,000 per year based on Ecology’s cost criteria for the individual pollutants.

Table DOC-2. DOC, Multi-Pollutant Cost-Effectiveness for "Reasonable Control Cost" vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Acceptable Annual Cost (\$/year) | |
|---|---------------------------------------|----------------------------|---|-----------------|
| NOX | \$10,000 | 0.00 | \$0 | per year |
| CO | \$5,000 | 2.19 | \$10,960 | per year |
| VOC | \$9,999 | 0.39 | \$3,852 | per year |
| PM (FH+BH) | \$23,200 | 0.39 | \$9,052 | per year |
| Total Reasonable Annual Control Cost for Combined Pollutants | | | \$23,863 | per year |
| Actual Annual Control Cost | | | \$120,766 | per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Reasonable) | |

ICF concludes that while DOCs are a potentially-feasible emission control technology for diesel engines, it is not economically feasible for this project. Therefore, ICF recommends that Ecology should reject this control option as BACT.

3-Way Catalysts (2-Stage Catalysts)

The theory and design of 2-stage diesel oxidation catalysts (i.e., diesel oxidation catalysts operating in a 3-way catalyst mode) was described previously under NO_x controls. As stated above, one manufacturer of one such commercially-available system (Clean Emission Products) claims their systems are capable of reducing up to 99% of CO, 70% of NO_x, 90% of VOC, and 90% of diesel particulate. For the Titan Data Center, Clean Emission Products issued a vendor guarantee for up to 35% NO_x removal, and also provided non-guaranteed estimates of 88% for PM, 99% for CO, and 90% for VOC.

ICF is concerned that Clean Emission Products has been unable to provide stack test performance data for use of their 3-Way Catalyst on a lean-burn, Tier-2 certified modern generator. Regardless, based on Clean Emission Products’ vendor guarantee for the Titan Data Center, ICF concludes this technology should be considered technically feasible for the Vantage Data Center.

However, ICF concludes 3-Way Catalysts are economically infeasible for the Vantage Data Center. As listed in Table 3WC-1 earlier in this memo, ICF estimates that the use of these catalysts would cost Vantage more than the following:

- \$125,000 for each ton of PM removed from the exhaust stream;
- \$71,000 for each ton of CO removed from the exhaust stream; and
- \$296,000 for each ton of VOC removed from the exhaust stream.

Ecology considers the above annual control cost estimates to be prohibitive under BACT guidelines. Ecology concludes that while specially designed 2-stage oxidation catalysts are promising and potentially effective for CO, PM and VOC control, they are not cost effective under general BACT guidelines. Therefore, ICF recommends Ecology should reject this technology as BACT for the Vantage Data Center.

Combustion Controls and Tier-2 Compliance

Diesel engine manufacturers typically use proprietary combustion control methods to achieve the emission reductions needed to meet applicable EPA Tier-2 standards. Common controls include fuel injection timing retard and exhaust gas recirculation. Injection timing retard reduces the peak flame temperature and NO_x emissions, but may lead to higher fuel consumption.

Vantage will install generators equipped with MTU engines that will use a combination of combustion control methods, including fuel injection timing retard, to comply with EPA Tier-2 emission limits. As described in Vantage's air quality permit application, Vantage will also install add-on controls consisting of the AirClarity system.

This is the only technology that provides substantial emission reductions while also satisfying cost-effectiveness criteria. ICF recommends that Ecology should require this technology as BACT for NO_x, PM, CO and VOCs.

BACT ANALYSIS FOR SULFUR DIOXIDE

ICF did not find any add-on control options commercially available and feasible for controlling sulfur dioxide emissions from diesel engines. Vantage's proposed BACT for sulfur dioxide is the use of ultra-low sulfur diesel fuel (15 ppm by weight of sulfur).

BACT Recommendation for Sulfur Dioxide. ICF recommends that BACT for sulfur dioxide is the use of ultra-low sulfur diesel fuel containing no more than 15 parts per million by weight of sulfur.

BEST AVAILABLE CONTROL TECHNOLOGY FOR AIR TOXICS

Best Available Control Technology for Toxics (tBACT) means BACT, as applied to toxic air pollutants. The procedure for determining tBACT follows the same procedure used above for determining BACT. Under state rules, tBACT is required for all toxic air pollutants for which the increase in emissions will exceed de minimis emission values as found in WAC 173-460-150.

For the proposed project, tBACT must be determined for each of the toxic air pollutants listed in Table TBACT-1 below. As illustrated by Table TBACT-1, ICF recommends that compliance with BACT, as determined above, satisfies the tBACT requirement.

Table TBACT-1. tBACT Determination

| Toxic Air Pollutant | tBACT |
|-----------------------------------|--|
| Acetaldehyde | Compliance with the VOC BACT requirement |
| Acrolein | Compliance with the VOC BACT requirement |
| Benzene | Compliance with the VOC BACT requirement |
| Benzo(a)pyrene | Compliance with the VOC BACT requirement |
| 1,3-Butadiene | Compliance with the VOC BACT requirement |
| Carbon monoxide | Compliance with the CO BACT requirement |
| Diesel engine exhaust particulate | Compliance with the PM BACT requirement |
| Formaldehyde | Compliance with the VOC BACT requirement |
| Nitrogen dioxide | Compliance with the NO _x BACT requirement |
| Sulfur dioxide | Compliance with the SO ₂ BACT requirement |
| Toluene | Compliance with the VOC BACT requirement |
| Total PAHs | Compliance with the VOC BACT requirement |
| Xylenes | Compliance with the VOC BACT requirement |

ATTACHMENT A
NOMINAL-UNCONTROLLED EMISSION ESTIMATES

TABLE UNC-1. NOMINAL UNCONTROLLED (COLD-START ADJUSTED) EMISSION RATES FOR BACT ANALYSIS

Table X. Nominal-Controlled Cold-Start NOX Emissions Accounting for SCR Delay Time

| Load | Nominal Uncontrolled NOX, lbs/hr | Minutes SCR Delay | Guaranteed Efficacy (%) | Nominal Controlled CO, lbs/hr | Minutes Full SCR Control | Nominal Controlled NOX Emission, lbs/hr | Overall Cold Start % NOX Removal |
|-------|----------------------------------|-------------------|-------------------------|-------------------------------|--------------------------|---|----------------------------------|
| 10% | 6.0 | 20 | 0% | 6.00 | 40 | 6.00 | 0% |
| 81.3% | 37.2 | 10 | 0% | 37.17 | 50 | 37.2 | 0% |
| 90% | 43.6 | 10 | 0% | 43.57 | 50 | 43.6 | 0% |
| 93.3% | 46.1 | 10 | 0% | 46.14 | 50 | 46.1 | 0% |
| 100% | 51.5 | 10 | 0% | 51.50 | 50 | 51.5 | 0% |

STEADY-STATE REMOVAL EFFICIENCIES

| Pollutant | Removal Effct (%) |
|------------|-------------------|
| Nox | 0% |
| PM (FH+BH) | 0% |
| CO | 0% |
| VOC | 0% |

Table X. Nominal-Controlled (Cold-Start Adjusted) PM Emission Rates (Includes FH+BH Factor)

| Elec Load | Nominal Uncontrolled Front-Half Only Emiss Rate (lbs/hr) | Total PM to Front Half PM Ratio | Nominal Uncontrolled Total PM Emiss Rate (lbs/hr) | Guaranteed Efficacy (%) | Nominal Contr Total PM (lbs/hr) | Dell 1-Hour Cold Start Factor | Nominal Controlled Total PM, lbs/hr |
|-----------|--|---------------------------------|---|-------------------------|---------------------------------|-------------------------------|-------------------------------------|
| 10% | 0.43 | 3.38 | 1.45 | 0% | 1.451 | 1.058 | 1.54 |
| 81.3% | 0.83 | 3.08 | 2.55 | 0% | 2.552 | 1.058 | 2.70 |
| 90% | 0.95 | 3.08 | 2.92 | 0% | 2.921 | 1.058 | 3.09 |
| 93.3% | 0.99 | 3.08 | 3.04 | 0% | 3.044 | 1.058 | 3.22 |
| 100% | 1.08 | 3.00 | 3.24 | 0% | 3.240 | 1.058 | 3.43 |

Total:FH Adjustment Factors

| Load | Stacktest Tot PM | Stacktest Only PM | Total PM to Front Half PM Ratio |
|---------|------------------|-------------------|---------------------------------|
| 80%-90% | | | 3.08 |
| 100% | 0.36 | 0.12 | 3.00 |
| 50% | 0.27 | 0.08 | 3.38 |

Table Y. Nominal-Controlled Cold-Start CO Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Efficacy (%) | Nominal Controlled CO, lbs/hr | Minutes Full DOC Control | Wtd Average 1-Hour CO Emission, lbs/hr | Cold Start Factor | Nominal Controlled CO, lbs/hr | Overall Cold Start % CO Removal |
|-------|-----------------------------------|-------------------|-------------------------|-------------------------------|--------------------------|--|-------------------|-------------------------------|---------------------------------|
| 10% | 2.8 | 20 | 0% | 2.80 | 40 | 2.80 | 1.058 | 2.96 | 0% |
| 81.3% | 5.3 | 10 | 0% | 5.30 | 50 | 5.30 | 1.058 | 5.61 | 0% |
| 90% | 6.0 | 10 | 0% | 6.00 | 50 | 6.00 | 1.058 | 6.35 | 0% |
| 93.3% | 6.3 | 10 | 0% | 6.30 | 50 | 6.30 | 1.058 | 6.67 | 0% |
| 100% | 6.8 | 10 | 0% | 6.80 | 50 | 6.80 | 1.058 | 7.19 | 0% |

Table Y. Nominal-Controlled Cold-Start VOC Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Efficacy (%) | Nominal Controlled VOC, lbs/hr | Minutes Full DOC Control | Wtd Average 1-Hour Emission, lbs/hr | Cold Start Factor | Nominal Controlled VOC, lbs/hr | Overall Cold Start % Removal |
|-------|-----------------------------------|-------------------|-------------------------|--------------------------------|--------------------------|-------------------------------------|-------------------|--------------------------------|------------------------------|
| 10% | 1.2 | 20 | 0% | 1.23 | 40 | 1.23 | 1.058 | 1.30 | 0% |
| 81.3% | 1.1 | 10 | 0% | 1.10 | 50 | 1.10 | 1.058 | 1.16 | 0% |
| 90% | 1.1 | 10 | 0% | 1.10 | 50 | 1.10 | 1.058 | 1.16 | 0% |
| 93.3% | 1.1 | 10 | 0% | 1.10 | 50 | 1.10 | 1.058 | 1.16 | 0% |
| 100% | 1.1 | 10 | 0% | 1.10 | 50 | 1.10 | 1.058 | 1.16 | 0% |

Table UNC-2. Uncontrolled Facility-Wide Emissions (Basis = ELM's Nominal-Uncontrolled, Plus Cold-Start Factors)

| Hours at Each Runtime Mode | | | | | | | | | | | | | | Each Genset DPM lbs/hr | Each Genset Fuel Gal/Hr | Each Genset NOX lbs/hr | Facility Wide Total PM Tons/yr | Facility-Wide Fuel Gal/Year | Facility Wide NOX Tons/yr | Each Genset CO lbs/hr | Facility-Wide CO Tons/yr | Each Genset HC lbs/hr | Facility-Wide VOC Tons/yr | | | | |
|---|----------|-----------|----------|----|---|---|-----|--------|---------------|------------------|-----------------------|------|--------------|------------------------------------|-------------------------|------------------------|--------------------------------|-----------------------------|---------------------------|-----------------------|--------------------------|-----------------------|---------------------------|----------------|--|------|--|
| Gen # | Gen Area | Elec Load | No. Gens | W | M | Q | A-F | A-Step | Correct Tests | De-En Bldg Maint | Outage or Storm Avoid | Cool | Total hrs/yr | | | | | | | | | | | AERMOD Hrs/day | | | |
| Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | | Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | | | | | | 24 | | 24 | 24 | 2.70 | 195 | 37.2 | 0.162 | 23,400 | 2.23 | 5.61 | 0.34 | 1.16 | 0.070 | | | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | | | | | | 24 | | 24 | 24 | 3.09 | 213 | 43.57 | 0.111 | 15,336 | 1.57 | 6.35 | 0.23 | 1.16 | 0.042 | | | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | | | | | | 24 | | 24 | 24 | 3.09 | 213 | 43.57 | 0.111 | 15,336 | 1.57 | 6.35 | 0.23 | 1.16 | 0.042 | | | |
| ETC-1 | ETC | 93% | 1 | | | | | | | | 24 | | 24 | 24 | 3.22 | 220 | 46.14 | 0.039 | 5,280 | 0.55 | 6.67 | 0.08 | 1.16 | 0.014 | | | |
| Testing at Full Outage Loads | | | | | | | | | | | | | | Testing at Full Outage Loads | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | 3 | 6 | | | 8 | | | 17 | 24 | 2.70 | 195 | 37.2 | 0.115 | 16,575 | 1.58 | 5.61 | 0.24 | 1.16 | 0.049 | | | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | 3 | 6 | | | 8 | | | 17 | 24 | 3.09 | 213 | 43.57 | 0.079 | 10,863 | 1.11 | 6.35 | 0.16 | 1.16 | 0.030 | | | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | 3 | 6 | | | 8 | | | 17 | 24 | 3.09 | 213 | 43.57 | 0.079 | 10,863 | 1.11 | 6.35 | 0.16 | 1.16 | 0.030 | | | |
| ETC-1 | ETC | 93% | 1 | | | 3 | 6 | | | 8 | | | 17 | 24 | 3.22 | 220 | 46.14 | 0.027 | 3,740 | 0.39 | 6.67 | 0.06 | 1.16 | 0.010 | | | |
| 100% Load | | | | | | | | | | | | | | Testing at 100% Load | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 100% | 5 | | | | | 0.5 | 8 | | | | 8.5 | 24 | 3.43 | 232 | 51.50 | 0.073 | 9,860 | 1.09 | 7.19 | 0.15 | 1.16 | 0.025 | | | |
| 2-1 to 2-3 | Bldg 2 | 100% | 3 | | | | | 0.5 | 8 | | | | 8.5 | 24 | 3.43 | 232 | 51.50 | 0.044 | 5,916 | 0.66 | 7.19 | 0.09 | 1.16 | 0.015 | | | |
| 3-1 to 3-3 | Bldg 3 | 100% | 3 | | | | | 0.5 | 8 | | | | 8.5 | 24 | 3.43 | 232 | 51.50 | 0.044 | 5,916 | 0.66 | 7.19 | 0.09 | 1.16 | 0.015 | | | |
| ETC-1 | ETC | 100% | 1 | | | | | 0.5 | 8 | | | | 8.5 | 24 | 3.43 | 232 | 51.50 | 0.015 | 1,972 | 0.22 | 7.19 | 0.03 | 1.16 | 0.005 | | | |
| 1-6 and 1-7 Reserve | Bldg 1 | 100% | 2 | | | | | 0.5 | 8 | | | | 8.5 | 24 | 3.43 | 232 | 51.50 | 0.029 | 3,944 | 0.44 | 7.19 | 0.06 | 1.16 | 0.010 | | | |
| 2-4 Reserve | Bldg 2 | 100% | 1 | | | | | 0.5 | 8 | | | | 8.5 | 24 | 3.43 | 232 | 51.50 | 0.015 | 1,972 | 0.22 | 7.19 | 0.03 | 1.16 | 0.005 | | | |
| 3-4 Reserve | Bldg 3 | 100% | 1 | | | | | 0.5 | 8 | | | | 8.5 | 24 | 3.43 | 232 | 51.50 | 0.015 | 1,972 | 0.22 | 7.19 | 0.03 | 1.16 | 0.005 | | | |
| ETC-2 Reserve | ETC | 100% | 1 | | | | | 0.5 | 8 | | | | 8.5 | 24 | 3.43 | 232 | 51.50 | 0.015 | 1,972 | 0.22 | 7.19 | 0.03 | 1.16 | 0.005 | | | |
| Idle (set to 10% for emission calculations) | | | | | | | | | | | | | | Idle | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 10% | 5 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 24 | 1.54 | 45 | 6.00 | 0.136 | 7,988 | 0.53 | 2.96 | 0.26 | 1.30 | 0.115 | | | |
| 2-1 to 2-3 | Bldg 2 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 24 | 1.54 | 45 | 6.00 | 0.082 | 4,793 | 0.32 | 2.96 | 0.16 | 1.30 | 0.069 | | | |
| 3-1 to 3-3 | Bldg 3 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 24 | 1.54 | 45 | 6.00 | 0.082 | 4,793 | 0.32 | 2.96 | 0.16 | 1.30 | 0.069 | | | |
| ETC-1 | ETC | 10% | 1 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 24 | 1.54 | 45 | 6.00 | 0.027 | 1,598 | 0.11 | 2.96 | 0.05 | 1.30 | 0.023 | | | |
| 1-6 and 1-7 Reserve | Bldg 1 | 10% | 2 | 20 | 6 | 3 | 6 | | | 8 | 24 | 1.5 | 68.5 | 24 | 1.54 | 45 | 6.00 | 0.105 | 6,165 | 0.41 | 2.96 | 0.20 | 1.30 | 0.089 | | | |
| 2-4 Reserve | Bldg 2 | 10% | 1 | 20 | 6 | 3 | 6 | | | 8 | 24 | 1.5 | 68.5 | 24 | 1.54 | 45 | 6.00 | 0.053 | 3,083 | 0.21 | 2.96 | 0.10 | 1.30 | 0.045 | | | |
| 3-4 Reserve | Bldg 3 | 10% | 1 | 20 | 6 | 3 | 6 | | | 8 | 24 | 1.5 | 68.5 | 24 | 1.54 | 45 | 6.00 | 0.053 | 3,083 | 0.21 | 2.96 | 0.10 | 1.30 | 0.045 | | | |
| ETC-2 Reserve | ETC | 10% | 1 | 20 | 6 | 3 | 6 | | | 8 | 24 | 1.5 | 68.5 | 24 | 1.54 | 45 | 6.00 | 0.053 | 3,083 | 0.21 | 2.96 | 0.10 | 1.30 | 0.045 | | | |
| | | | | | | | | | | | | | | | | | | PM (tpy) | | NOX (tpy) | | CO (tpy) | | VOC (tpy) | | | |
| Uncontrolled Facility-Wide Emissions | | | | | | | | | | | | | | | | | | 1.56 | | 169,500 | | 16.14 | | 3.15 | | 0.87 | |

ATTACHMENT B
AIRCLARITY EMISSION CONTROL SYSTEM (CATALYZED DPF + SCR)
BACT ASSESSMENT

**MTU AIRCLARITY CONTROL SYSTEM
CATALYZED DPF + UREA SCR**

ELM Permitting Information

9. Narrative of Tier-4 emission control equipment, including vendor-guaranteed removal efficiencies.

The diesel emission control strategy the AirClarity utilizes highly oxidizing precious metal particulate matter filters to control PM, HC, and CO reductions, as well as a Selective Catalytic Reducer coupled with an airless DEF injection system.

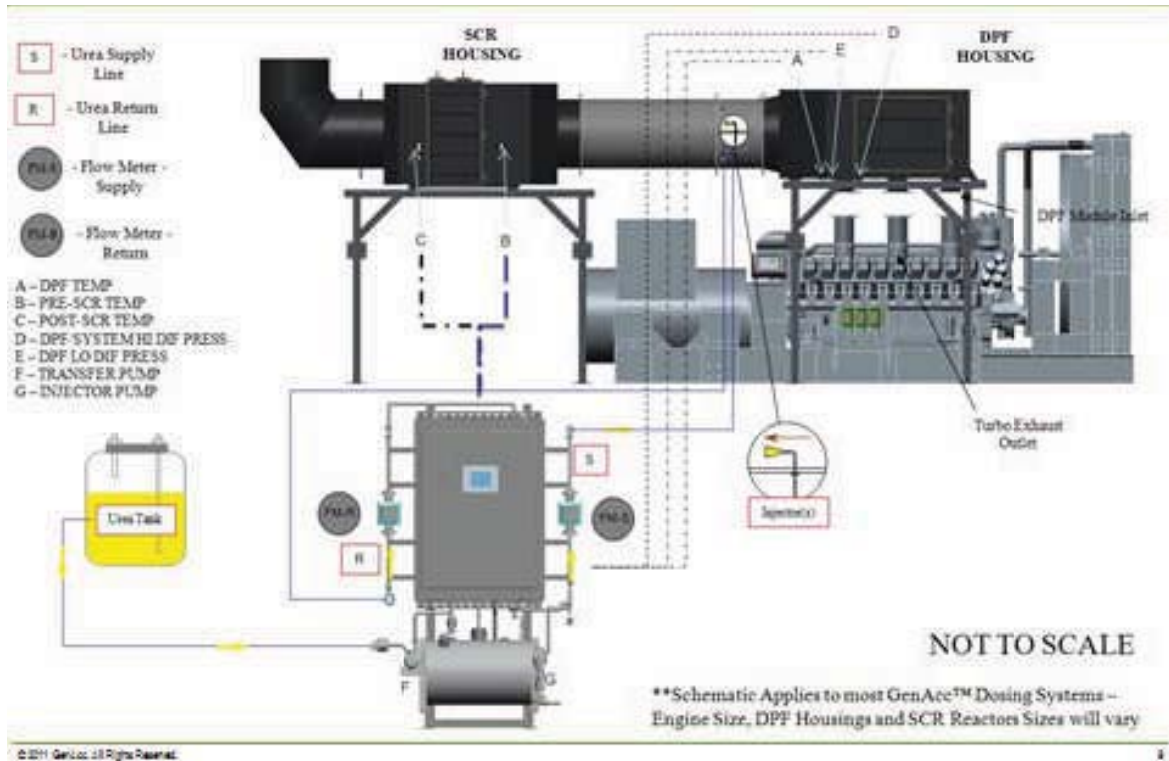
The injection system includes reductant tank level monitoring, return and supply flow metering, DPF temperature, SCR temperature (pre and post), DPF backpressure, system backpressure, and SCR outlet NO_x sensor; all parameters are logged and will produce alarms should the system operate out of spec. A relative humidity sensor will also be utilized in the system, as humidity has been known to affect engine-out NO_x by as much as 15% depending on ambient conditions.

The EnviCat[®] 2055 DPF is a wall flow ceramic Diesel Particulate Filter coated with a Süd-Chemie proprietary precious metal based coating on a cordierite ceramic substrate. The device is designed to filter and passively reduce >95% diesel particulate matter mass found in diesel engine exhaust. Furthermore, carbon monoxide and hydrocarbon emissions in the exhaust are reduced by means of catalytic oxidation. This device does not employ zone coating. The catalyzed DPF is also responsible for reducing hydrocarbons by almost 96%, as well as carbon monoxide reductions of greater than 99% (reductions based on engine baseline and emissions testing at 5-mode average).

The EnviCat[®] 20019 SCR is a flow through ceramic substrate coated with a Süd-Chemie proprietary SCR coating. The SCR is designed to reduce engine out NO_x emissions across a broad range of engine operating conditions.

Vendor-guaranteed removal efficiencies are as follows:

NO_x >90%
CO >90%
HC >90%
PM >87%



10. Has the Tier-4 generator achieved CARB certification? If so, provide the certification data.

No. In process.

11. Vendor-estimated purchase price of emission control equipment compared to Tier-2 generators

Estimated \$400,000 increase per Tier-2 generator.

12. Vendor's "Not-to-Exceed" and "Nominal" emission data.

See attached spreadsheets for both "Not-to-Exceed" (NTE) and nominal controlled emissions information.

13. Narrative of cold-start delay time before catalysts reach activation temperature and perform at vendor-guaranteed removal efficiency

The SCR is designed to operate nominally at 900 degrees Fahrenheit, however NOx conversion can be achieved from 300 to 1000 degrees Fahrenheit. Due to the possibility of forming ammonia salts at lower temperatures, DEF will only be injected at 425 degrees Fahrenheit or higher. Should the temperatures exceed 1000 degrees, the system will alarm as temperatures higher than this can result in catalyst degradation and possible destruction of the honeycomb material. Testing on the 20v4000 indicates

we can run at 10% load and dose Urea to reduce NOx. We believe this would happen in under 20 minutes with most conditions having dosing start in less than 15 minutes.

The DPF will reduce PM at all times but should be regenerated when one of the following conditions is met:

- After back pressure readings have reached the maximum allowable backpressure per manufacturers specifications (27" W.C.)
- After 24 idle cold starts of 30-minutes or less and no regeneration has been performed between the cold starts.
- After operation below the recommended regeneration temperature of 300°C for a consecutive period of 720-minutes

Regeneration is accomplished by bringing the engine load level required to achieve a minimum 300°C exhaust gas temperature at the filter inlet and holding for a minimum period of 30-minutes. In testing with the 20v4000 the filters should regen at 10% load unless ambient temperatures are extremely low.

Should the soot loading reach a high level before cold start maximum is reached, the DPF differential pressure sensor will read a high backpressure and the system will alarm. Should the system reach 24 cold starts without reaching the maximum backpressure, the system will alarm and alert the user for the need to regenerate the DPF elements.

14. Can the vendor provide a document of stack test data?

Stack test data (except for particulate and ammonia) are attached for NOx, CO, & HC at 100%, 75%, 50%, 25%, and 10% loads. Final stack test results for ammonia and particulate are expected to be available next week and completed results will be forwarded as soon as they are received.

TABLE AIRCLARITY-1. AIRCLARITY NOMINAL CONTROLLED (COLD-START ADJUSTED) EMISSION RATES FOR BACT ANALYSIS

Table X. Nominal-Controlled Cold-Start NOX Emissions Accounting for SCR Delay Time

| Load | Nominal Uncontrolled NOX, lbs/hr | Minutes SCR Delay | Guaranteed Effic (%) | Nominal Controlled CO, lbs/hr | Minutes Full SCR Control | Nominal Controlled NOX Emission, lbs/hr | Overall Cold Start % NOX Removal |
|-------|----------------------------------|-------------------|----------------------|-------------------------------|--------------------------|---|----------------------------------|
| 10% | 6.0 | 20 | 90% | 0.60 | 40 | 2.40 | 60% |
| 81.3% | 37.2 | 10 | 90% | 3.72 | 50 | 9.29 | 75% |
| 90% | 43.6 | 10 | 90% | 4.36 | 50 | 10.89 | 75% |
| 93.3% | 46.1 | 10 | 90% | 4.61 | 50 | 11.53 | 75% |
| 100% | 51.5 | 10 | 90% | 5.15 | 50 | 12.88 | 75% |

AIRCLARITY STEADY-STATE REMOVAL EFFICIENCIES

| Pollutant | Removal Effct (%) |
|------------|-------------------|
| Nox | 90% |
| PM (FH+BH) | 87% |
| CO | 90% |
| VOC | 90% |

Table X. Nominal-Controlled (Cold-Start Adjusted) PM Emission Rates (Includes FH+BH Factor)

| Elec Load | Nominal Uncontrolled Front-Half Only Emiss Rate (lbs/hr) | Total PM to Front Half PM Ratio | Nominal Uncontrolled Total PM Emiss Rate (lbs/hr) | Guaranteed Effic (%) | Nominal Contr Total PM (lbs/hr) | Dell 1-Hour Cold Start Factor | Nominal Controlled Total PM, lbs/hr |
|-----------|--|---------------------------------|---|----------------------|---------------------------------|-------------------------------|-------------------------------------|
| 10% | 0.43 | 3.38 | 1.45 | 87% | 0.189 | 1.058 | 0.200 |
| 81.3% | 0.83 | 3.08 | 2.55 | 87% | 0.332 | 1.058 | 0.351 |
| 90% | 0.95 | 3.08 | 2.92 | 87% | 0.380 | 1.058 | 0.402 |
| 93.3% | 0.99 | 3.08 | 3.04 | 87% | 0.396 | 1.058 | 0.419 |
| 100% | 1.08 | 3.00 | 3.24 | 87% | 0.421 | 1.058 | 0.446 |

Total:FH Adjustment Factors

| Load | Stacktest Tot PM | Stacktest FH Only PM | Total PM to Front Half PM Ratio |
|---------|------------------|----------------------|---------------------------------|
| 80%-90% | | | 3.08 |
| 100% | 0.36 | 0.12 | 3.00 |
| 50% | 0.27 | 0.08 | 3.38 |

Table Y. Nominal-Controlled Cold-Start CO Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Effic (%) | Nominal Controlled CO, lbs/hr | Minutes Full DOC Control | Wtd Average 1-Hour CO Emission, lbs/hr | Cold Start Factor | Nominal Controlled CO, lbs/hr | Overall Cold Start % CO Removal |
|-------|-----------------------------------|-------------------|----------------------|-------------------------------|--------------------------|--|-------------------|-------------------------------|---------------------------------|
| 10% | 2.8 | 20 | 90% | 0.28 | 40 | 1.12 | 1.058 | 1.18 | 60% |
| 81.3% | 5.3 | 10 | 90% | 0.53 | 50 | 1.33 | 1.058 | 1.40 | 75% |
| 90% | 6.0 | 10 | 90% | 0.60 | 50 | 1.50 | 1.058 | 1.59 | 75% |
| 93.3% | 6.3 | 10 | 90% | 0.63 | 50 | 1.58 | 1.058 | 1.67 | 75% |
| 100% | 6.8 | 10 | 90% | 0.68 | 50 | 1.70 | 1.058 | 1.80 | 75% |

Table Y. Nominal-Controlled Cold-Start VOC Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Effic (%) | Nominal Controlled VOC, lbs/hr | Minutes Full DOC Control | Wtd Average 1-Hour Emission, lbs/hr | Cold Start Factor | Nominal Controlled VOC, lbs/hr | Overall Cold Start % Removal |
|-------|-----------------------------------|-------------------|----------------------|--------------------------------|--------------------------|-------------------------------------|-------------------|--------------------------------|------------------------------|
| 10% | 1.2 | 20 | 90% | 0.12 | 40 | 0.49 | 1.058 | 0.52 | 60% |
| 81.3% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 90% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 93.3% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 100% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |

Table AIRCLARITY-2. AirClarity Nominal-Controlled Facility-Wide Emissions (Basis = ELM's Nominal-Uncontrolled + Cold-Start Factors)

| Gen # | Gen Area | Elec Load | No. Gens | Hours at Each Runtime Mode | | | | | | | | | | Each Genset DPM lbs/hr | Each Genset Fuel Gal/Hr | Each Genset NOX lbs/hr | Facility Wide Total PM Tons/yr | Facility-Wide Fuel Gal/Year | Facility Wide NOX Tons/yr | Each Genset CO lbs/hr | Facility-Wide CO Tons/yr | Each Genset HC lbs/hr | Facility-Wide VOC Tons/yr | | | | | |
|---|----------|-----------|----------|----------------------------|---|---|-----|--------|---------------|------------------|-----------------------|------|--------------|------------------------|-------------------------|------------------------|--------------------------------------|-----------------------------|---------------------------|-----------------------|--------------------------|-----------------------|---------------------------|------|------|------|-------|-------|
| | | | | W | M | Q | A-F | A-Step | Correct Tests | De-En Bldg Maint | Outage or Storm Avoid | Cool | Total hrs/yr | | | | | | | | | | | | | | | |
| Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | | | | | | | | | | 24 | | 24 | 0.35 | 195 | 9.3 | 0.021 | 23,400 | 0.56 | 1.40 | 0.08 | 0.29 | 0.017 | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | | | | | | | | | | 24 | | 24 | 0.40 | 213 | 10.89 | 0.014 | 15,336 | 0.39 | 1.59 | 0.06 | 0.29 | 0.010 | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | | | | | | | | | | 24 | | 24 | 0.40 | 213 | 10.89 | 0.014 | 15,336 | 0.39 | 1.59 | 0.06 | 0.29 | 0.010 | |
| ETC-1 | ETC | 93% | 1 | | | | | | | | | | | | 24 | | 24 | 0.42 | 220 | 11.53 | 0.005 | 5,280 | 0.14 | 1.67 | 0.02 | 0.29 | 0.003 | |
| Testing at Full Outage Loads | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Testing at Full Outage Loads | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | | 3 | 6 | | | | | | | | | 17 | 0.35 | 195 | 9.3 | 0.015 | 16,575 | 0.39 | 1.40 | 0.06 | 0.29 | 0.012 | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | | 3 | 6 | | | | | | | | | 17 | 0.40 | 213 | 10.89 | 0.010 | 10,863 | 0.28 | 1.59 | 0.04 | 0.29 | 0.007 | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | | 3 | 6 | | | | | | | | | 17 | 0.40 | 213 | 10.89 | 0.010 | 10,863 | 0.28 | 1.59 | 0.04 | 0.29 | 0.007 | |
| ETC-1 | ETC | 93% | 1 | | | | 3 | 6 | | | | | | | | | 17 | 0.42 | 220 | 11.53 | 0.004 | 3,740 | 0.10 | 1.67 | 0.01 | 0.29 | 0.002 | |
| 100% Load | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Testing at 100% Load | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 100% | 5 | | | | | | 0.5 | 8 | | | | | | | 8.5 | 0.45 | 232 | 12.88 | 0.009 | 9,860 | 0.27 | 1.80 | 0.04 | 0.29 | 0.006 | |
| 2-1 to 2-3 | Bldg 2 | 100% | 3 | | | | | | 0.5 | 8 | | | | | | | 8.5 | 0.45 | 232 | 12.88 | 0.006 | 5,916 | 0.16 | 1.80 | 0.02 | 0.29 | 0.004 | |
| 3-1 to 3-3 | Bldg 3 | 100% | 3 | | | | | | 0.5 | 8 | | | | | | | 8.5 | 0.45 | 232 | 12.88 | 0.006 | 5,916 | 0.16 | 1.80 | 0.02 | 0.29 | 0.004 | |
| ETC-1 | ETC | 100% | 1 | | | | | | 0.5 | 8 | | | | | | | 8.5 | 0.45 | 232 | 12.88 | 0.002 | 1,972 | 0.05 | 1.80 | 0.01 | 0.29 | 0.001 | |
| 1-6 and 1-7 Reserve | Bldg 1 | 100% | 2 | | | | | | 0.5 | 8 | | | | | | | 8.5 | 0.45 | 232 | 12.88 | 0.004 | 3,944 | 0.11 | 1.80 | 0.02 | 0.29 | 0.002 | |
| 2-4 Reserve | Bldg 2 | 100% | 1 | | | | | | 0.5 | 8 | | | | | | | 8.5 | 0.45 | 232 | 12.88 | 0.002 | 1,972 | 0.05 | 1.80 | 0.01 | 0.29 | 0.001 | |
| 3-4 Reserve | Bldg 3 | 100% | 1 | | | | | | 0.5 | 8 | | | | | | | 8.5 | 0.45 | 232 | 12.88 | 0.002 | 1,972 | 0.05 | 1.80 | 0.01 | 0.29 | 0.001 | |
| ETC-2 Reserve | ETC | 100% | 1 | | | | | | 0.5 | 8 | | | | | | | 8.5 | 0.45 | 232 | 12.88 | 0.002 | 1,972 | 0.05 | 1.80 | 0.01 | 0.29 | 0.001 | |
| Idle (set to 10% for emission calculations) | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Idle | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 10% | 5 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | | | 35.5 | 0.20 | 45 | 2.40 | 0.018 | 7,988 | 0.21 | 1.18 | 0.11 | 0.52 | 0.046 | |
| 2-1 to 2-3 | Bldg 2 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | | | 35.5 | 0.20 | 45 | 2.40 | 0.011 | 4,793 | 0.13 | 1.18 | 0.06 | 0.52 | 0.028 | |
| 3-1 to 3-3 | Bldg 3 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | | | 35.5 | 0.20 | 45 | 2.40 | 0.011 | 4,793 | 0.13 | 1.18 | 0.06 | 0.52 | 0.028 | |
| ETC-1 | ETC | 10% | 1 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | | | 35.5 | 0.20 | 45 | 2.40 | 0.004 | 1,598 | 0.04 | 1.18 | 0.02 | 0.52 | 0.009 | |
| 1-6 and 1-7 Reserve | Bldg 1 | 10% | 2 | 20 | 6 | 3 | 6 | | | | | | 8 | 24 | 1.5 | 68.5 | | 68.5 | 0.20 | 45 | 2.40 | 0.014 | 6,165 | 0.16 | 1.18 | 0.08 | 0.52 | 0.036 |
| 2-4 Reserve | Bldg 2 | 10% | 1 | 20 | 6 | 3 | 6 | | | | | | 8 | 24 | 1.5 | 68.5 | | 68.5 | 0.20 | 45 | 2.40 | 0.007 | 3,083 | 0.08 | 1.18 | 0.04 | 0.52 | 0.018 |
| 3-4 Reserve | Bldg 3 | 10% | 1 | 20 | 6 | 3 | 6 | | | | | | 8 | 24 | 1.5 | 68.5 | | 68.5 | 0.20 | 45 | 2.40 | 0.007 | 3,083 | 0.08 | 1.18 | 0.04 | 0.52 | 0.018 |
| ETC-2 Reserve | ETC | 10% | 1 | 20 | 6 | 3 | 6 | | | | | | 8 | 24 | 1.5 | 68.5 | | 68.5 | 0.20 | 45 | 2.40 | 0.007 | 3,083 | 0.08 | 1.18 | 0.04 | 0.52 | 0.018 |
| | | | | | | | | | | | | | | | | | Total PM | | NOX | | CO | | VOC | | | | | |
| | | | | | | | | | | | | | | | | | CONTROLLED Facility-Wide Emissions | 0.203 | 169,500 | 4.38 | 0.958 | | 0.293 | | | | | |
| | | | | | | | | | | | | | | | | | UNCONTROLLED Facility-Wide Emissions | 1.56 | | 16.14 | 3.15 | | 0.870 | | | | | |
| | | | | | | | | | | | | | | | | | Tons/Yr Removed | 1.36 | | 11.76 | 2.19 | | 0.58 | | | | | |
| | | | | | | | | | | | | | | | | | Overall Removal Effcy, % | 87% | | 73% | 70% | | 66% | | | | | |

Table AIRCLARITY-3. BACT Capital Cost for MTU AirClarity System (SCR and Catalyzed DPF)

| Vantage Data Center | | | | | |
|--|------------------------|------------------------|--------|-----------|---------------|
| Cost Category | Cost Factor | Source of Cost Factor | Quant. | Unit Cost | Subtotal Cost |
| Direct Costs | | | | | |
| Purchased Equipment Costs | | | | | |
| FOB Purchase Price | As quoted by MTU | MTU | 17 | \$400,000 | \$6,800,000 |
| Instrumentation | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Sales Tax | WA state tax | WA state tax | 6.5% | -- | \$442,000 |
| Shipping | 0.05A | EPA Cost Manual | 5.0% | -- | \$340,000 |
| Subtotal Purchased Equipment Cost, PEC | | | | | \$7,582,000 |
| Direct Installation Costs | | | | | |
| Enclosure structural supports | Assume no cost | Assume no cost | 0 | \$0 | \$0 |
| Installation | 1/2 of EPA Cost Manual | 1/2 of EPA Cost Manual | 2.5% | -- | \$189,550 |
| Electrical | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Piping | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Insulation | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Painting | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Subtotal Direct Installation Costs | | | | | \$189,550 |
| Site Preparation and Buildings (SP) | | | | | |
| Site Preparation and Buildings (SP) | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Total Direct Costs, DC (PEC + Direct Installation + Site Prep) | | | | | \$7,771,550 |
| Indirect Costs (Installation) | | | | | |
| Engineering | 0.025*PEC | 1/4 of EPA Cost Manual | 2.5% | -- | \$189,550 |
| Construction and field expenses | 0.025*PEC | 1/2 of EPA Cost Manual | 2.5% | -- | \$189,550 |
| Contractor Fees | From DIS data center | From DIS data center | 6.8% | -- | \$532,645 |
| Startup | 0.02*PEC | EPA Cost Manual | 2.0% | -- | \$151,640 |
| Performance Test (Tech support) | 0.01*PEC | EPA Cost Manual | 1.0% | -- | \$75,820 |
| Contingencies | 0.03*PEC | EPA Cost Manual | 3.0% | -- | \$227,460 |
| Subtotal Indirect Costs, IC | | | | | \$1,366,665 |
| Total Capital Investment (TCI = DC+IC) | | | | | \$9,138,215 |
| | | | | | TCI per gen |
| | | | | | \$537,542 |

Table AIRCLARITY-4. Nominal-Controlled BACT Cost-Effectiveness for MTU AirClarity System

| Item | Quantity | Units | Unit cost | Subtotal |
|--|------------------------|-------|-----------|------------------|
| Annualized Capital Recovery | | | | |
| Total Capital Cost | | | | \$9,138,215 |
| Capital Recovery Factor, 25 yrs, 4% discount rate | | | | 0.06401 |
| Subtotal Annualized 25-year Capital Recovery Cost | | | | \$584,937 |
| Direct Annual Costs | | | | |
| Annual Admin charges | 2% of TCI (EPA Manual) | | 0.02 | \$182,764 |
| Annual Property tax | 1% of TCI (EPA Manual) | | 0.01 | \$91,382 |
| Annual Insurance | 1% of TCI (EPA Manual) | | 0.01 | \$91,382 |
| Annual operation/labor/maintenance costs: Upperbound estimate would assume CARB's value of \$3.00/hp/year and would result in \$206,000/year. Lower bound estimate would assume zero annual O&M. Mid-range value would account for urea, fuel for pressure drop, increased inspections, periodic OEM visits, and the costs for Ecology's increased emission testing requirements. <u>For this screening-level analysis we assumed the lower-bound annual O&M cost of zero.</u> | | | | \$0 |
| Subtotal Direct Annual Costs | | | | \$365,529 |
| Total Annual Cost (Capital Recovery + Direct Annual Costs) | | | | \$950,466 |
| Uncontrolled emissions (Combined Pollutants) | | | | 21.7 |
| Assumed Control Efficiency | | | | Varies |
| Annual Tons Removed (Combined Pollutants) | | | | 15.89 |
| Cost Effectiveness (\$ per tons combined pollutant destroyed) | | | | \$59,823 |

| | |
|---------|-----------|
| TCI/gen | \$537,542 |
|---------|-----------|

Combined Pollutants Removal Tonnages (Nominal-Controlled)

| Pollutant | PM (FH+BH) | CO | VOC | NOX |
|-------------------------------------|------------|-----------|-------------|----------|
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 0.203 | 0.958 | 0.293 | 4.38 |
| Tons Removed/Year | 1.36 | 2.19 | 0.578 | 11.8 |
| Overall Cold-Start Removal Effcy | 87% | 70% | 66% | 73% |
| Indiv Poll \$/Ton Removed | \$700,039 | \$433,611 | \$1,644,950 | \$80,819 |

Multi-Pollutant Cost-Effectiveness for Acceptable Control Cost vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Acceptable Annual Cost (\$/year) |
|---|---------------------------------------|----------------------------|---|
| NOX | \$10,000 | 11.76 | \$117,604 per year |
| CO | \$5,000 | 2.19 | \$10,960 per year |
| VOC | \$9,999 | 0.58 | \$5,778 per year |
| PM (FH+BH) | \$23,200 | 1.36 | \$31,499 per year |
| Total Acceptable Annual Control Cost for Combined Pollutants | | | \$165,841 per year |
| Actual Annual Control Cost | | | \$950,466 per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Acceptable) |

ATTACHMENT C
CATALYZED DPF BACT ASSESSMENT

**CATALYZED DPF TECHNICAL DATA AND COST QUOTE
SABEY-INTERGATE-QUINCY DATA CENTER**

PROPOSAL

Proposal Date: **Wednesday, December 08, 2010**

Quotation Number: **10120806RW-F** Rev:

| | |
|--|--|
| <p>Customer Contact: John Ford Title: Director of Technology Real Estate Email: johnf@sabey.com Phone: 206-277-5209 Cell: Company Name: Sabey Corporation Address : 12201 Tukwila International Blvd. Seattle, WA 98168</p> | <p style="text-align: center;">Project Description</p> <p style="text-align: center; background-color: #4a86e8; color: white;">Sabey Construction - CAT 3516C 2000 kW Generator</p> <p>Address:</p> |
| <p>Product Quoted: PERMIT Filter System in a 304L Stainless Steel Double Wall Insulated Critical Grade Silencer</p> | |
| <p>Purchase Order Date:</p> | <p>Requested Installation Date:</p> |

| Engine Specifications: | | CAT |
|-------------------------------|----------------------------|--------------------------------|
| Engine Model: | 3516C | Engine S/N: |
| EPA Tier Level: | Tier 2 | EPA Family #: |
| Engine Displacement: | 69 liters | Engine Specification #: DM8263 |
| Fuel Type: | ULSD (<50 PPM) | Engine Model Year: 2010 |
| Required Fuel Content: | <50 ppm | Sulfur |
| Generator Power Rating: | 2,000 kW | Standby Model #: |
| Average Running Load: | Runtime: | hours/year |
| Engine Power Output: | 2,937 bhp or | 2188 kW @ 1,800 RPM |
| Exhaust Flow Rate: | 15,136 ACFM | |
| Exhaust Stack Temp: | 762 deg F | |
| Maximum Exhaust Pressure: | 27 inches H ₂ O | |

| Emissions Specifications: | | |
|---|-------------------------|--------------------|
| Engine Emissions: <i>Certified</i> | | |
| NOx: | 3.93 g/bhp-hr | |
| CO: | 0.49 g/bhp-hr | |
| HC: | 0.25 g/bhp-hr | |
| PM: | 0.08 g/bhp-hr | |
| Emissions Reduction Required: | | |
| | | % Reduction |
| CO: | g/bhp-hr | |
| HC: | g/bhp-hr | |
| PM: | g/bhp-hr | |
| Emissions Post After Treatment: | | |
| | <i>Estimated</i> | % Reduction |
| CO: | 0.049 g/bhp-hr | 90% |
| HC: | 0.025 g/bhp-hr | 90% |
| PM: | 0.012 g/bhp-hr | 85% |

PERMIT Filter Specifications:

Material: Catalyzed Cordierite Ceramic wall-flow filter substrates
 PM Reduction: 85% *CARB Level 3+ verified for greater than 85%*
 CO Reduction: 90%
 HC(VOC) Reduction: 90%
 PERMIT Filter Part Number: FDA221
 Number of Filters: 9
 Filter Pressure Drop: 10.2 inches H₂O as configured at rated load
 Regeneration using ULSD: Above 350 deg C (662 deg F) for 30% of the engine operating time and greater than 40% engine load
 Stationary Cold Starts: 12 consecutive 10 minute idle sessions followed by 2 hrs regeneration
 Cleaning: 2,500 hour intervals
 Catalyst Life Expectancy: 10,000 hours

Critical Grade Silencer Housing Specifications:

10081103AF

Material: 304L Stainless Steel
 Construction: Double Wall, Rigid, & Light Weight
 Insulation: 2" Between two 304L Stainless Steel Walls
 Approximate Dimensions (inches): 96 " Length 90 " Width 52 " Height
 Estimated Weight: 3,750 pounds 1,705 kilograms
 Sound Reduction: 27-35 dBa, Critical Grade Silencing
 Total System Pressure Drop Silencer+DPF: 13.2 inches H₂O as configured at rated load
 Inlet Size: 22 inches Flange
 Outlet Size: 22 inches Flange

HiBACK USB Controller:

07010204AG

Data Logger: Monitors and Records the Exhaust Temperature, Pressure, Date, and Time every 15 sec. for 26,000 readings
 Alarm System: Red warning light for maximum pressure exceeded
 Yellow warning light for pending high pressure levels
 Self Diagnostics: Flashing lights indicate if the pressure or temperature not recording
 Rugged Construction: Cast Aluminum weathertight housing
 Easy data downloads: With software the logged data can be downloaded to an excel spreadsheet for analysis

This System Includes:

| | | |
|---|-----|--|
| PERMIT DPF | Yes | >85% PM, >90% CO, >90% HC Reductions |
| CRITICAL GRADE SILENCER - Stainless Steel | Yes | Double wall Insulated Critical Grade Silencer |
| HiBACK USB Controller | Yes | Required by CARB and to validate warranty |
| HiBACK USB Level 2 Software | Yes | Required to download HiBACK USB data information |
| Operation & Maintenance Manual | Yes | |

This System Excludes:

- Delivery/Freight Expenses
- Installation of the PERMIT Filter System
- Exhaust piping insulation (*CleanAIR Systems recommends insulating the exhaust from the engine to the inlet of the filter*)
- All necessary permitting

Terms & Conditions: *FOB Santa Fe*

| | | |
|------------------|-------------|--|
| Shipping Date: | 12 | weeks from date of purchase order and approved design |
| Terms: | Net 30 Days | |
| Proposal Valid : | 30 | days from proposal date |
| Warranty: | 1 | year(s) or 1,000 hours of Operation from Commissioning |

Notes:

Pricing:

| Part Number | Description | Quantity | Unit Price | Total (USD) |
|---------------|--|----------|------------|---------------------|
| 1 | 10081103AF PERMIT Filter In an Insulated Double Wall 304L Stainless Steel Critical Grade Silencer System | 3 | \$106,586 | \$319,758.00 |
| 2 | 07010204AG HiBACK USB Pressure Alarm/ Data Logger | 3 | \$1,023 | \$3,069.00 |
| 3 | 07010202AG HiBACK USB Level 2 Software | 1 | \$165 | \$165.00 |
| 4 | | | | \$ - |
| 5 | Handling/Skidding: | | | \$3,229.91 |
| 6 | Estimated Freight: | | | |
| Total: | | | | \$329,221.91 |

| <i>Recommended Optional Equipment:</i> | | | | |
|--|--|----------|------------|-------------|
| Part Number | Description | Quantity | Unit Price | Total (USD) |
| 1 | Custom Insulating Blanket for exhaust piping, etc. | Size TBD | | TBD |
| 2 | Load Bank | Size TBD | | TBD |
| 3 | | | | \$ - |
| 4 | Spare Set of Filter Elements for one system | 9 | \$8,992.50 | \$80,932.50 |

Handling/Skidding : 1% of the total order will be charged to prepare the unit for shipping with a \$10 minimum for orders under \$100, \$20 minimum for orders \$101 to \$1000, and a \$30 minimum for orders \$1,001 to \$3,000.

Order Cancellations: Standard Parts – A flat 20% fee will be charged on canceled orders for standard parts.

Custom Parts – Customer will incur all expenses at the time of order cancellation including; materials, engineering & labor plus 20

Contact Information:

N C Power Systems

Don Lee King
Power Generation Sales
425-656-4586

DLKing@ncpowersystems.com

For additional information, visit:

TABLE DPF-1. CATALYZED DPF NOMINAL CONTROLLED (COLD-START ADJUSTED) EMISSION RATES FOR BACT ANALYSIS

Table X. Nominal-Controlled Cold-Start NOX Emissions Accounting for 3WC Delay Time

| Load | Nominal Uncontrolled NOX, lbs/hr | Minutes SCR Delay | Guaranteed Efficacy (%) | Nominal Controlled CO, lbs/hr | Minutes Full SCR Control | Nominal Controlled NOX Emission, lbs/hr | Overall Cold Start % NOX Removal |
|-------|----------------------------------|-------------------|-------------------------|-------------------------------|--------------------------|---|----------------------------------|
| 10% | 6.0 | 20 | 0% | 6.00 | 40 | 6.00 | 0% |
| 81.3% | 37.2 | 10 | 0% | 37.17 | 50 | 37.17 | 0% |
| 90% | 43.6 | 10 | 0% | 43.57 | 50 | 43.57 | 0% |
| 93.3% | 46.1 | 10 | 0% | 46.14 | 50 | 46.14 | 0% |
| 100% | 51.5 | 10 | 0% | 51.50 | 50 | 51.50 | 0% |

CATALYZED DPF STEADY-STATE REMOVAL EFFICIENCIES

| Pollutant | Removal Effct (%) |
|------------|-------------------|
| Nox | 0% |
| PM (FH+BH) | 85% |
| CO | 90% |
| VOC | 90% |

Table X. Nominal-Controlled (Cold-Start Adjusted) PM Emission Rates (Includes FH+BH Factor)

| Elec Load | Nominal Uncontrolled Front-Half Only Emiss Rate (lbs/hr) | Total PM to Front Half PM Ratio | Nominal Uncontrolled Total PM Emiss Rate (lbs/hr) | Guaranteed Efficacy (%) | Nominal Contr Total PM (lbs/hr) | Dell 1-Hour Cold Start Factor | Nominal Controlled Total PM, lbs/hr |
|-----------|--|---------------------------------|---|-------------------------|---------------------------------|-------------------------------|-------------------------------------|
| 10% | 0.43 | 3.38 | 1.45 | 85% | 0.218 | 1.058 | 0.230 |
| 81.3% | 0.83 | 3.08 | 2.55 | 85% | 0.383 | 1.058 | 0.405 |
| 90% | 0.95 | 3.08 | 2.92 | 85% | 0.438 | 1.058 | 0.464 |
| 93.3% | 0.99 | 3.08 | 3.04 | 85% | 0.457 | 1.058 | 0.483 |
| 100% | 1.08 | 3.00 | 3.24 | 85% | 0.486 | 1.058 | 0.514 |

Total:FH Adjustment Factors

| Load | Stacktest Tot PM | Stacktest t FH Only PM | Total PM to Front Half PM Ratio |
|---------|------------------|------------------------|---------------------------------|
| 80%-90% | | | 3.08 |
| 100% | 0.36 | 0.12 | 3.00 |
| 50% | 0.27 | 0.08 | 3.38 |

Table Y. Nominal-Controlled Cold-Start CO Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Efficacy (%) | Nominal Controlled CO, lbs/hr | Minutes Full DOC Control | Wtd Average 1-Hour CO Emission, lbs/hr | Cold Start Factor | Nominal Controlled CO, lbs/hr | Overall Cold Start % CO Removal |
|-------|-----------------------------------|-------------------|-------------------------|-------------------------------|--------------------------|--|-------------------|-------------------------------|---------------------------------|
| 10% | 2.8 | 20 | 90% | 0.28 | 40 | 1.12 | 1.058 | 1.18 | 60% |
| 81.3% | 5.3 | 10 | 90% | 0.53 | 50 | 1.33 | 1.058 | 1.40 | 75% |
| 90% | 6.0 | 10 | 90% | 0.60 | 50 | 1.50 | 1.058 | 1.59 | 75% |
| 93.3% | 6.3 | 10 | 90% | 0.63 | 50 | 1.58 | 1.058 | 1.67 | 75% |
| 100% | 6.8 | 10 | 90% | 0.68 | 50 | 1.70 | 1.058 | 1.80 | 75% |

Table Y. Nominal-Controlled Cold-Start VOC Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Efficacy (%) | Nominal Controlled VOC, lbs/hr | Minutes Full DOC Control | Wtd Average 1-Hour Emission, lbs/hr | Cold Start Factor | Nominal Controlled VOC, lbs/hr | Overall Cold Start % Removal |
|-------|-----------------------------------|-------------------|-------------------------|--------------------------------|--------------------------|-------------------------------------|-------------------|--------------------------------|------------------------------|
| 10% | 1.2 | 20 | 90% | 0.12 | 40 | 0.49 | 1.058 | 0.52 | 60% |
| 81.3% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 90% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 93.3% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 100% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |

Table DPF-2. DPF Nominal-Controlled Facility-Wide Emissions (Basis = ELM's Nominal-Uncontrolled + Cold-Start Factors)

| Gen # | Gen Area | Elec Load | No. Gens | Hours at Each Runtime Mode | | | | | | | | | | Each Genset DPM lbs/hr | Each Genset Fuel Gal/Hr | Each Genset NOX lbs/hr | Facility Wide Total PM Tons/yr | Facility-Wide Fuel Gal/Year | Facility Wide NOX Tons/yr | Each Genset CO lbs/hr | Facility-Wide CO Tons/Yr | Each Genset HC lbs/hr | Facility-Wide VOC Tons/Yr | | |
|---|----------|-----------|----------|----------------------------|---|---|-----|--------|---------------|------------------|-----------------------|------|--------------|------------------------|-------------------------|------------------------|--------------------------------|-----------------------------|---------------------------|-----------------------|--------------------------|-----------------------|---------------------------|-------|-------|
| | | | | W | M | Q | A-F | A-Step | Correct Tests | De-En Bldg Maint | Outage or Storm Avoid | Cool | Total hrs/yr | | | | | | | | | | | | |
| Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | | | | | | | 24 | | 24 | 0.41 | 195 | 37.2 | 0.024 | 23,400 | 2.23 | 1.40 | 0.08 | 0.29 | 0.017 | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | | | | | | | 24 | | 24 | 0.46 | 213 | 43.57 | 0.017 | 15,336 | 1.57 | 1.59 | 0.06 | 0.29 | 0.010 | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | | | | | | | 24 | | 24 | 0.46 | 213 | 43.57 | 0.017 | 15,336 | 1.57 | 1.59 | 0.06 | 0.29 | 0.010 | |
| ETC-1 | ETC | 93% | 1 | | | | | | | | | 24 | | 24 | 0.48 | 220 | 46.14 | 0.006 | 5,280 | 0.55 | 1.67 | 0.02 | 0.29 | 0.003 | |
| Testing at Full Outage Loads | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | 3 | 6 | | | | | 8 | | 17 | 0.41 | 195 | 37.2 | 0.017 | 16,575 | 1.58 | 1.40 | 0.06 | 0.29 | 0.012 | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | 3 | 6 | | | | | 8 | | 17 | 0.46 | 213 | 43.57 | 0.012 | 10,863 | 1.11 | 1.59 | 0.04 | 0.29 | 0.007 | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | 3 | 6 | | | | | 8 | | 17 | 0.46 | 213 | 43.57 | 0.012 | 10,863 | 1.11 | 1.59 | 0.04 | 0.29 | 0.007 | |
| ETC-1 | ETC | 93% | 1 | | | 3 | 6 | | | | | 8 | | 17 | 0.48 | 220 | 46.14 | 0.004 | 3,740 | 0.39 | 1.67 | 0.01 | 0.29 | 0.002 | |
| 100% Load | | | | | | | | | | | | | | | | | | | | | | | | | |
| Testing at 100% Load | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 100% | 5 | | | | | 0.5 | 8 | | | | | 8.5 | 0.51 | 232 | 51.50 | 0.011 | 9,860 | 1.09 | 1.80 | 0.04 | 0.29 | 0.006 | |
| 2-1 to 2-3 | Bldg 2 | 100% | 3 | | | | | 0.5 | 8 | | | | | 8.5 | 0.51 | 232 | 51.50 | 0.007 | 5,916 | 0.66 | 1.80 | 0.02 | 0.29 | 0.004 | |
| 3-1 to 3-3 | Bldg 3 | 100% | 3 | | | | | 0.5 | 8 | | | | | 8.5 | 0.51 | 232 | 51.50 | 0.007 | 5,916 | 0.66 | 1.80 | 0.02 | 0.29 | 0.004 | |
| ETC-1 | ETC | 100% | 1 | | | | | 0.5 | 8 | | | | | 8.5 | 0.51 | 232 | 51.50 | 0.002 | 1,972 | 0.22 | 1.80 | 0.01 | 0.29 | 0.001 | |
| 1-6 and 1-7 Reserve | Bldg 1 | 100% | 2 | | | | | 0.5 | 8 | | | | | 8.5 | 0.51 | 232 | 51.50 | 0.004 | 3,944 | 0.44 | 1.80 | 0.02 | 0.29 | 0.002 | |
| 2-4 Reserve | Bldg 2 | 100% | 1 | | | | | 0.5 | 8 | | | | | 8.5 | 0.51 | 232 | 51.50 | 0.002 | 1,972 | 0.22 | 1.80 | 0.01 | 0.29 | 0.001 | |
| 3-4 Reserve | Bldg 3 | 100% | 1 | | | | | 0.5 | 8 | | | | | 8.5 | 0.51 | 232 | 51.50 | 0.002 | 1,972 | 0.22 | 1.80 | 0.01 | 0.29 | 0.001 | |
| ETC-2 Reserve | ETC | 100% | 1 | | | | | 0.5 | 8 | | | | | 8.5 | 0.51 | 232 | 51.50 | 0.002 | 1,972 | 0.22 | 1.80 | 0.01 | 0.29 | 0.001 | |
| Idle (set to 10% for emission calculations) | | | | | | | | | | | | | | | | | | | | | | | | | |
| Idle | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 10% | 5 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 0.23 | 45 | 6.00 | 0.020 | 7,988 | 0.53 | 1.18 | 0.11 | 0.52 | 0.046 | |
| 2-1 to 2-3 | Bldg 2 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 0.23 | 45 | 6.00 | 0.012 | 4,793 | 0.32 | 1.18 | 0.06 | 0.52 | 0.028 | |
| 3-1 to 3-3 | Bldg 3 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 0.23 | 45 | 6.00 | 0.012 | 4,793 | 0.32 | 1.18 | 0.06 | 0.52 | 0.028 | |
| ETC-1 | ETC | 10% | 1 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 0.23 | 45 | 6.00 | 0.004 | 1,598 | 0.11 | 1.18 | 0.02 | 0.52 | 0.009 | |
| 1-6 and 1-7 Reserve | Bldg 1 | 10% | 2 | 20 | 6 | 3 | 6 | | | | | 8 | 24 | 1.5 | 68.5 | 0.23 | 45 | 6.00 | 0.016 | 6,165 | 0.41 | 1.18 | 0.08 | 0.52 | 0.036 |
| 2-4 Reserve | Bldg 2 | 10% | 1 | 20 | 6 | 3 | 6 | | | | | 8 | 24 | 1.5 | 68.5 | 0.23 | 45 | 6.00 | 0.008 | 3,083 | 0.21 | 1.18 | 0.04 | 0.52 | 0.018 |
| 3-4 Reserve | Bldg 3 | 10% | 1 | 20 | 6 | 3 | 6 | | | | | 8 | 24 | 1.5 | 68.5 | 0.23 | 45 | 6.00 | 0.008 | 3,083 | 0.21 | 1.18 | 0.04 | 0.52 | 0.018 |
| ETC-2 Reserve | ETC | 10% | 1 | 20 | 6 | 3 | 6 | | | | | 8 | 24 | 1.5 | 68.5 | 0.23 | 45 | 6.00 | 0.008 | 3,083 | 0.21 | 1.18 | 0.04 | 0.52 | 0.018 |
| | | | | | | | | | | | | | | | | | Total PM | | NOX | | CO | | VOC | | |
| CONTROLLED Facility-Wide Emissions | | | | | | | | | | | | | | | | | 0.234 | 169,500 | 16.14 | | 0.958 | | 0.293 | | |
| UNCONTROLLED Facility-Wide Emissions | | | | | | | | | | | | | | | | | 1.56 | | 16.14 | | 3.15 | | 0.870 | | |
| Tons/Yr Removed | | | | | | | | | | | | | | | | | 1.33 | | 0.00 | | 2.19 | | 0.58 | | |
| Overall Removal Effcy, % | | | | | | | | | | | | | | | | | 85% | | 0% | | 70% | | 66% | | |

Table DPF-3. Catalyzed DPF BACT Capital Cost (Based on Sabey-Quincy)

Vantage Data Center

| Cost Category | Cost Factor | Source of Cost Factor | Quant. | Unit Cost | Subtotal Cost |
|--|-------------------------|------------------------|--------|-----------|---------------|
| Direct Costs | | | | | |
| Purchased Equipment Costs | | | | | |
| FOB purchase price for Sabey Data Center's 2000 kWe generators was \$107,700 each. The FOB price for Vantage's 3,000 kWe generators was scaled using the "0.6 rule": Cost for 3,000 kWe units = \$109,700 *(3000/2000) ^{0.6} = \$139,900 each | | | | | |
| Vantage 3000 kWe FOB Purchase Price | Clean Emission Products | CEP | 17 | \$139,900 | \$2,378,300 |
| Instrumentation | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Sales Tax | WA state tax | WA state tax | 6.5% | -- | \$154,590 |
| Shipping | 0.05A | EPA Cost Manual | 5.0% | -- | \$118,915 |
| Subtotal Purchased Equipment Cost, PEC | | | | | \$2,651,805 |
| Direct Installation Costs | | | | | |
| Enclosure structural supports | From MSFT CO-3 | Robinson Enclosures | 0 | \$9,812 | \$0 |
| Installation | 1/2 of EPA Cost Manual | 1/2 of EPA Cost Manual | 2.5% | -- | \$66,295 |
| Electrical | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Piping | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Insulation | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Painting | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Subtotal Direct Installation Costs | | | | | \$66,295 |
| Site Preparation and Buildings (SP) | | | | | |
| Site Preparation and Buildings (SP) | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Total Direct Costs, DC (PEC + Direct Installation + Site Prep) | | | | | \$2,718,100 |
| Indirect Costs (Installation) | | | | | |
| Engineering | 0.025*PEC | 1/4 of EPA Cost Manual | 2.5% | -- | \$66,295 |
| Construction and field expenses | 0.025*PEC | 1/2 of EPA Cost Manual | 2.5% | -- | \$66,295 |
| Contractor Fees | From DIS data center | From DIS data center | 6.8% | -- | \$198,871 |
| Startup | 0.02*PEC | EPA Cost Manual | 2.0% | -- | \$53,036 |
| Performance Test (Tech support) | 0.01*PEC | EPA Cost Manual | 1.0% | -- | \$26,518 |
| Contingencies | 0.03*PEC | EPA Cost Manual | 3.0% | -- | \$79,554 |
| Subtotal Indirect Costs, IC | | | | | \$490,570 |
| Total Capital Investment (TCI = DC+IC) | | | | | \$3,208,669 |
| | | | | | TCI per gen |
| | | | | | \$188,745 |

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Table DPF-4. Catalyzed DPF Nominal-Controlled BACT Cost-Effectiveness

| Item | Quantity | Units | Unit cost | Subtotal |
|---|------------------------|-------|-----------|------------------|
| Annualized Capital Recovery | | | | |
| Total Capital Cost | | | | \$3,208,669 |
| Capital Recovery Factor, 25 yrs, 4% discount rate | | | | 0.06401 |
| Subtotal Annualized 25-year Capital Recovery Cost | | | | \$205,387 |
| Direct Annual Costs | | | | |
| Annual Admin charges | 2% of TCI (EPA Manual) | | 0.02 | \$64,173 |
| Annual Property tax | 1% of TCI (EPA Manual) | | 0.01 | \$32,087 |
| Annual Insurance | 1% of TCI (EPA Manual) | | 0.01 | \$32,087 |
| For this screening-level analysis we assumed the lower-bound annual O&M cost of zero. | | | | \$0 |
| Subtotal Direct Annual Costs | | | | \$128,347 |
| Total Annual Cost (Capital Recovery + Direct Annual Costs) | | | | \$333,734 |
| Uncontrolled emissions (Combined Pollutants) | | | | 21.7 |
| Assumed Control Efficiency | | | | Varies |
| Annual Tons Removed (Combined Pollutants) | | | | 4.10 |
| Cost Effectiveness (\$ per tons combined pollutant destroyed) | | | | \$81,472 |

| | |
|---------|-----------|
| TCI/gen | \$188,745 |
|---------|-----------|

Combined Pollutants Removal Tonnages (Nominal-Controlled)

| Pollutant | PM (FH+BH) | CO | VOC | NOX |
|-------------------------------------|------------|-----------|-----------|---------|
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 0.234 | 0.958 | 0.293 | 16.14 |
| Tons Removed/Year | 1.33 | 2.19 | 0.578 | 0.0 |
| Overall Cold-Start Removal Efficacy | 85% | 70% | 66% | 0% |
| Indiv Poll \$/Ton Removed | \$251,586 | \$152,252 | \$577,585 | #DIV/0! |

Multi-Pollutant Cost-Effectiveness for "Reasonable Control Cost" vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Acceptable Annual Cost (\$/year) |
|---|---------------------------------------|----------------------------|---|
| NOX | \$10,000 | 0.00 | \$0 per year |
| CO | \$5,000 | 2.19 | \$10,960 per year |
| VOC | \$9,999 | 0.58 | \$5,778 per year |
| PM (FH+BH) | \$23,200 | 1.33 | \$30,775 per year |
| Total Reasonable Annual Control Cost for Combined Pollutants | | | \$47,513 per year |
| Actual Annual Control Cost | | | \$333,734 per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Acceptable) |

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ATTACHMENT D
UREA-SCR CONTROL SYSTEM
BACT ANALYSIS

**UREA-SCR TECHNICAL DATA AND COST QUOTE
SABEY-INTERGATE-QUINCY DATA CENTER**

PROPOSAL

Proposal Date: **Wednesday, December 08, 2010**

Quotation Number: **10120805RW-E** Revision:

| | |
|---|--|
| Customer Contact: John Ford Title: Director of Technology Real Estate Email: johnf@sabey.com Phone: 206-277-5209 Cell: Company Name: Sabey Corporation Address : 12201 Tukwila International Blvd. Seattle, WA 98168 | Project Description Sabey Construction - CAT 3516C 2000 ekW Generator Address: |
| Product Quoted: | E-POD with ENDURE SCR & ASSURE DOC or PERMIT Filter units in a 304L Stainless Steel Double Wall Insulated Critical Grade Silencer |
| Purchase Order Date: | Requested Installation Date: |

| Engine Specifications: | | CAT | |
|----------------------------------|----------------------------|--------------------------------|------------------|
| Engine Model: | 3516C | Engine S/N: | |
| EPA Tier Level: | Tier 2 | EPA Family #: | |
| Engine Displacement: | 69 liters | Engine Specification #: | DM8263 |
| Fuel Type: | ULSD (<50 PPM) | Engine Model Year: | 2010 |
| Required Fuel Content: | <50 ppm | Sulfur Standby | |
| Generator Power Rating: | 2,000 ekW | Model #: | |
| Average Running Load: | Runtime: | 2188 bkW @ | 1,800 RPM |
| Engine Power Output: | 2,937 bhp or | | |
| Exhaust Flow Rate: | 15,136 ACFM | | |
| Exhaust Stack Temp: | 762 deg F | | |
| Maximum Exhaust Pressure: | 27 inches H ₂ O | | |

| Emissions Specifications: | | | |
|--|----------------------------|--------------------|--|
| Engine Emissions: | Certified | | |
| NOx: | 3.93 g/bhp-hr | | |
| CO: | 0.49 g/bhp-hr | | |
| HC: | 0.25 g/bhp-hr | | |
| PM: | 0.08 g/bhp-hr | | |
| Emissions Reduction Required: | Tier 4 Final Levels | % Reduction | |
| NOx: | 0.50 g/bhp-hr | 87.3% | |
| CO: | 2.60 g/bhp-hr | 44.0% | |
| HC: | 0.14 g/bhp-hr | 75.6% | |
| PM: | 0.02 g/bhp-hr | | <i>Tier 4 Interim PM Level is 0.075 g/bhp-hr</i> |
| Emissions Post After Treatment: | Estimated | % Reduction | |
| NOx: | 0.39 g/bhp-hr | 90.0% | |
| CO: | 0.05 g/bhp-hr | 90.0% | |
| HC: | 0.03 g/bhp-hr | 90.0% | |
| PM with ASSURE DOC Units: | 0.07 g/bhp-hr | 20.0% | <i>Meets Tier 4 Interim w/ASSURE DOCs</i> |
| PM with PERMIT Filter Units: | 0.01 g/bhp-hr | 85.0% | <i>Meets Tier 4 Final w/PERMIT Filters</i> |

ENDURE SCR Specifications:

| | |
|----------------------------------|---|
| NOx Reduction: | 90% |
| Material: | Zeolite based |
| Temperature Range: | 550 to 1,025 deg. F |
| ENDURE SCR Catalyst Part Number: | EAA060612A |
| Total Amount of Catalyst: | 44 cubic feet |
| Number of Catalyst Layers: | 3 layers @ 64 blocks/layer |
| SCR Pressure Drop: | 3.4 inches H ₂ O as configured at rated load |
| Estimated Reductant Consumption: | 5.1 gal/hr of 32.5% Technical Urea @ rated load |
| Estimated Reductant Consumption: | 19.1 liters/hr of 32.5% Technical Urea @ rated load |
| Ammonia Slip: | <10 ppm |
| Catalyst Life Expectancy: | 20,000 hours |

E-POD Control System: *Integrated within the Dosing Cabinet*

- *Touch Screen Display & Dual NOx Sensors for a True Closed-Loop System
- *Controller, Pressure Sensor, Temperature Sensor
- *Power requirement: 240/120 volts AC, 10/20 amps, 50/60 Hertz
- *Records NOx levels pre and post, Temperature and Pressure, Time and Date

Dosing Cabinet: *Included*

- *Housed in a NEMA 4 enclosure (30" tall by 24" wide by 12" deep)
- *Auto Start, Stop and Purge Cycle
- *Dosing Pump
- *Pressure Regulator
- *Secondary Urea / Aqua Ammonia Filter

Tube Bundle: *Included*

- *1/4" Heat Traced Stainless Steel tubing for Urea Flow
- *1/2" Stainless Steel tubing for Compressed Air
- *Signal Wires from Dosing Cabinet to E-POD

Injection and Mixing Section: *Integrated within the E-POD housing*

- Type of Injector: Air/Liquid Lance with Urea
- Compressed Air Required: Yes, 10 SCFM @ 100 PSIG with refrigerated dryer / oil-free
- Mixer: Static

Reductant Supply: *Not Included*

Reductant Supply Pump: *Not Provided & May not be necessary if gravity fed*

Urea Heat Tracing: *Not Provided before the Dosing Cabinet*

Storage Tanks: *Customer Supplied*

Reducing Agent: *Customer Supplied*

**The customer will supply the necessary tanks, plumbing safety equipment, monitoring devices, permitting and all parts and expenses to contain the selected reducing agent and supply the required amount to the Reducing Agent Injection System.*

| ASSURE DOC Specifications: | Option 1 |
|----------------------------|---|
| Material: | Catalyzed Cordierite Ceramic substrates |
| PM Reduction: | ~20% @ steady state |
| CO Reduction: | 90% |
| HC(VOC) Reduction: | 90% |
| ASSURE DOC Part Number: | CBH1250B |
| Amount of Catalyst: | 4.3 cubic ft. 10 DOC units |
| Catalyst Pressure Drop: | 5.1 inches H ₂ O as configured at rated load |
| Regeneration: | Not required |

| PERMIT Filter Specifications: | Option 2 |
|---|---|
| Material: | Catalyzed Cordierite Ceramic wall-flow filter substrates |
| PM Reduction: | 85% <i>CARB Level 3+ verified for greater than 85%</i> |
| CO Reduction: | 90% |
| HC(VOC) Reduction: | 90% |
| PERMIT Filter Part Number: | FDA221 |
| Number of Filters: | 10 |
| Filter Pressure Drop: | 9.2 inches H ₂ O as configured at rated load |
| Regeneration using ULSD: | Above 350 deg C (662 deg F) for 30% of the engine operating time and greater than 40% engine load |
| Maximum Number of Stationary Cold Starts: | 12 consecutive 10 minute idle sessions followed by 2 hrs regeneration |
| Typical Cleaning Interval: | 2,500 hours |
| Catalyst Life Expectancy: | 10,000 hours |

| Silencer Housing Specifications: | 09093003AE |
|--|--|
| Material: | 304L Stainless Steel |
| Construction: | Double Wall, Rigid, & Light Weight |
| Insulation: | 2" Between two Stainless Steel Walls |
| Approximate Dimensions (inches): | 172 " Length 94 " Width 58 " Height |
| Estimated Weight: | 9,000 pounds 4,090 kilograms |
| Sound Reduction: | 27-35 dBa, Critical Grade Silencing |
| Total System Pressure Drop Silencer+SCR+DOC: | 13.5 inches H ₂ O as configured at rated load |
| Total System Pressure Drop Silencer+SCR+DPF: | 17.7 inches H ₂ O as configured at rated load |
| Inlet Size: | 20 inches Flange |
| Outlet Size: | 20 inches Flange |

**The E-POD Silencer Housing is designed to accommodate the ENDURE SCR and either the ASSURE DOC or the PERMIT Filter systems. If not initially purchased, any of these products can be installed at a future date.*

This System Includes:

| | | |
|---|----------|-----------------------------|
| ENDURE SCR Catalyst | Yes | |
| ASSURE DOC | Option 1 | <i>Meets Tier 4 Interim</i> |
| PERMIT DPF | Option 2 | <i>Meets Tier 4 Final</i> |
| SILENCER - Stainless Steel | Yes | |
| INTERNAL Mixing and Reductant Injection | Yes | |
| E-POD Controller | Yes | <i>*Closed-Loop System</i> |
| Operation & Maintenance Manual | Yes | |
| Start-up Commissioning | Yes | |

This System Excludes:

Delivery/Freight Expenses
 Consumables and Utilities (chemicals, water, electricity, etc.)
 Reductant tanks, plumbing, supply pumps, etc.
 Installation and supply of interconnecting power, control cables, and conduit
 Installation of the E-POD System
 Exhaust piping insulation (*CleanAIR Systems recommends insulating the exhaust from the engine to the inlet of the filter*)
 All necessary permitting

Terms & Conditions: *FOB Santa Fe*

Shipping Date: 20 weeks from date of purchase order and approved design
Terms: Net 30 Days
Proposal Valid : 30 days from proposal date
Warranty: 2 year or 8,000 hours of operation from commissioning

Notes:

Pricing:

| <i>Option 1 *Closed-Loop System Meets Tier 4 Interim & Upgradeable to Tier 4 Final</i> | | | | | |
|--|--------------------|--|------------|---------------|---------------------|
| Part Number | Description | Quantity | Unit Price | Total (USD) | |
| 1 | 09093003AE | E-POD w/ ENDURE SCR & ASSURE DOC in a 304L Stainless Steel Double Wall Insulated Critical Grade Silencer | 3 | \$124,915.00 | \$374,745.00 |
| 2 | | Atlas Copco SF-4 Air Compressor (typically 460 Volt/ 3 phase, call for options) | 3 | \$10,450.00 | \$31,350.00 |
| 3 | | | | \$ | - |
| 4 | | | | \$ | - |
| 5 | | | | \$ | - |
| 6 | | | | \$ | - |
| 7 | SCEPD090121 | Commissioning / technician / day (2 days on site)* Please allow 6 weeks to schedule Commissioning | 3 | \$3,025.00 | \$ 49,075.00 |
| 8 | Handling/Skidding: | | | | \$ 4,060.00 |
| 9 | Estimated Freight: | | | | |
| | | | | Total: | \$459,230.00 |

| <i>Option 2 *Closed-Loop System Meets Tier 4 Final</i> | | | | | |
|--|--------------------|---|------------|---------------|---------------------|
| Part Number | Description | Quantity | Unit Price | Total (USD) | |
| 1 | 09093003AE | E-POD w/ ENDURE SCR & PERMIT Filter in a 304L Stainless Steel Double Wall Insulated Critical Grade Silencer | 3 | \$197,658.00 | \$592,975.00 |
| 2 | | Atlas Copco SF-4 Air Compressor (typically 460 Volt/ 3 phase, call for options) | 3 | \$10,450.00 | \$31,350.00 |
| 3 | | | | \$ | - |
| 4 | | | | \$ | - |
| 5 | | | | \$ | - |
| 6 | | | | \$ | - |
| 7 | SCEPD090121 | Commissioning / technician / day (2 days on site)* Please allow 6 weeks to schedule Commissioning | 3 | \$3,025.00 | \$9,075.00 |
| 8 | Handling/Skidding: | | | | \$6,245.00 |
| 9 | Estimated Freight: | | | | |
| | | | | Total: | \$639,645.00 |

| <i>Recommended Optional Equipment:</i> | | | | | |
|--|-------------|--|------------|-------------|--------------|
| Part Number | Description | Quantity | Unit Price | Total (USD) | |
| 1 | 09022405AG | Replacement NOx Sensors (replace every 8,000 hours) | 6 | \$2,420.00 | \$14,520.00 |
| 2 | | ModBus Controller Software upgrade | 3 | \$1,265.00 | \$3,795.00 |
| 3 | | Injector Nozzle Kit | 3 | \$396.00 | \$1,188.00 |
| 4 | | Replacement set of ENDURE SCR Catalyst (20,000 hrs) | 3 | \$27,346.00 | \$82,038.00 |
| 5 | | Replacement set of PERMIT Filter Elements (10,000 hrs) | 3 | \$89,595.00 | \$268,785.00 |
| 6 | | Replacement set of ASSURE DOC Elements (10,000 hrs) | 3 | \$16,850 | \$50,552.00 |
| 7 | | Custom Insulating Blanket for Exhaust Piping | 3 | TBD | #VALUE! |

*Commissioning exceeding 2 days will be charged a flat rate of \$1,150 per day per technician.

Handling/Skidding : 1% of the total order will be charged to prepare the unit for shipping with a \$10 minimum for orders under \$100, \$20 minimum for orders \$101 to \$1000, and a \$30 minimum for orders \$1,001 to \$3,000.

Order Cancellations: **Standard Parts** – A flat 20% fee will be charged on canceled orders for standard parts.

Custom Parts – Customer will incur all expenses at the time of order cancellation including; materials, engineering & labor plus 20%.

Contact Information: N C Power Systems

Don Lee King
Power Generation Sales
425-656-4586
DLKing@ncpowersystems.com

For additional information, visit:

TABLE SCR-1. UREA-SCR NOMINAL CONTROLLED (COLD-START ADJUSTED) EMISSION RATES FOR BACT ANALYSIS

Table X. Nominal-Controlled Cold-Start NOX Emissions Accounting for 3WC Delay Time

| Load | Nominal Uncontrolled NOX, lbs/hr | Minutes SCR Delay | Guaranteed Effic (%) | Nominal Controlled CO, lbs/hr | Minutes Full SCR Control | Nominal Controlled NOX Emission, lbs/hr | Overall Cold Start % NOX Removal |
|-------|----------------------------------|-------------------|----------------------|-------------------------------|--------------------------|---|----------------------------------|
| 10% | 6.0 | 20 | 90% | 0.60 | 40 | 2.40 | 60% |
| 81.3% | 37.2 | 10 | 90% | 3.72 | 50 | 9.29 | 75% |
| 90% | 43.6 | 10 | 90% | 4.36 | 50 | 10.89 | 75% |
| 93.3% | 46.1 | 10 | 90% | 4.61 | 50 | 11.53 | 75% |
| 100% | 51.5 | 10 | 90% | 5.15 | 50 | 12.88 | 75% |

SCR STEADY-STATE REMOVAL EFFICIENCIES

| Pollutant | Removal Effct (%) |
|------------|-------------------|
| Nox | 90% |
| PM (FH+BH) | 20% |
| CO | 90% |
| VOC | 90% |

Table X. Nominal-Controlled (Cold-Start Adjusted) PM Emission Rates (Includes FH+BH Factor)

| Elec Load | Nominal Uncontrolled Front-Half Only Emiss Rate (lbs/hr) | Total PM to Front Half PM Ratio | Nominal Uncontrolled Total PM Emiss Rate (lbs/hr) | Guaranteed Effic (%) | Nominal Contr Total PM (lbs/hr) | Dell 1-Hour Cold Start Factor | Nominal Controlled Total PM, lbs/hr |
|-----------|--|---------------------------------|---|----------------------|---------------------------------|-------------------------------|-------------------------------------|
| 10% | 0.43 | 3.38 | 1.45 | 20% | 1.161 | 1.058 | 1.228 |
| 81.3% | 0.83 | 3.08 | 2.55 | 20% | 2.042 | 1.058 | 2.160 |
| 90% | 0.95 | 3.08 | 2.92 | 20% | 2.337 | 1.058 | 2.473 |
| 93.3% | 0.99 | 3.08 | 3.04 | 20% | 2.435 | 1.058 | 2.577 |
| 100% | 1.08 | 3.00 | 3.24 | 20% | 2.592 | 1.058 | 2.742 |

Total:FH Adjustment Factors

| Load | StacktestTot PM | Stacktes t FH Only PM | Total PM to Front Half PM Ratio |
|---------|-----------------|-----------------------|---------------------------------|
| 80%-90% | | | 3.08 |
| 100% | 0.36 | 0.12 | 3.00 |
| 50% | 0.27 | 0.08 | 3.38 |

Table Y. Nominal-Controlled Cold-Start CO Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Effic (%) | Nominal Controlled CO, lbs/hr | Minutes Full DOC Control | Wtd Average 1-Hour CO Emission, lbs/hr | Cold Start Factor | Nonimal Controlled CO, lbs/hr | Overall Cold Start % CO Removal |
|-------|-----------------------------------|-------------------|----------------------|-------------------------------|--------------------------|--|-------------------|-------------------------------|---------------------------------|
| 10% | 2.8 | 20 | 90% | 0.28 | 40 | 1.12 | 1.058 | 1.18 | 60% |
| 81.3% | 5.3 | 10 | 90% | 0.53 | 50 | 1.33 | 1.058 | 1.40 | 75% |
| 90% | 6.0 | 10 | 90% | 0.60 | 50 | 1.50 | 1.058 | 1.59 | 75% |
| 93.3% | 6.3 | 10 | 90% | 0.63 | 50 | 1.58 | 1.058 | 1.67 | 75% |
| 100% | 6.8 | 10 | 90% | 0.68 | 50 | 1.70 | 1.058 | 1.80 | 75% |

Table Y. Nominal-Controlled Cold-Start VOC Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Effic (%) | Nominal Controlled VOC, lbs/hr | Minutes Full DOC Control | Wtd Average 1-Hour Emission, lbs/hr | Cold Start Factor | Nominal Controlled VOC, lbs/hr | Overall Cold Start % Removal |
|-------|-----------------------------------|-------------------|----------------------|--------------------------------|--------------------------|-------------------------------------|-------------------|--------------------------------|------------------------------|
| 10% | 1.2 | 20 | 90% | 0.12 | 40 | 0.49 | 1.058 | 0.52 | 60% |
| 81.3% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 90% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 93.3% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 100% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |

Table SCR-2. Urea-SCR Nominal-Controlled Facility-Wide Emissions (Basis = ELM's Nominal-Uncontrolled + Cold-Start Factors)

| Gen # | Gen Area | Elec Load | No. Gens | Hours at Each Runtime Mode | | | | | | | | | | Each Genset DPM lbs/hr | Each Genset Fuel Gal/Hr | Each Genset NOX lbs/hr | Facility Wide Total PM Tons/yr | Facility Wide Fuel Gal/Year | Facility Wide NOX Tons/yr | Each Genset CO lbs/hr | Facility Wide CO Tons/Yr | Each Genset HC lbs/hr | Facility Wide VOC Tons/Yr | | | | | | |
|---|----------|-----------|----------|----------------------------|---|---|-----|--------|---------------|------------------|-----------------------|------|--------------|------------------------|-------------------------|------------------------|--------------------------------|--------------------------------------|---------------------------|-----------------------|--------------------------|-----------------------|---------------------------|------|------|-------|-------|-------|--|
| | | | | W | M | Q | A-F | A-Step | Correct Tests | De-En Bldg Maint | Outage or Storm Avoid | Cool | Total hrs/yr | | | | | | | | | | | | | | | | |
| Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | | | | | | | | | | 24 | | 24 | 2.16 | 195 | 9.3 | 0.130 | 23,400 | 0.56 | 1.40 | 0.08 | 0.29 | 0.017 | | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | | | | | | | | | | 24 | | 24 | 2.47 | 213 | 10.89 | 0.089 | 15,336 | 0.39 | 1.59 | 0.06 | 0.29 | 0.010 | | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | | | | | | | | | | 24 | | 24 | 2.47 | 213 | 10.89 | 0.089 | 15,336 | 0.39 | 1.59 | 0.06 | 0.29 | 0.010 | | |
| ETC-1 | ETC | 93% | 1 | | | | | | | | | | | | 24 | | 24 | 2.58 | 220 | 11.53 | 0.031 | 5,280 | 0.14 | 1.67 | 0.02 | 0.29 | 0.003 | | |
| Testing at Full Outage Loads | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | 3 | 6 | | | | | | | | 8 | | 17 | 2.16 | 195 | 9.3 | 0.092 | 16,575 | 0.39 | 1.40 | 0.06 | 0.29 | 0.012 | | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | 3 | 6 | | | | | | | | 8 | | 17 | 2.47 | 213 | 10.89 | 0.063 | 10,863 | 0.28 | 1.59 | 0.04 | 0.29 | 0.007 | | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | 3 | 6 | | | | | | | | 8 | | 17 | 2.47 | 213 | 10.89 | 0.063 | 10,863 | 0.28 | 1.59 | 0.04 | 0.29 | 0.007 | | |
| ETC-1 | ETC | 93% | 1 | | | 3 | 6 | | | | | | | | 8 | | 17 | 2.58 | 220 | 11.53 | 0.022 | 3,740 | 0.10 | 1.67 | 0.01 | 0.29 | 0.002 | | |
| 100% Load | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Testing at 100% Load | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 100% | 5 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.74 | 232 | 12.88 | 0.058 | 9,860 | 0.27 | 1.80 | 0.04 | 0.29 | 0.006 | | |
| 2-1 to 2-3 | Bldg 2 | 100% | 3 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.74 | 232 | 12.88 | 0.035 | 5,916 | 0.16 | 1.80 | 0.02 | 0.29 | 0.004 | | |
| 3-1 to 3-3 | Bldg 3 | 100% | 3 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.74 | 232 | 12.88 | 0.035 | 5,916 | 0.16 | 1.80 | 0.02 | 0.29 | 0.004 | | |
| ETC-1 | ETC | 100% | 1 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.74 | 232 | 12.88 | 0.012 | 1,972 | 0.05 | 1.80 | 0.01 | 0.29 | 0.001 | | |
| 1-6 and 1-7 Reserve | Bldg 1 | 100% | 2 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.74 | 232 | 12.88 | 0.023 | 3,944 | 0.11 | 1.80 | 0.02 | 0.29 | 0.002 | | |
| 2-4 Reserve | Bldg 2 | 100% | 1 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.74 | 232 | 12.88 | 0.012 | 1,972 | 0.05 | 1.80 | 0.01 | 0.29 | 0.001 | | |
| 3-4 Reserve | Bldg 3 | 100% | 1 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.74 | 232 | 12.88 | 0.012 | 1,972 | 0.05 | 1.80 | 0.01 | 0.29 | 0.001 | | |
| ETC-2 Reserve | ETC | 100% | 1 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.74 | 232 | 12.88 | 0.012 | 1,972 | 0.05 | 1.80 | 0.01 | 0.29 | 0.001 | | |
| Idle (set to 10% for emission calculations) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Idle | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 10% | 5 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | | | 35.5 | 1.23 | 45 | 2.40 | 0.109 | 7,988 | 0.21 | 1.18 | 0.11 | 0.52 | 0.046 | | |
| 2-1 to 2-3 | Bldg 2 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | | | 35.5 | 1.23 | 45 | 2.40 | 0.065 | 4,793 | 0.13 | 1.18 | 0.06 | 0.52 | 0.028 | | |
| 3-1 to 3-3 | Bldg 3 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | | | 35.5 | 1.23 | 45 | 2.40 | 0.065 | 4,793 | 0.13 | 1.18 | 0.06 | 0.52 | 0.028 | | |
| ETC-1 | ETC | 10% | 1 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | | | 35.5 | 1.23 | 45 | 2.40 | 0.022 | 1,598 | 0.04 | 1.18 | 0.02 | 0.52 | 0.009 | | |
| 1-6 and 1-7 Reserve | Bldg 1 | 10% | 2 | 20 | 6 | 3 | 6 | | | | | | 8 | 24 | 1.5 | 68.5 | | 68.5 | 1.23 | 45 | 2.40 | 0.084 | 6,165 | 0.16 | 1.18 | 0.08 | 0.52 | 0.036 | |
| 2-4 Reserve | Bldg 2 | 10% | 1 | 20 | 6 | 3 | 6 | | | | | | 8 | 24 | 1.5 | 68.5 | | 68.5 | 1.23 | 45 | 2.40 | 0.042 | 3,083 | 0.08 | 1.18 | 0.04 | 0.52 | 0.018 | |
| 3-4 Reserve | Bldg 3 | 10% | 1 | 20 | 6 | 3 | 6 | | | | | | 8 | 24 | 1.5 | 68.5 | | 68.5 | 1.23 | 45 | 2.40 | 0.042 | 3,083 | 0.08 | 1.18 | 0.04 | 0.52 | 0.018 | |
| ETC-2 Reserve | ETC | 10% | 1 | 20 | 6 | 3 | 6 | | | | | | 8 | 24 | 1.5 | 68.5 | | 68.5 | 1.23 | 45 | 2.40 | 0.042 | 3,083 | 0.08 | 1.18 | 0.04 | 0.52 | 0.018 | |
| | | | | | | | | | | | | | | | | | | Total PM | | NOX | | CO | | VOC | | | | | |
| | | | | | | | | | | | | | | | | | | CONTROLLED Facility-Wide Emissions | | 1.248 | | 169,500 | | 4.38 | | 0.958 | | 0.293 | |
| | | | | | | | | | | | | | | | | | | UNCONTROLLED Facility-Wide Emissions | | 1.56 | | 16.14 | | 3.15 | | 0.870 | | | |
| | | | | | | | | | | | | | | | | | | Tons/Yr Removed | | 0.31 | | 11.76 | | 2.19 | | 0.58 | | | |
| | | | | | | | | | | | | | | | | | | Overall Removal Efficcy, % | | 20% | | 73% | | 70% | | 66% | | | |

Table SCR-3. Urea-SCR BACT Capital Cost (Based on Sabey-Quincy)

Vantage Data Center

| Cost Category | Cost Factor | Source of Cost Factor | Quant. | Unit Cost | Subtotal Cost |
|---|-------------------------|------------------------|--------|-----------|--------------------|
| Direct Costs | | | | | |
| Purchased Equipment Costs | | | | | |
| FOB purchase price for Sabey Data Center's 2000 kWe generators was \$153,000 each. The FOB price for Vantage's 3,000 kWe generators was scaled using the "0.6 rule: Cost for 3,000 kWe units = \$109,700 *(3000/2000) ^{0.6} = \$195,000 each | | | | | |
| Vantage 3000 kWe FOB Purchase Price | Clean Emission Products | CEP | 17 | \$195,000 | \$3,315,000 |
| Instrumentation | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Sales Tax | WA state tax | WA state tax | 6.5% | -- | \$215,475 |
| Shipping | 0.05A | EPA Cost Manual | 5.0% | -- | \$165,750 |
| Subtotal Purchased Equipment Cost, PEC | | | | | \$3,696,225 |
| Direct Installation Costs | | | | | |
| Enclosure structural supports | From MSFT CO-3 | Robinson Enclosures | 0 | \$9,812 | \$0 |
| Installation | EPA Cost Manual | EPA Cost Manual | 5.0% | -- | \$184,811 |
| Electrical | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Piping | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Insulation | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Painting | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Subtotal Direct Installation Costs | | | | | \$184,811 |
| Site Preparation and Buildings (SP) | | | | | |
| Site Preparation and Buildings (SP) | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Total Direct Costs, DC (PEC + Direct Installation + Site Prep) | | | | | \$3,881,036 |
| Indirect Costs (Installation) | | | | | |
| Engineering | 0.025*PEC | 1/4 of EPA Cost Manual | 2.5% | -- | \$92,406 |
| Construction and field expenses | 0.025*PEC | 1/2 of EPA Cost Manual | 2.5% | -- | \$92,406 |
| Contractor Fees | From DIS data center | From DIS data center | 6.8% | -- | \$269,578 |
| Startup | 0.02*PEC | EPA Cost Manual | 2.0% | -- | \$73,925 |
| Performance Test (Tech support) | 0.01*PEC | EPA Cost Manual | 1.0% | -- | \$36,962 |
| Contingencies | 0.03*PEC | EPA Cost Manual | 3.0% | -- | \$110,887 |
| Subtotal Indirect Costs, IC | | | | | \$676,163 |
| Total Capital Investment (TCI = DC+IC) | | | | | \$4,557,199 |
| | | | | | TCI per gen |
| | | | | | \$268,071 |

Table SCR-4. Urea-SCR Nominal-Controlled BACT Cost-Effectiveness

| Item | Quantity | Units | Unit cost | Subtotal |
|---|------------------------|-------|-----------|------------------|
| Annualized Capital Recovery | | | | |
| Total Capital Cost | | | | \$4,557,199 |
| Capital Recovery Factor, 25 yrs, 4% discount rate | | | | 0.06401 |
| Subtotal Annualized 25-year Capital Recovery Cost | | | | \$291,706 |
| Direct Annual Costs | | | | |
| Annual Admin charges | 2% of TCI (EPA Manual) | | 0.02 | \$91,144 |
| Annual Property tax | 1% of TCI (EPA Manual) | | 0.01 | \$45,572 |
| Annual Insurance | 1% of TCI (EPA Manual) | | 0.01 | \$45,572 |
| For this screening-level analysis we assumed the lower-bound annual O&M cost of zero. | | | | \$0 |
| Subtotal Direct Annual Costs | | | | \$182,288 |
| Total Annual Cost (Capital Recovery + Direct Annual Costs) | | | | \$473,994 |
| Uncontrolled emissions (Combined Pollutants) | | | | 21.7 |
| Assumed Control Efficiency | | | | Varies |
| Annual Tons Removed (Combined Pollutants) | | | | 14.84 |
| Cost Effectiveness (\$ per tons combined pollutant destroyed) | | | | \$31,935 |

| Combined Pollutants Removal Tonnages (Nominal-Controlled) | | | | |
|--|-------------|-----------|-----------|----------|
| Pollutant | PM (FH+BH) | CO | VOC | NOX |
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 1.248 | 0.958 | 0.293 | 4.38 |
| Tons Removed/Year | 0.31 | 2.19 | 0.578 | 11.8 |
| Overall Cold-Start Removal Efficacy | 20% | 70% | 66% | 73% |
| Indiv Poll \$/Ton Removed | \$1,518,616 | \$216,240 | \$820,331 | \$40,304 |

Multi-Pollutant Cost-Effectiveness for "Reasonable Control Cost" vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Acceptable Annual Cost (\$/year) |
|---|---------------------------------------|----------------------------|---|
| NOX | \$10,000 | 11.76 | \$117,604 per year |
| CO | \$5,000 | 2.19 | \$10,960 per year |
| VOC | \$9,999 | 0.58 | \$5,778 per year |
| PM (FH+BH) | \$23,200 | 0.31 | \$7,241 per year |
| Total Reasonable Annual Control Cost for Combined Pollutants | | | \$141,583 per year |
| Actual Annual Control Cost | | | \$473,994 per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Acceptable) |

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ATTACHMENT E
3-WAY CATALYST BACT ASSESSMENT

3-WAY CATALYST PERMITTED FOR TITAN DATA CENTER

Clean Emissions Products Inc. Exhaust Purifier

Part Number *FL-35-20ASA 3-WAY x 2*



Basic Catalyst & Housing Composition

- Stainless Steel Foil (Substrate Core)
- Stainless Steel 14 Gauge, Grade 304 (Housing) containing 2 x 35" dia x 3.5" thick 3-way catalysts
- Weight = approx.. 140lbs.
- Dimensions = 35" diameter x 22" total length (approx.) – 20" ASA Flanges
- 320 CPSI
- Pressure drop across catalyst = < 3.9" w.c.

Effectiveness in Reducing Exhaust Emissions

- CO (Carbon Monoxide) up to 99%
- HC (Hydrocarbons & Odor) up to 90%
- Acrolein up to 90%
- DPM (Diesel Particulate Matter) up to 88%
- **NOx Reduction35% guaranteed**

Purchase Prices
 2,000 kW generator: 35" Catalyst; \$56,000
 2,500 kW generator: 35" Catalyst; \$56,000
 Est. installation cost: \$6,500 each catalyst
 Note, these costs do not include indirect costs for shipping, taxes, site-specific engineering, or administrative costs.

Lifespan of Catalyst

- For standby generator sets: Maximum 500 hours per year (**results in an average lifespan of 15 years**).
- For peak shaving gen sets: Maximum 1500 hours per year (**results in an average lifespan of 5 years**).

Installation

- Installs primarily between the muffler and the engine manifold (can be installed directly behind the muffler in most applications).
- The catalyst can be installed either vertically, horizontally or right to left.

Maintenance

- Designed to be maintenance free. Once you install the catalyst on a regularly maintained engine you should not need to maintain the catalyst at all.
- If maintenance is required simply unbolt catalyst and blow out in opposite direction of exhaust flow with high pressure air or water (maximum 1600 psi recommended).

Operating Conditions for Successful Catalyst Use

-Exhaust Temperature must be at least 250° C (482° F) and not exceed 750° C (1382° F). The hotter the exhaust temperature that reaches the catalyst the higher the reduction levels of emissions you will experience.



P.O. Box 271
Midhurst, Ontario
Canada L0L 1X0

TO ORDER CALL
Tel: (705) 739-2225
Fax: (705) 739-9216
Toll Free: 1-866-787-2473

Contact: Brian Cameron



P.O. Box 271
Midhurst, Ontario
Canada L0L 1X0

TO ORDER CALL
Tel: (705) 739-2225
Fax: (705) 739-9216
Toll Free: 1-866-787-2473

Catalyst Reaction Process for P/N FL-35-20ASA-3W

Catalyst Physical Description:

Brazed stainless steel element using 300 CPSI, honeycomb cell pattern.

Catalyst Chemical Description:

NSCR (non-selective catalyst reduction) composed of a Cerium based washcoating with a combination of Platinum (Pt) and Rhodium (Rh) applied.

Exhaust Emission Reductions Targeted:

CO (carbon monoxide) = up to 99%
HC (hydrocarbons) = up to 90%
DPM (diesel particulate matter) = up to 88%
NOx (oxides of nitrogen) = up to 35%

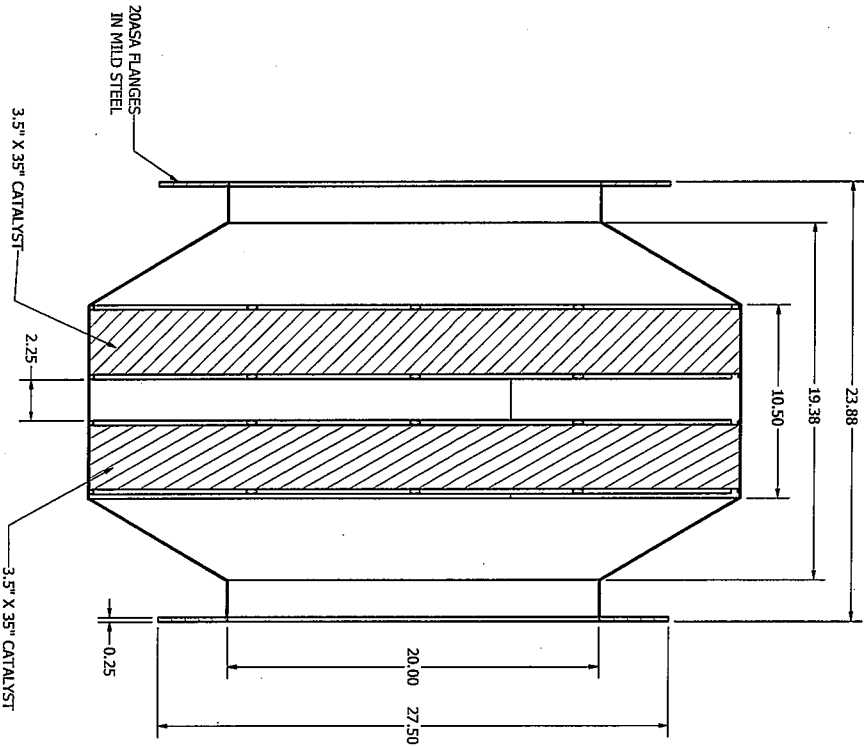
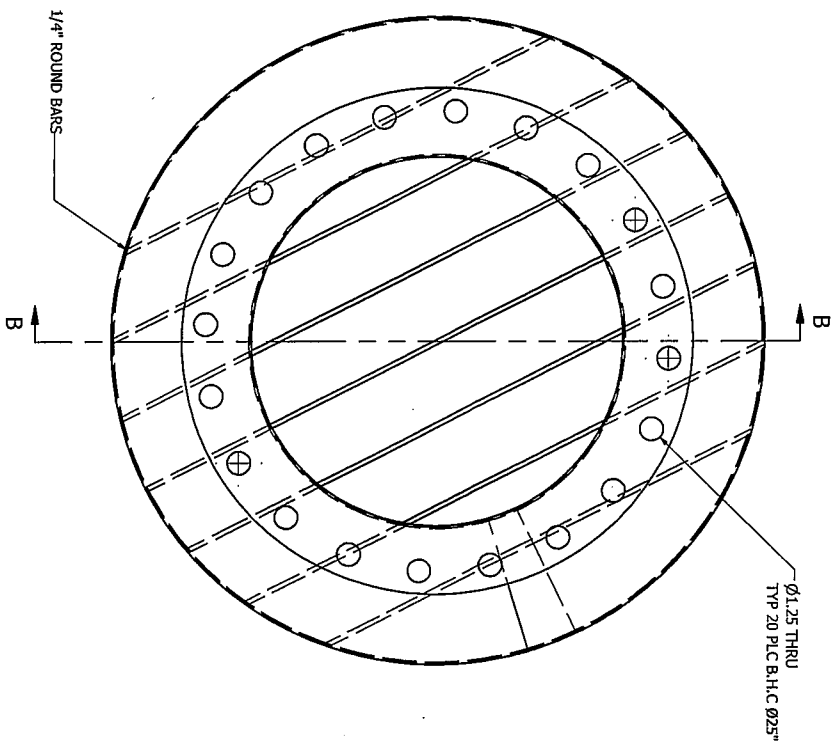
Catalyst Process Description:

With this particular catalyst there are two (2) chemical reactions taking place: **Oxidation** and **Reduction**. With the oxidation reaction oxygen (O_2) is being added to atoms to form oxide molecules. Carbon Monoxide (CO) has additional oxygen added to it to form less lethal carbon dioxide (CO_2). Hydrocarbons (HC) are fuel based molecules comprised of carbon and hydrogen atoms which are then oxidized to form CO_2 and simple water vapor (H_2O). The reduction reaction is one whereby we then remove excess oxygen from the exhaust molecules. NOx is made up of nitrogen (N) and oxygen atoms. When you remove the oxygen you end up with nitrogen gas (N_2).

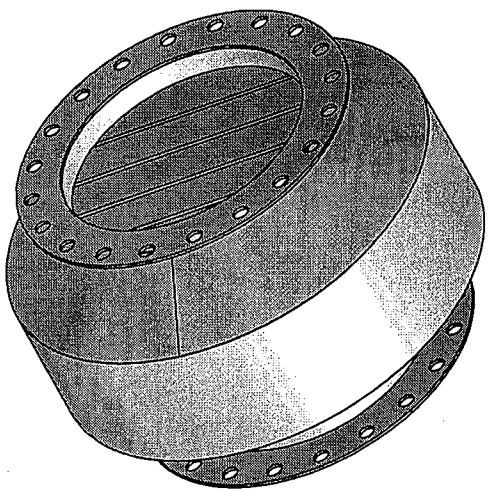
When exhaust gases enter the catalyst the NOx, CO and HC molecules are attracted to the surface of the catalyst where they come into contact with the coating materials of Pt and Rh. Our NSCR catalyst washcoating contains a series of rare earth materials that working in concert with the Rh to have the ability to extract oxygen. This extracted oxygen is then donated to either CO or HC by the reaction with Pt coating.

As this application is a lean burn (diesel) engine we will use the Pt coating in combination with the Rh to remove as much excess oxygen from the exhaust stream (once CO and HC have taken their required molecules to form less lethal CO_2 and water vapor) and then the remaining oxygen deprived environment (stoichiometric) can react with the Rh coating to facilitate NOx reduction (as the remaining exhaust environment will be a rich burn environment which is what is required for NOx reduction).

In addition we use a combination of exhaust backpressure and exhaust temperature to trap and breakdown particulate matter (DPM) which is composed of SOF (soluble organic fraction) and carbon (i.e. soot).



SECTION B-B
SCALE 1:5



MATERIAL: 14GA 304-2B SS

| | | | | |
|----------|----------|-----------|-------------------------------|-----------------|
| DRAWN | M KAMAMI | 3/31/2011 | CLEAN EMISSIONS PRODUCTS INC. | |
| CHECKED | | | TITLE | |
| QA | | | FL35-20ASA-3WAY | |
| MFG | | | SIZE | DWG NO |
| APPROVED | | | C | FL35-20ASA-3WAY |
| | | | SCALE | REV |
| | | | | |

TABLE 3WC-1. 3-WAY CATALYST NOMINAL CONTROLLED (COLD-START ADJUSTED) EMISSION RATES FOR BACT ANALYSIS

Table X. Nominal-Controlled Cold-Start NOX Emissions Accounting for 3WC Delay Time

| Load | Nominal Uncontrolled NOX, lbs/hr | Minutes SCR Delay | Guaranteed Efcy (%) | Nominal Controlled CO, lbs/hr | Minutes Full SCR Control | Nominal Controlled NOX Emission, lbs/hr | Overall Cold Start % NOX Removal |
|-------|----------------------------------|-------------------|---------------------|-------------------------------|--------------------------|---|----------------------------------|
| 10% | 6.0 | 20 | 35% | 3.90 | 40 | 4.60 | 23% |
| 81.3% | 37.2 | 10 | 35% | 24.16 | 50 | 26.33 | 29% |
| 90% | 43.6 | 10 | 35% | 28.32 | 50 | 30.86 | 29% |
| 93.3% | 46.1 | 10 | 35% | 29.99 | 50 | 32.68 | 29% |
| 100% | 51.5 | 10 | 35% | 33.48 | 50 | 36.48 | 29% |

3-WAY CATALYST STEADY-STATE REMOVAL EFFICIENCIES

| Pollutant | Removal Effct (%) |
|------------|-------------------|
| Nox | 35% |
| PM (FH+BH) | 88% |
| CO | 99% |
| VOC | 90% |

Table X. Nominal-Controlled (Cold-Start Adjusted) PM Emission Rates (Includes FH+BH Factor)

| Elec Load | Nominal Uncontrolled Front-Half Only Emiss Rate (lbs/hr) | Total PM to Front Half PM Ratio | Nominal Uncontrolled Total PM Emiss Rate (lbs/hr) | Guaranteed Efcy (%) | Nominal Contr Total PM (lbs/hr) | Dell 1-Hour Cold Start Factor | Nominal Controlled Total PM, lbs/hr |
|-----------|--|---------------------------------|---|---------------------|---------------------------------|-------------------------------|-------------------------------------|
| 10% | 0.43 | 3.38 | 1.45 | 88% | 0.174 | 1.058 | 0.184 |
| 81.3% | 0.83 | 3.08 | 2.55 | 88% | 0.306 | 1.058 | 0.324 |
| 90% | 0.95 | 3.08 | 2.92 | 88% | 0.351 | 1.058 | 0.371 |
| 93.3% | 0.99 | 3.08 | 3.04 | 88% | 0.365 | 1.058 | 0.386 |
| 100% | 1.08 | 3.00 | 3.24 | 88% | 0.389 | 1.058 | 0.411 |

Total:FH Adjustment Factors

| Load | Stacktest Tot PM | Stacktest FH Only PM | Total PM to Front Half PM Ratio |
|---------|------------------|----------------------|---------------------------------|
| 80%-90% | | | 3.08 |
| 100% | 0.36 | 0.12 | 3.00 |
| 50% | 0.27 | 0.08 | 3.38 |

Table Y. Nominal-Controlled Cold-Start CO Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Efcy (%) | Nominal Controlled CO, lbs/hr | Minutes Full DOC Control | Wt. Average 1-Hour CO Emission, lbs/hr | Cold Start Factor | Nominal Controlled CO, lbs/hr | Overall Cold Start % CO Removal |
|-------|-----------------------------------|-------------------|---------------------|-------------------------------|--------------------------|--|-------------------|-------------------------------|---------------------------------|
| 10% | 2.8 | 20 | 99% | 0.03 | 40 | 0.95 | 1.058 | 1.01 | 66% |
| 81.3% | 5.3 | 10 | 99% | 0.05 | 50 | 0.93 | 1.058 | 0.98 | 83% |
| 90% | 6.0 | 10 | 99% | 0.06 | 50 | 1.05 | 1.058 | 1.11 | 83% |
| 93.3% | 6.3 | 10 | 99% | 0.06 | 50 | 1.10 | 1.058 | 1.17 | 83% |
| 100% | 6.8 | 10 | 99% | 0.07 | 50 | 1.19 | 1.058 | 1.26 | 83% |

Table Y. Nominal-Controlled Cold-Start VOC Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Efcy (%) | Nominal Controlled VOC, lbs/hr | Minutes Full DOC Control | Wtd Average 1-Hour Emission, lbs/hr | Cold Start Factor | Nominal Controlled VOC, lbs/hr | Overall Cold Start % Removal |
|-------|-----------------------------------|-------------------|---------------------|--------------------------------|--------------------------|-------------------------------------|-------------------|--------------------------------|------------------------------|
| 10% | 1.2 | 20 | 90% | 0.12 | 40 | 0.49 | 1.058 | 0.52 | 60% |
| 81.3% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 90% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 93.3% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |
| 100% | 1.1 | 10 | 90% | 0.11 | 50 | 0.28 | 1.058 | 0.29 | 75% |

Table 3WC-2. 3-Way Catalyst Nominal-Controlled Facility-Wide Emissions (Basis = ELM's Nominal-Uncontrolled + Cold-Start Factors)

| Gen # | Gen Area | Elec Load | No. Gens | Hours at Each Runtime Mode | | | | | | | | | | Each Genset DPM lbs/hr | Each Genset Fuel Gal/Hr | Each Genset NOX lbs/hr | Facility Wide Total PM Tons/yr | Facility Wide Fuel Gal/Year | Facility Wide NOX Tons/yr | Each Genset CO lbs/hr | Facility Wide CO Tons/yr | Each Genset HC lbs/hr | Facility Wide VOC Tons/yr | | | | | | | | | | | |
|---|----------|-----------|----------|----------------------------|---|---|-----|--------|---------------|------------------|-----------------------|------|--------------|--------------------------------------|-------------------------|------------------------|--------------------------------|-----------------------------|---------------------------|-----------------------|--------------------------|-----------------------|---------------------------|----------|---------|-------|--|-------|--|-------|--|--|--|--|
| | | | | W | M | Q | A-F | A-Step | Correct Tests | De-En Bldg Maint | Outage or Storm Avoid | Cool | Total hrs/yr | | | | | | | | | | | | | | | | | | | | | |
| Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | | Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | | | | | | | 24 | | 24 | 0.32 | 195 | 26.3 | 0.019 | 23,400 | 1.58 | 0.98 | 0.06 | 0.29 | 0.017 | | | | | | | | | | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | | | | | | | 24 | | 24 | 0.37 | 213 | 30.86 | 0.013 | 15,336 | 1.11 | 1.11 | 0.04 | 0.29 | 0.010 | | | | | | | | | | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | | | | | | | 24 | | 24 | 0.37 | 213 | 30.86 | 0.013 | 15,336 | 1.11 | 1.11 | 0.04 | 0.29 | 0.010 | | | | | | | | | | |
| ETC-1 | ETC | 93% | 1 | | | | | | | | | 24 | | 24 | 0.39 | 220 | 32.68 | 0.005 | 5,280 | 0.39 | 1.17 | 0.01 | 0.29 | 0.003 | | | | | | | | | | |
| Testing at Full Outage Loads | | | | | | | | | | | | | | Testing at Full Outage Loads | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | | 3 | 6 | | | | | | 17 | 0.32 | 195 | 26.3 | 0.014 | 16,575 | 1.12 | 0.98 | 0.04 | 0.29 | 0.012 | | | | | | | | | | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | | 3 | 6 | | | | | | 17 | 0.37 | 213 | 30.86 | 0.009 | 10,863 | 0.79 | 1.11 | 0.03 | 0.29 | 0.007 | | | | | | | | | | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | | 3 | 6 | | | | | | 17 | 0.37 | 213 | 30.86 | 0.009 | 10,863 | 0.79 | 1.11 | 0.03 | 0.29 | 0.007 | | | | | | | | | | |
| ETC-1 | ETC | 93% | 1 | | | | 3 | 6 | | | | | | 17 | 0.39 | 220 | 32.68 | 0.003 | 3,740 | 0.28 | 1.17 | 0.01 | 0.29 | 0.002 | | | | | | | | | | |
| 100% Load | | | | | | | | | | | | | | Testing at 100% Load | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 100% | 5 | | | | | | 0.5 | 8 | | | | 8.5 | 0.41 | 232 | 36.48 | 0.009 | 9,860 | 0.78 | 1.26 | 0.03 | 0.29 | 0.006 | | | | | | | | | | |
| 2-1 to 2-3 | Bldg 2 | 100% | 3 | | | | | | 0.5 | 8 | | | | 8.5 | 0.41 | 232 | 36.48 | 0.005 | 5,916 | 0.47 | 1.26 | 0.02 | 0.29 | 0.004 | | | | | | | | | | |
| 3-1 to 3-3 | Bldg 3 | 100% | 3 | | | | | | 0.5 | 8 | | | | 8.5 | 0.41 | 232 | 36.48 | 0.005 | 5,916 | 0.47 | 1.26 | 0.02 | 0.29 | 0.004 | | | | | | | | | | |
| ETC-1 | ETC | 100% | 1 | | | | | | 0.5 | 8 | | | | 8.5 | 0.41 | 232 | 36.48 | 0.002 | 1,972 | 0.16 | 1.26 | 0.01 | 0.29 | 0.001 | | | | | | | | | | |
| 1-6 and 1-7 Reserve | Bldg 1 | 100% | 2 | | | | | | 0.5 | 8 | | | | 8.5 | 0.41 | 232 | 36.48 | 0.003 | 3,944 | 0.31 | 1.26 | 0.01 | 0.29 | 0.002 | | | | | | | | | | |
| 2-4 Reserve | Bldg 2 | 100% | 1 | | | | | | 0.5 | 8 | | | | 8.5 | 0.41 | 232 | 36.48 | 0.002 | 1,972 | 0.16 | 1.26 | 0.01 | 0.29 | 0.001 | | | | | | | | | | |
| 3-4 Reserve | Bldg 3 | 100% | 1 | | | | | | 0.5 | 8 | | | | 8.5 | 0.41 | 232 | 36.48 | 0.002 | 1,972 | 0.16 | 1.26 | 0.01 | 0.29 | 0.001 | | | | | | | | | | |
| ETC-2 Reserve | ETC | 100% | 1 | | | | | | 0.5 | 8 | | | | 8.5 | 0.41 | 232 | 36.48 | 0.002 | 1,972 | 0.16 | 1.26 | 0.01 | 0.29 | 0.001 | | | | | | | | | | |
| Idle (set to 10% for emission calculations) | | | | | | | | | | | | | | Idle | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 10% | 5 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 0.18 | 45 | 4.60 | 0.016 | 7,988 | 0.41 | 1.01 | 0.09 | 0.52 | 0.046 | | | | | | | | | | |
| 2-1 to 2-3 | Bldg 2 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 0.18 | 45 | 4.60 | 0.010 | 4,793 | 0.24 | 1.01 | 0.05 | 0.52 | 0.028 | | | | | | | | | | |
| 3-1 to 3-3 | Bldg 3 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 0.18 | 45 | 4.60 | 0.010 | 4,793 | 0.24 | 1.01 | 0.05 | 0.52 | 0.028 | | | | | | | | | | |
| ETC-1 | ETC | 10% | 1 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 0.18 | 45 | 4.60 | 0.003 | 1,598 | 0.08 | 1.01 | 0.02 | 0.52 | 0.009 | | | | | | | | | | |
| 1-6 and 1-7 Reserve | Bldg 1 | 10% | 2 | 20 | 6 | 3 | 6 | | | | | 8 | 24 | 1.5 | 68.5 | 0.18 | 45 | 4.60 | 0.013 | 6,165 | 0.32 | 1.01 | 0.07 | 0.52 | 0.036 | | | | | | | | | |
| 2-4 Reserve | Bldg 2 | 10% | 1 | 20 | 6 | 3 | 6 | | | | | 8 | 24 | 1.5 | 68.5 | 0.18 | 45 | 4.60 | 0.006 | 3,083 | 0.16 | 1.01 | 0.03 | 0.52 | 0.018 | | | | | | | | | |
| 3-4 Reserve | Bldg 3 | 10% | 1 | 20 | 6 | 3 | 6 | | | | | 8 | 24 | 1.5 | 68.5 | 0.18 | 45 | 4.60 | 0.006 | 3,083 | 0.16 | 1.01 | 0.03 | 0.52 | 0.018 | | | | | | | | | |
| ETC-2 Reserve | ETC | 10% | 1 | 20 | 6 | 3 | 6 | | | | | 8 | 24 | 1.5 | 68.5 | 0.18 | 45 | 4.60 | 0.006 | 3,083 | 0.16 | 1.01 | 0.03 | 0.52 | 0.018 | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | Total PM | | NOX | | CO | | VOC | | | | |
| | | | | | | | | | | | | | | CONTROLLED Facility-Wide Emissions | | | | | | | | | | 0.187 | 169,500 | 11.57 | | 0.739 | | 0.293 | | | | |
| | | | | | | | | | | | | | | UNCONTROLLED Facility-Wide Emissions | | | | | | | | | | 1.56 | | 16.14 | | 3.15 | | 0.870 | | | | |
| | | | | | | | | | | | | | | Tons/Yr Removed | | | | | | | | | | 1.37 | | 4.57 | | 2.41 | | 0.58 | | | | |
| | | | | | | | | | | | | | | Overall Removal Effcy, % | | | | | | | | | | 88% | | 28% | | 77% | | 66% | | | | |

Table 3WC-3. BACT Capital Cost for 3-Way Catalysts (Based on Titan Data Center)

| Vantage Data Center | | | | | |
|--|-------------------------|------------------------------|---------------|------------------|----------------------|
| Cost Category | Cost Factor | Source of Cost Factor | Quant. | Unit Cost | Subtotal Cost |
| Direct Costs | | | | | |
| Purchased Equipment Costs | | | | | |
| FOB purchase price for Titan Data Center's 2000 kWe generators was \$56,000. The FOB price for Vantage's 3,000 kWe generators was scaled using the "0.6 rule": Cost for 3,000 kWe units = \$56,000 *(3000/2000) ^{0.6} = \$71,400 each | | | | | |
| Vantage 3000 kWe FOB Purchase Price | Clean Emission Products | CEP | 17 | \$71,400 | \$1,213,800 |
| Instrumentation | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Sales Tax | WA state tax | WA state tax | 6.5% | -- | \$78,897 |
| Shipping | 0.05A | EPA Cost Manual | 5.0% | -- | \$60,690 |
| Subtotal Purchased Equipment Cost, PEC | | | | | \$1,353,387 |
| Direct Installation Costs | | | | | |
| Enclosure structural supports | From MSFT CO-3 | Robinson Enclosures | 0 | \$9,812 | \$0 |
| Installation | 1/2 of EPA Cost Manual | 1/2 of EPA Cost Manual | 2.5% | -- | \$33,835 |
| Electrical | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Piping | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Insulation | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Painting | Assume no cost | Assume no cost | 0 | 0 | 0 |
| Subtotal Direct Installation Costs | | | | | \$33,835 |
| Site Preparation and Buildings (SP) | | | | | |
| Assume no cost | | | | | |
| Total Direct Costs, DC (PEC + Direct Installation + Site Prep) | | | | | \$1,387,222 |
| Indirect Costs (Installation) | | | | | |
| Engineering | 0.025*PEC | 1/4 of EPA Cost Manual | 2.5% | -- | \$33,835 |
| Construction and field expenses | 0.025*PEC | 1/2 of EPA Cost Manual | 2.5% | -- | \$33,835 |
| Contractor Fees | From DIS data center | From DIS data center | 6.8% | -- | \$110,968 |
| Startup | 0.02*PEC | EPA Cost Manual | 2.0% | -- | \$27,068 |
| Performance Test (Tech support) | 0.01*PEC | EPA Cost Manual | 1.0% | -- | \$13,534 |
| Contingencies | 0.03*PEC | EPA Cost Manual | 3.0% | -- | \$40,602 |
| Subtotal Indirect Costs, IC | | | | | \$259,841 |
| Total Capital Investment (TCI = DC+IC) | | | | | \$1,647,063 |
| | | | | | TCI per gen |
| | | | | | \$96,886 |

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Table 3WC-4. 3-Way Catalyst Nominal-Controlled BACT Cost-Effectiveness

| Item | Quantity | Units | Unit cost | Subtotal |
|---|----------|------------------------|-----------|------------------|
| Annualized Capital Recovery | | | | |
| Total Capital Cost | | | | \$1,647,063 |
| Capital Recovery Factor, 25 yrs, 4% discount rate | | | | 0.06401 |
| Subtotal Annualized 25-year Capital Recovery Cost | | | | \$105,428 |
| Direct Annual Costs | | | | |
| Annual Admin charges | | 2% of TCI (EPA Manual) | 0.02 | \$32,941 |
| Annual Property tax | | 1% of TCI (EPA Manual) | 0.01 | \$16,471 |
| Annual Insurance | | 1% of TCI (EPA Manual) | 0.01 | \$16,471 |
| For this screening-level analysis we assumed the lower-bound annual O&M cost of zero. | | | | \$0 |
| Subtotal Direct Annual Costs | | | | \$65,883 |
| Total Annual Cost (Capital Recovery + Direct Annual Costs) | | | | \$171,311 |
| Uncontrolled emissions (Combined Pollutants) | | | | 21.7 |
| Assumed Control Efficiency | | | | Varies |
| Annual Tons Removed (Combined Pollutants) | | | | 8.94 |
| Cost Effectiveness (\$ per tons combined pollutant destroyed) | | | | \$19,171 |

| | |
|---------|----------|
| TCl/gen | \$96,886 |
|---------|----------|

Combined Pollutants Removal Tonnages (Nominal-Controlled)

| Pollutant | PM (FH+BH) | CO | VOC | NOX |
|-------------------------------------|------------|----------|-----------|----------|
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 0.187 | 0.739 | 0.293 | 11.57 |
| Tons Removed/Year | 1.37 | 2.41 | 0.578 | 4.6 |
| Overall Cold-Start Removal Efficacy | 88% | 77% | 66% | 28% |
| Indiv Poll \$/Ton Removed | \$124,740 | \$71,049 | \$296,484 | \$37,457 |

Multi-Pollutant Cost-Effectiveness for "Reasonable Control Cost" vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Acceptable Annual Cost (\$/year) |
|---|---------------------------------------|----------------------------|---|
| NOX | \$10,000 | 4.57 | \$45,735 per year |
| CO | \$5,000 | 2.41 | \$12,056 per year |
| VOC | \$9,999 | 0.58 | \$5,778 per year |
| PM (FH+BH) | \$23,200 | 1.37 | \$31,861 per year |
| Total Reasonable Annual Control Cost for Combined Pollutants | | | \$95,430 per year |
| Actual Annual Control Cost | | | \$171,311 per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Acceptable) |

G:\Seattle\PNWProjects\PACLAND_-11_Riker Data Center\03_Reports-Analyses\BACT-July-2012\3-way-CEP_Vantage-BACT_July-2012.xls\Vantage capital Cost

ATTACHMENT F
DIESEL OXIDATION CATALYST BACT ASSESSMENT



DIESEL OXIDATION CATALYSTS INSTALLED AT DIS DATA CENTER IN OLYMPIA, WA

| | |
|--|---|
| To: Alex Charlton EC Power (Portland) 1805 NW 21st. Ave Portland, OR 97210 | Phone: 503 220-3536 Fax: 503 224-3907 Email: alexc@e-c-co.com |
| CC: Brett Fuller/MIRATECH Corporation Scott McBryde/MIRATECH Corporation Courtney McAlpine/MIRATECH Corporation | |
| From: David Hammond Renosa Company 608 Joel Palmer Way Dayton, OR 97114 | Phone: 503-864-3952 Fax: 503-864-9282 Email: dhammond@renosacorp.com |

Project Reference: WA DIS
 Proposal Number: REN-10-0695 Rev(4)
 Date: 6/21/2010
 Firm Quote For: 30 days from Proposal Date

(\$22,128 including shipping)
 Not including:
 • Taxes
 • Installation
 • Commissioning
 • Vendor Support

Dear Alex:

MIRATECH Corporation welcomes the opportunity to provide you with a proposal for an NSCR system. We are confident that your organization will benefit from selecting us for this project for the following reasons:

- **Experience.**
 - MIRATECH is the leader in providing NSCR, SCR & DPF systems; having more than 17,000 successfully operating units installed in North America, South America, Europe and Asia.
- **World-Class Technology.**
 - Consistently set the standards for Best Available Control Technology (BACT)
 - Simple, user-friendly control and communication technology; connects to any building's communication systems
- **U.S.-based Field Services & Support.**
 - Fast-response field service & technical support
 - Replacement components in stock in Tulsa, Oklahoma
 - In-house engineering & product support

The system offered for this project is in accordance with the data received or estimated from your company. The system is designed to provide emission reduction for carbon monoxide (CO), hydrocarbons (NMHC), and particulate matter (PM) as listed on the System Specifications and Performance Warranty Data page. MIRATECH warrants the quoted performance based on the engine emission and operating data you have provided us and that is contained in this proposal. Please note that some engine assumptions were used and converter size may change based on actual engine data.

Once again, thank you for the opportunity to provide this proposal. If you have any questions, please do not hesitate to contact me. I will call you next week to confirm your receipt and satisfaction with this proposal.

Best Regards,

David Hammond
 Renosa Company
 Renosa Company

Original Proposal By: Brett Fuller/MIRATECH Corporation

Scope of Supply

MIRATECH Corporation Scope of Supply

| | Model Number | Quantity per Engine |
|------------------------------------|------------------------|---------------------|
| NSCR Housing & Catalyst | SP-IQ-30-24-EL2 | 1 |
| NSCR Housing | SP-IQ-30-24-HSG | 1 |
| Oxidation Catalyst | IQ-RE-30EL | 2 |
| Nut, Bolt, and Gasket Set | NBG-IQ30-2 | 1 |

Customer Scope of Supply

| Description |
|---|
| Support Structure |
| Attachment to Support Structure (Bolts, Nuts, Levels, etc.) |
| Expansion Joints |
| Exhaust Piping |
| Inlet Pipe Bolts, Nuts, & Gasket |
| Outlet Pipe Bolts, Nuts, & Gasket |

Application Data

Project Information

Site Location: Olympia
 Project Name: WA DIS
 Application: Standby Power
 Number of Engines: 5
 Operating Hours per Year: 200

Engine Specifications

Engine Manufacturer: MTU
 Model Number: 20V4000G43
 Operating Load for Engine Data Provided: 100%
 Power Output: 3,675 bhp
 Speed: 1,800 RPM
 Type of Fuel: Number 2 Diesel
 Sulfur Content: 500 ppmv or less
 Fuel Consumption: 6,000 BTU/bhp-hr
 Type of Lube Oil: 1.0 wt%
 Lube Oil Consumption: < 0.00027 gal/bhp-hr
 Exhaust Flow Rate: 20,553 acfm (cfm)
 Exhaust Temperature: 878°F

Raw Engine Emission Data

| | g/bhp-hr | lb/MW-hr | ppmv | ppmv @ 15% O ₂ | lb/hr | g/kW-hr | tons/yr |
|------------------|----------|----------|-------|---------------------------|-------|---------|---------|
| CO | 0.45 | 1.32 | 117 | 63 | 3.62 | 0.60 | 0.36 |
| NMHC | 1.06 | 3.13 | 484 | 262 | 8.58 | 1.42 | 0.86 |
| PM ₁₀ | 0.13 | 0.37 | 77.43 | 41.91 | 1.03 | 0.17 | 0.10 |

% O₂ 10.0
 H₂O Assumption 12.5

System Specifications and Performance Warranty Data

NSCR System Specifications (SP-IQ-30-24-EL2)

Design Exhaust Flow Rate: 20,553 acfm (cfm)
 Design Exhaust Temperature*: 878°F
 System Pressure Loss: 11.0 inches of WC (Fresh)
 Exhaust Temperature Limits: 550 – 1250°F (catalyst inlet); 1350°F (catalyst outlet)

Post System Emission Data

| | g/bhp-hr | lb/MW-hr | ppmv | ppmv @ 15% O ₂ | lb/hr | g/kW-hr | tons/yr |
|------------------|----------|----------|------|---------------------------|-------|---------|---------|
| CO | 0.04 | 0.13 | 12 | 6 | 0.36 | 0.06 | 0.04 |
| NMHC | 0.42 | 1.25 | 194 | 105 | 3.43 | 0.57 | 0.34 |
| PM ₁₀ | 0.10 | 0.28 | 58 | 31 | 0.77 | 0.13 | 0.08 |

Calculated Percent Reductions

| | % Reduction |
|------|-------------|
| CO | 90.0 |
| NMHC | 60.0 |
| PM10 | 25.0 |

| |
|------|
| co |
| nmhc |
| pm |

Equipment Details

NSCR Housing & Catalyst Details (SP-IQ-30-24-EL2)

NSCR Housing Details

- | | |
|----------------------------------|--|
| | IQ-30-20 SD |
| • Model Number: | SP-IQ-30-24-HSG |
| • Quantity ² : | 1 |
| • Material: | Carbon Steel |
| • Paint: | Standard High Temperature Black Paint |
| • Diameter: | 30 inches |
| • Inlet Pipe Size & Connection: | 24 inch FF Flange, 150# ANSI standard bolt pattern |
| • Outlet Pipe Size & Connection: | 24 inch FF Flange, 150# ANSI standard bolt pattern |
| • Overall Length: | 53 inches |
| • Weight Without Catalyst: | 472 lbs |
| • Weight Including Catalyst: | 602 lbs |
| • Instrumentation Ports: | 2 inlet/2 outlet (1/2" NPT) |
| • Oxygen Sensor Ports: | 1 inlet/1 outlet (18mm) |

Oxidation Catalyst Details

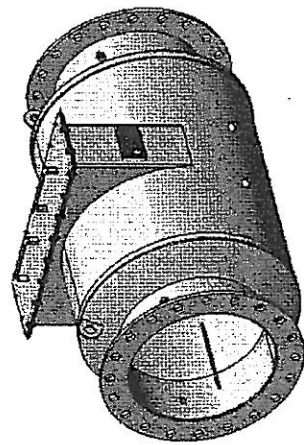
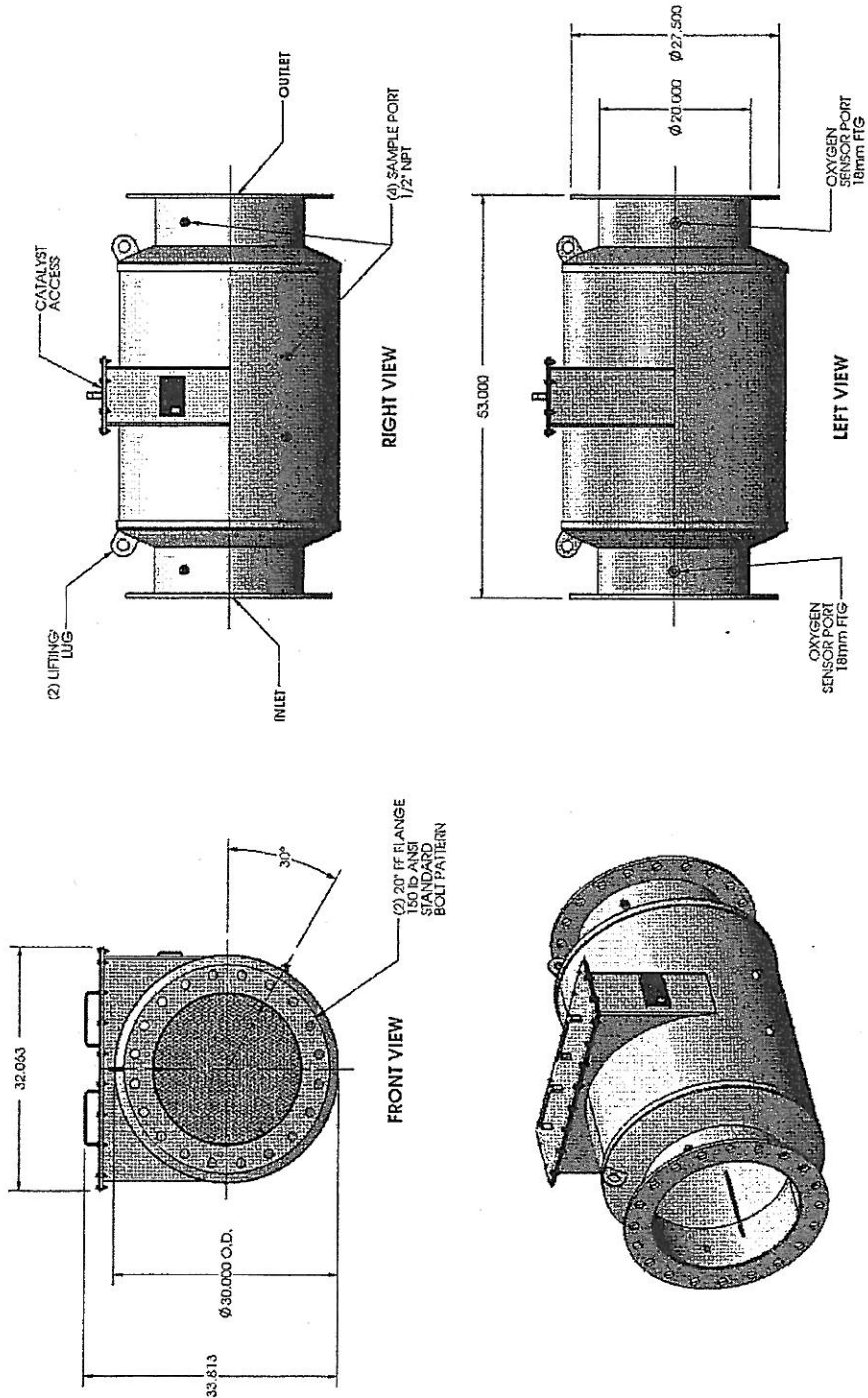
- | | |
|---------------------------|------------|
| • Model Number: | IQ-RE-30EL |
| • Quantity ² : | 2 |

Nut, Bolt, and Gasket Set Details

- | | |
|---------------------------|------------|
| • Model Number: | NBG-IQ30-2 |
| • Quantity ² : | 1 |

Special Notes/Conditions

- 1 Carbon steel housings are suitable for use in all applications where the housing will not be insulated. Carbon steel housings may only be insulated in applications where the exhaust temperature does not exceed 900°F. If your application requires insulation with an engine exhaust temperature exceeding 900°F, a stainless steel housing is required. Customer installed insulation on carbon steel housings in applications where exhaust temperature exceeds 900°F voids any MIRATECH product warranty.
 - 2 Quantities are per engine.
- MIRATECH does not allow any silencer, packed or unpacked, to be installed upstream of any MIRATECH equipment. Installation of such equipment will void the warranty per MIRATECH Holdings Terms and Conditions.
 - Final catalyst housings are dependent on engine output and required emission reductions. Changes may be made to optimize the system design at the time of order.
 - Any drawings included with this proposal are preliminary in nature and could change depending on final product selection.



IQ-30-20
Sales Drawing

DIMENSIONS ARE APPROXIMATE IN INCHES UNLESS OTHERWISE SPECIFIED
 DO NOT SCALE DRAWING
 DRAWN: JCU DATE: 12/29/2009
 REVIEWED BY: JMS DATE: 12/29/2009

PROPRIETARY AND CONFIDENTIAL
 THE INFORMATION CONTAINED IN THIS DRAWING IS THE SOLE PROPERTY OF MIRATECH CORPORATION. ANY REPRODUCTION IN PART OR AS A WHOLE WITHOUT THE WRITTEN PERMISSION OF MIRATECH CORPORATION IS PROHIBITED.

PROJECT NAME _____
 SALES ORDER NO. _____
 FABRICATION P.O. _____

MATERIAL CONSTRUCTION:
 - CARBON STEEL

| | | |
|---------|-------------|-----------------------------|
| REV | 1 | SHEET 1 OF 1 |
| DRAWING | IQ-30-20 SD | WEIGHT: 485 Lb FULLY LOADED |
| SCALE | 1:2 | |
| SITE | A | |



Domestic Onshore Technical Service Rate Schedule

The Day Rate is charged for supervision of work performed over and above the scope of an installation or services contract. MIRATECH standard Terms and Conditions of Sale apply to all activities.

Technical Services Supervisor Day Rate **\$1,200.00**

Additional Information

- **The standard Day Rate is for an 8-hour, onshore, non-holiday, weekday and is the minimum charge.**
- **Charges for greater than 8 hours but less than 12 hours in a single calendar day** - The number of hours of supervision in a single calendar day divided by 8 and multiplied by the standard Day Rate times any applicable multipliers for Weekends and Holidays (see below). (example - 10 hours of supervision in a single day - $10/8 \times \$1,200 = \$1,500$)
- **Charges for greater than 12 hours per day** - Actual time worked over 12 hours per day will be charged at a rate of \$225.00 per hours or 1.5 times the calculated hourly rate, which ever is greatest.
- **Travel Time** - actual hours traveled each way divided by 8 and multiplied by the standard Day Rate. No multipliers are applicable. (example - 5 hours traveled to site - $5/8 \times \$1,200 = \750)
- **Saturday** - 1.5 times the standard Day Rate
- **Sundays** - 2 times the standard Day Rate
- **All National Holidays** - 3 times the standard Day Rate

Expense Invoicing Rates

MIRATECH Actual Cost plus 5% - Lodging, phone, meals, parking, air travel, rental cars and incidental costs.

| | |
|------------------------------------|-------------------------------|
| Company Vehicle Mileage at: | \$ 1.00 per mile |
| Portable Exhaust Gas Analyzer | \$ 400.00/calendar day |
| Special Tools and Equipment rental | cost plus 15% |

420 S. 145th E. Avenue, Mail Drop A, Tulsa, OK 74108-1305
Phone Number (800) 640-3141 FAX Number (918) 622-3928
www.MIRATECHcorp.com

MIRATECH Onshore Technical Service Day Rate Sheet date January 2009

ACTUAL COSTS TO INSTALL DOCs AT
OLYMPIA DATA CENTER, 2010

WRIGHT
RUNSTAD
& COMPANY

PRINCIPALS:
H. JON RUNSTAD
GREGORY K. JOHNSON
WALTER R. INGRAM

December 17, 2010

Sally Alhadeff
Department of Information Services, Director's Office
1110 Jefferson Street SE
P.O. Box 42445
Olympia, WA 98504

TOTAL INSTALLED COST =
\$306,222 for 5 gensets =
\$61,200 each genset (2,500 kWe)

**DIS - WHEELER PROJECT
CHANGE ORDER #24
DIESEL OXYDATION CATALYSTS
@ UTILITY BUILDING**

Dear Sally:

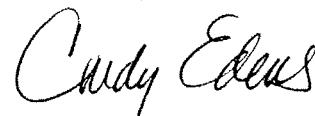
Attached is Change Order #24 for your approval. The purpose of this change order is to add the Diesel Oxydation Catalysts at the generators for the Data Center in accordance with the attached proposal as required by ORCAA.

The total cost for this additional work is \$306,222 and it will not impact the schedule.

If you find everything in order, please sign the attached Change Order and return one original for my files.

Please feel free to contact me with any questions or concerns.

Very truly yours,



Cindy Edens
Senior Vice President

CE/sg

Enclosures

DIS – Wheeler Project
Tenant Change Order #24
12/17/2010

TENANT CHANGE ORDER #24

Description: Diesel Oxydation Catalysts @ Utility Building


Cost Summary:

| | |
|--------------------|---------------------|
| Construction Costs | \$ 268,793 |
| Sales Tax | \$ 22,847 |
| | Subtotal \$ 291,640 |
| Developer's Fee | \$ 14,582 |
| TOTAL | \$ 306,222 |

Total Delay for Tenant Change Order #24 **No Impact**

Please sign below approving the total cost of \$306,222 for this additional work.

APPROVED BY:



Facilities Development Manager
Department of Information Services

12/21/2010

Date

Proposal Description: Provide Diesel Oxydation Catalysts at the generators for the Data Center.

Proposal Date: 11/2/10

PCO NUMBER: DCSC-0134

| Item | Qty | UNITS | Hours per Unit | Units per Hour | MH | Labor Rate | Cost | Mat U.P. | Cost | Sub U.P. | Cost | Extended Totals | Division Totals |
|--|-----|-------|----------------|----------------|----|------------|------|----------|------|----------|---------|-----------------|-----------------|
| GENERAL CONDITIONS / GENERAL REQUIREMENTS | | | | | | | | | | | | | |
| Project Staff: | | | | | | | | | | | | | 0 |
| Sr. Project Mgr | 0 | MH | 1.0000 | 1.00 | 0 | 93 | 0 | | 0 | | 0 | 0 | |
| Project Mgr | 0 | MH | 1.0000 | 1.00 | 0 | 93 | 0 | | 0 | | 0 | 0 | |
| Project Engr | 0 | MH | 1.0000 | 1.00 | 0 | 93 | 0 | | 0 | | 0 | 0 | |
| BIM Detailing / MEP Coordination | 0 | MH | 1.0000 | 1.00 | 0 | 93 | 0 | | 0 | | 0 | 0 | |
| Project Supt. | | MH | 1.0000 | 1.00 | 0 | 93 | 0 | | 0 | | 0 | 0 | |
| Foreman | | MH | 1.0000 | 1.00 | 0 | 93 | 0 | | 0 | | 0 | 0 | |
| Temporary Protection & Safety | | MH | 1.0000 | 1.00 | 0 | 93 | 0 | | 0 | | 0 | 0 | |
| Layout / Field Engineering | | MHz | 1.0000 | 1.00 | 0 | 93 | 0 | | 0 | | 0 | 0 | |
| Cleanup | | MH | 1.0000 | 1.00 | 0 | 93 | 0 | | 0 | | 0 | 0 | |
| Disposal / Dump Fee's / Eco Pans | | EA | 1.0000 | 1.00 | 0 | 93 | 0 | | 0 | | 0 | 0 | |
| HSW DIRECT FIELD LABOR | | | | | | | | | | | | | |
| | | | | | 0 | | 0 | | 0 | | 0 | 0 | 0 |
| SUBCONTRACTORS | | | | | | | | | | | | | |
| UMCI - Install DOC's | 5 | ea | | | 0 | | 0 | | 0 | 5,476 | 27,378 | 27,378 | |
| UMCI - Store fabricated sound traps | 1 | ls | | | 0 | | 0 | | 0 | 67,114 | 67,114 | 67,114 | |
| EC - Provide DOC's w/ Insulating blankets | 5 | ea | | | 0 | | 0 | | 0 | 31,543 | 157,717 | 157,717 | |
| | | | | | 0 | | 0 | | 0 | | 0 | 0 | |
| | | | | | 0 | | 0 | | 0 | | 0 | 0 | |
| | | | | | 0 | | 0 | | 0 | | 0 | 0 | |
| | | | | | 0 | | 0 | | 0 | | 0 | 0 | |
| | | | | | 0 | | 0 | | 0 | | 0 | 0 | |
| Totals | | | | | 0 | | 0 | | 0 | | 252,209 | 252,209 | 252,209 |

Total Direct

0 MH

| | | |
|---------------------|-------|----------------|
| Subguard | 1.05% | 2,648 |
| Liability Insurance | 1.00% | 2,549 |
| Excise - B & O Tax | 0.57% | 1,470 |
| Bond | 0.66% | 1,709 |
| Overhead & Profit | 3.15% | 8,208 |
| SUB - TOTAL | | 268,793 |
| Contingency | 0.00% | 0 |

Proposal Total \$268,793

Qualifications:

- 1) WSST is not included
- 2) Proposal is valid for 10 days from when it is submitted.
- 3) No structural modifications are anticipated to be needed, therefore none are included.
- 4) Costs for storing the generator sound traps is included since this equipment had to be stored 6-7 months longer than anticipated due to the emissions permit delay.

TABLE DOC-1. DOC NOMINAL CONTROLLED (COLD-START ADJUSTED) EMISSION RATES FOR BACT ANALYSIS

Miratech Model SP-IQ-30-24-EL2 used at DIS Data Center

Table X. Nominal-Controlled Cold-Start NOX Emissions Accounting for 3WC Delay Time

| Load | Nominal Uncontrolled NOX, lbs/hr | Minutes SCR Delay | Guaranteed Effic (%) | Nominal Controlled CO, lbs/hr | Minutes Full SCR Control | Nominal Controlled NOX Emission, lbs/hr | Overall Cold Start % NOX Removal |
|-------|----------------------------------|-------------------|----------------------|-------------------------------|--------------------------|---|----------------------------------|
| 10% | 6.0 | 20 | 0% | 6.00 | 40 | 6.00 | 0% |
| 81.3% | 37.2 | 10 | 0% | 37.17 | 50 | 37.17 | 0% |
| 90% | 43.6 | 10 | 0% | 43.57 | 50 | 43.57 | 0% |
| 93.3% | 46.1 | 10 | 0% | 46.14 | 50 | 46.14 | 0% |
| 100% | 51.5 | 10 | 0% | 51.50 | 50 | 51.50 | 0% |

Miratech DOC STEADY-STATE REMOVAL EFFICIENCIES

| Pollutant | Removal Effct (%) |
|------------|-------------------|
| Nox | 0% |
| PM (FH+BH) | 25% |
| CO | 90% |
| VOC | 60% |

Table X. Nominal-Controlled (Cold-Start Adjusted) PM Emission Rates (Includes FH+BH Factor)

| Elec Load | Nominal Uncontrolled Front-Half Only Emiss Rate (lbs/hr) | Total PM to Front Half PM Ratio | Nominal Uncontrolled Total PM Emiss Rate (lbs/hr) | Guaranteed Effic (%) | Nominal Contr Total PM (lbs/hr) | Dell 1-Hour Cold Start Factor | Nominal Controlled Total PM, lbs/hr |
|-----------|--|---------------------------------|---|----------------------|---------------------------------|-------------------------------|-------------------------------------|
| 10% | 0.43 | 3.38 | 1.45 | 25% | 1.088 | 1.058 | 1.152 |
| 81.3% | 0.83 | 3.08 | 2.55 | 25% | 1.914 | 1.058 | 2.025 |
| 90% | 0.95 | 3.08 | 2.92 | 25% | 2.191 | 1.058 | 2.318 |
| 93.3% | 0.99 | 3.08 | 3.04 | 25% | 2.283 | 1.058 | 2.416 |
| 100% | 1.08 | 3.00 | 3.24 | 25% | 2.430 | 1.058 | 2.571 |

Total:FH Adjustment Factors

| Load | Stacktest Tot PM | Stacktest t FH Only PM | Total PM to Front Half PM Ratio |
|---------|------------------|------------------------|---------------------------------|
| 80%-90% | | | 3.08 |
| 100% | 0.36 | 0.12 | 3.00 |
| 50% | 0.27 | 0.08 | 3.38 |

Table Y. Nominal-Controlled Cold-Start CO Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Effic (%) | Nominal Controlled CO, lbs/hr | Minutes Full DOC Control | Wt. Average 1-Hour CO Emission, lbs/hr | Cold Start Factor | Nonimal Controlled CO, lbs/hr | Overall Cold Start % CO Removal |
|-------|-----------------------------------|-------------------|----------------------|-------------------------------|--------------------------|--|-------------------|-------------------------------|---------------------------------|
| 10% | 2.8 | 20 | 90% | 0.28 | 40 | 1.12 | 1.058 | 1.18 | 60% |
| 81.3% | 5.3 | 10 | 90% | 0.53 | 50 | 1.33 | 1.058 | 1.40 | 75% |
| 90% | 6.0 | 10 | 90% | 0.60 | 50 | 1.50 | 1.058 | 1.59 | 75% |
| 93.3% | 6.3 | 10 | 90% | 0.63 | 50 | 1.58 | 1.058 | 1.67 | 75% |
| 100% | 6.8 | 10 | 90% | 0.68 | 50 | 1.70 | 1.058 | 1.80 | 75% |

Table Y. Nominal-Controlled Cold-Start VOC Emissions Accounting for DOC Delay Time

| Load | Nominal Uncontrolled Rate, lbs/hr | Minutes DOC Delay | Guaranteed Effic (%) | Nominal Controlled VOC, lbs/hr | Minutes Full DOC Control | Wtd Average 1-Hour Emission, lbs/hr | Cold Start Factor | Nominal Controlled VOC, lbs/hr | Overall Cold Start % Removal |
|-------|-----------------------------------|-------------------|----------------------|--------------------------------|--------------------------|-------------------------------------|-------------------|--------------------------------|------------------------------|
| 10% | 1.2 | 20 | 60% | 0.49 | 40 | 0.74 | 1.058 | 0.78 | 40% |
| 81.3% | 1.1 | 10 | 60% | 0.44 | 50 | 0.55 | 1.058 | 0.58 | 50% |
| 90% | 1.1 | 10 | 60% | 0.44 | 50 | 0.55 | 1.058 | 0.58 | 50% |
| 93.3% | 1.1 | 10 | 60% | 0.44 | 50 | 0.55 | 1.058 | 0.58 | 50% |
| 100% | 1.1 | 10 | 60% | 0.44 | 50 | 0.55 | 1.058 | 0.58 | 50% |

Table DOC-2. DOC Nominal-Controlled Facility-Wide Emissions (Basis = Miratch DOC; ELM's Nominal-Uncontrolled + Cold-Start Factors)

| Gen # | Gen Area | Elec Load | No. Gens | Hours at Each Runtime Mode | | | | | | | | | | Each Genset DPM lbs/hr | Each Genset Fuel Gal/Hr | Each Genset NOX lbs/hr | Facility Wide Total PM Tons/yr | Facility-Wide Fuel Gal/Year | Facility Wide NOX Tons/yr | Each Genset CO lbs/hr | Facility-Wide CO Tons/Yr | Each Genset HC lbs/hr | Facility-Wide VOC Tons/Yr | | | | | | |
|---|----------|-----------|----------|----------------------------|---|---|-----|--------|---------------|------------------|-----------------------|------|--------------|------------------------|-------------------------|------------------------|--------------------------------------|-----------------------------|---------------------------|-----------------------|--------------------------|-----------------------|---------------------------|-------|------|------|-------|------|-------|
| | | | | W | M | Q | A-F | A-Step | Correct Tests | De-En Bldg Maint | Outage or Storm Avoid | Cool | Total hrs/yr | | | | | | | | | | | | | | | | |
| Unplanned Outage + Storm Avoidance | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | | | | | | | | | | 24 | | 24 | 2.03 | 195 | 37.2 | 0.122 | 23,400 | 2.23 | 1.40 | 0.08 | 0.58 | 0.035 | | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | | | | | | | | | | 24 | | 24 | 2.32 | 213 | 43.57 | 0.083 | 15,336 | 1.57 | 1.59 | 0.06 | 0.58 | 0.021 | | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | | | | | | | | | | 24 | | 24 | 2.32 | 213 | 43.57 | 0.083 | 15,336 | 1.57 | 1.59 | 0.06 | 0.58 | 0.021 | | |
| ETC-1 | ETC | 93% | 1 | | | | | | | | | | | | 24 | | 24 | 2.42 | 220 | 46.14 | 0.029 | 5,280 | 0.55 | 1.67 | 0.02 | 0.58 | 0.007 | | |
| Testing at Full Outage Loads | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Testing at Full Outage Loads | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 81% | 5 | | | 3 | 6 | | | | | | | | | | 17 | 2.03 | 195 | 37.2 | 0.086 | 16,575 | 1.58 | 1.40 | 0.06 | 0.58 | 0.025 | | |
| 2-1 to 2-3 | Bldg 2 | 90% | 3 | | | 3 | 6 | | | | | | | | | | 17 | 2.32 | 213 | 43.57 | 0.059 | 10,863 | 1.11 | 1.59 | 0.04 | 0.58 | 0.015 | | |
| 3-1 to 3-3 | Bldg 3 | 90% | 3 | | | 3 | 6 | | | | | | | | | | 17 | 2.32 | 213 | 43.57 | 0.059 | 10,863 | 1.11 | 1.59 | 0.04 | 0.58 | 0.015 | | |
| ETC-1 | ETC | 93% | 1 | | | 3 | 6 | | | | | | | | | | 17 | 2.42 | 220 | 46.14 | 0.021 | 3,740 | 0.39 | 1.67 | 0.01 | 0.58 | 0.005 | | |
| 100% Load | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Testing at 100% Load | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 100% | 5 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.57 | 232 | 51.50 | 0.055 | 9,860 | 1.09 | 1.80 | 0.04 | 0.58 | 0.012 | | |
| 2-1 to 2-3 | Bldg 2 | 100% | 3 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.57 | 232 | 51.50 | 0.033 | 5,916 | 0.66 | 1.80 | 0.02 | 0.58 | 0.007 | | |
| 3-1 to 3-3 | Bldg 3 | 100% | 3 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.57 | 232 | 51.50 | 0.033 | 5,916 | 0.66 | 1.80 | 0.02 | 0.58 | 0.007 | | |
| ETC-1 | ETC | 100% | 1 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.57 | 232 | 51.50 | 0.011 | 1,972 | 0.22 | 1.80 | 0.01 | 0.58 | 0.002 | | |
| 1-6 and 1-7 Reserve | Bldg 1 | 100% | 2 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.57 | 232 | 51.50 | 0.022 | 3,944 | 0.44 | 1.80 | 0.02 | 0.58 | 0.005 | | |
| 2-4 Reserve | Bldg 2 | 100% | 1 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.57 | 232 | 51.50 | 0.011 | 1,972 | 0.22 | 1.80 | 0.01 | 0.58 | 0.002 | | |
| 3-4 Reserve | Bldg 3 | 100% | 1 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.57 | 232 | 51.50 | 0.011 | 1,972 | 0.22 | 1.80 | 0.01 | 0.58 | 0.002 | | |
| ETC-2 Reserve | ETC | 100% | 1 | | | | | 0.5 | 8 | | | | | | | | 8.5 | 2.57 | 232 | 51.50 | 0.011 | 1,972 | 0.22 | 1.80 | 0.01 | 0.58 | 0.002 | | |
| Idle (set to 10% for emission calculations) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Idle | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 1-1 to 1-5 | Bldg 1 | 10% | 5 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 1.15 | 45 | 6.00 | 0.102 | 7,988 | 0.53 | 1.18 | 0.11 | 0.78 | 0.069 | | |
| 2-1 to 2-3 | Bldg 2 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 1.15 | 45 | 6.00 | 0.061 | 4,793 | 0.32 | 1.18 | 0.06 | 0.78 | 0.042 | | |
| 3-1 to 3-3 | Bldg 3 | 10% | 3 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 1.15 | 45 | 6.00 | 0.061 | 4,793 | 0.32 | 1.18 | 0.06 | 0.78 | 0.042 | | |
| ETC-1 | ETC | 10% | 1 | 20 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9.5 | 35.5 | 1.15 | 45 | 6.00 | 0.020 | 1,598 | 0.11 | 1.18 | 0.02 | 0.78 | 0.014 | | |
| 1-6 and 1-7 Reserve | Bldg 1 | 10% | 2 | 20 | 6 | 3 | 6 | | | | | | | | | 8 | 24 | 1.5 | 68.5 | 1.15 | 45 | 6.00 | 0.079 | 6,165 | 0.41 | 1.18 | 0.08 | 0.78 | 0.053 |
| 2-4 Reserve | Bldg 2 | 10% | 1 | 20 | 6 | 3 | 6 | | | | | | | | | 8 | 24 | 1.5 | 68.5 | 1.15 | 45 | 6.00 | 0.039 | 3,083 | 0.21 | 1.18 | 0.04 | 0.78 | 0.027 |
| 3-4 Reserve | Bldg 3 | 10% | 1 | 20 | 6 | 3 | 6 | | | | | | | | | 8 | 24 | 1.5 | 68.5 | 1.15 | 45 | 6.00 | 0.039 | 3,083 | 0.21 | 1.18 | 0.04 | 0.78 | 0.027 |
| ETC-2 Reserve | ETC | 10% | 1 | 20 | 6 | 3 | 6 | | | | | | | | | 8 | 24 | 1.5 | 68.5 | 1.15 | 45 | 6.00 | 0.039 | 3,083 | 0.21 | 1.18 | 0.04 | 0.78 | 0.027 |
| | | | | | | | | | | | | | | | | | Total PM | | NOX | | CO | | VOC | | | | | | |
| | | | | | | | | | | | | | | | | | CONTROLLED Facility-Wide Emissions | 1.17 | 169,500 | 16.14 | 0.958 | | 0.485 | | | | | | |
| | | | | | | | | | | | | | | | | | UNCONTROLLED Facility-Wide Emissions | 1.56 | | 16.14 | 3.15 | | 0.870 | | | | | | |
| | | | | | | | | | | | | | | | | | Tons/Yr Removed | 0.39 | | 0.00 | 2.19 | | 0.39 | | | | | | |
| | | | | | | | | | | | | | | | | | Overall Removal Effcy, % | 25% | | 0% | 70% | | 44% | | | | | | |

Table DOC-3. BACT Capital Cost for DOCs (Based on DIS Data Center)

Vantage Data Center

| Cost Category | Cost Factor | Source of Cost Factor | Quant. | Unit Cost | Subtotal Cost |
|---|-----------------|-----------------------|--------|-----------|--------------------|
| Direct Costs | | | | | |
| Purchased Equipment Costs | | | | | |
| Total Installed Cost for DIS Data Center's 2500 kWe generators was \$306,200 for 5 gensets or \$61,200 per genset, including all engineering, fees, and construction costs. The total installed price for Vantage's 3,000 kWe generators was scaled using the "0.6 rule": Cost for 3,000 kWe units = \$61,200 *(3000/2500) ^{0.6} = \$68,300 each | | | | | |
| Vantage 3000 kWe Total Installed Cost | DIS Data Center | DIS Data Center | 17 | \$68,300 | \$1,161,100 |
| Instrumentation | Included | Included | 0 | 0 | 0 |
| Sales Tax | Included | Included | 0.0% | -- | \$0 |
| Shipping | Included | Included | 0.0% | -- | \$0 |
| Subtotal Purchased Equipment Cost, PEC | | | | | \$1,161,100 |
| Direct Installation Costs | | | | | |
| Enclosure structural supports | Included | Included | 0 | \$9,812 | \$0 |
| Installation | Included | Included | 0.0% | -- | \$0 |
| Electrical | Included | Included | 0 | 0 | 0 |
| Piping | Included | Included | 0 | 0 | 0 |
| Insulation | Included | Included | 0 | 0 | 0 |
| Painting | Included | Included | 0 | 0 | 0 |
| Subtotal Direct Installation Costs | | | | | \$0 |
| Site Preparation and Buildings (SP) | Included | Included | 0 | 0 | 0 |
| Total Direct Costs, DC (PEC + Direct Installation + Site Prep) | | | | | \$1,161,100 |
| Indirect Costs (Installation) | | | | | |
| Engineering | Included | Included | 0.0% | -- | \$0 |
| Construction and field expenses | Included | Included | 0.0% | -- | \$0 |
| Contractor Fees | Included | Included | 0.0% | -- | \$0 |
| Startup | Included | Included | 0.0% | -- | \$0 |
| Performance Test (Tech support) | Included | Included | 0.0% | -- | \$0 |
| Contingencies | Included | Included | 0.0% | -- | \$0 |
| Subtotal Indirect Costs, IC | | | | | \$0 |
| Total Capital Investment (TCI = DC+IC) | | | | | \$1,161,100 |
| | | | | | TCI per gen |
| | | | | | \$68,300 |

Table DOC-4. DOC Nominal-Controlled BACT Cost-Effectiveness

| Item | Quantity | Units | Unit cost | Subtotal |
|---|------------------------|-------|-----------|------------------|
| Annualized Capital Recovery | | | | |
| Total Capital Cost | | | | \$1,161,100 |
| Capital Recovery Factor, 25 yrs, 4% discount rate | | | | 0.06401 |
| Subtotal Annualized 25-year Capital Recovery Cost | | | | \$74,322 |
| Direct Annual Costs | | | | |
| Annual Admin charges | 2% of TCI (EPA Manual) | | 0.02 | \$23,222 |
| Annual Property tax | 1% of TCI (EPA Manual) | | 0.01 | \$11,611 |
| Annual Insurance | 1% of TCI (EPA Manual) | | 0.01 | \$11,611 |
| For this screening-level analysis we assumed the lower-bound annual O&M cost of zero. | | | | \$0 |
| Subtotal Direct Annual Costs | | | | \$46,444 |
| Total Annual Cost (Capital Recovery + Direct Annual Costs) | | | | \$120,766 |
| Uncontrolled emissions (Combined Pollutants) | | | | 21.7 |
| Assumed Control Efficiency | | | | Varies |
| Annual Tons Removed (Combined Pollutants) | | | | 2.97 |
| Cost Effectiveness (\$ per tons combined pollutant destroyed) | | | | \$40,698 |

Multi-Pollutant Cost-Effectiveness for "Reasonable Control Cost" vs. Actual Control Cost

| Pollutant | Ecology Acceptable Unit Cost (\$/ton) | Forecast Removal (tons/yr) | Subtotal Acceptable Annual Cost (\$/year) |
|---|---------------------------------------|----------------------------|---|
| NOX | \$10,000 | 0.00 | \$0 per year |
| CO | \$5,000 | 2.19 | \$10,960 per year |
| VOC | \$9,999 | 0.39 | \$3,852 per year |
| PM (FH+BH) | \$23,200 | 0.39 | \$9,052 per year |
| Total Reasonable Annual Control Cost for Combined Pollutants | | | \$23,863 per year |
| Actual Annual Control Cost | | | \$120,766 per year |
| Is The Control Device Reasonable? | | | NO (Actual >> Acceptable) |

| DOC Combined Pollutants Removal Tonnages (Nominal-Controlled) | | | | |
|--|------------|-----------|-----------|-----------|
| Pollutant | PM (FH+BH) | CO | VOC | NOX |
| Nominal Cold-Start Uncontrolled TPY | 1.56 | 3.15 | 0.870 | 16.1 |
| Nominal Cold-Start Controlled TPY | 1.170 | 0.958 | 0.485 | 16.14 |
| Tons Removed/Year | 0.39 | 2.19 | 0.385 | 0.0 |
| Overall Cold-Start Removal Efficacy | 25% | 70% | 44% | 0% |
| Total Annual Cost | \$120,766 | \$120,766 | \$120,766 | \$120,766 |
| Indiv Poll \$/Ton Removed | \$309,535 | \$55,094 | \$313,511 | #DIV/0! |

G:\Seattle\PNWProjects\PACLAND_-11_Riker Data Center\03_Reports-Analyses\BACT-July-2012\DOC_Vantage-BACT_July-2012.xls\Vantage capital Cost

APPENDIX E
STACK TEST DATA AND VENDOR-SUPPLIED
EMISSION DATA

STACK TEST GROUP, INC.
Air Quality Services

Client: GenAcc
Project No: 11-2146
Load: 100%
Source: MTU 3250

| Test No: | T1 | T2 | T3 | Avg. |
|---------------------------------------|-----------|-----------|-----------|--------|
| Start Time: | 08:35 AM | 07:35 AM | 08:52 AM | |
| Finish Time: | 10:20 AM | 08:38 AM | 09:54 AM | |
| Date: | 7/18/2011 | 7/19/2011 | 7/19/2011 | |
| Pitot Cal. Factor: | 0.84 | 0.84 | 0.84 | |
| Meter Calibration Factor: | 1.035 | 1.035 | 1.035 | |
| Stack Length, inches: | 0 | 0 | 0 | |
| Stack Width, inches: | 0 | 0 | 0 | |
| Stack Diameter, inches: | 35.5 | 35.5 | 35.5 | |
| Nozzle Diameter, inches: | 0.311 | 0.311 | 0.311 | |
| Barometric Pressure, inches Hg: | 29.20 | 29.10 | 29.10 | |
| Static Pressure in Stack, Inches H2O: | -0.33 | -0.23 | -0.27 | |
| Duration of Sample, minutes: | 60 | 60 | 60 | |
| Meter Start Volume: | 487.480 | 874.750 | 914.820 | |
| Meter Final Volume: | 529.150 | 914.340 | 956.000 | |
| Average Meter Pressure, Inches H2O: | 1.6800 | 1.4075 | 1.5150 | 1.5342 |
| Average Meter Temperature, degrees F: | 88.21 | 89.9 | 93.52 | 90.5 |
| Average Sqrt. Velocity Pressure: | 0.6503 | 0.5990 | 0.6177 | 0.6223 |
| Stack Gas Temperature, degrees F: | 838.2 | 823 | 829.21 | 830.1 |
| % Carbon Dioxide: | 10.2 | 10.2 | 10.2 | 10.2 |
| % Oxygen: | 8.4 | 8.4 | 8.4 | 8.4 |
| % Carbon Monoxide: | 0.0 | 0.0 | 0.0 | 0.0 |
| Liquid Volume Collected, milliliters: | 102.5 | 100 | 99.5 | 100.7 |

Sample Train Calculations

| | | | | |
|-------------------------------------|--------|--------|--------|--------|
| Meter Volume, Actual: | 41,670 | 39,590 | 41,180 | 40,813 |
| Meter Volume, STP: | 40,695 | 38,386 | 39,679 | 39,587 |
| Volume of Water Vapor Condensed: | 4,825 | 4,707 | 4,683 | 4,738 |
| Total Gas Sampled: | 45,520 | 43,093 | 44,362 | 44,325 |
| % Moisture: | 10.60 | 10.92 | 10.56 | 10.69 |
| Area of Stack, Square Feet: | 6.87 | 6.87 | 6.87 | 6.87 |
| % Excess Air at Test Location: | 64.2 | 64.2 | 64.2 | 64.2 |
| Molecular Weight dry, lb/lb-Mole: | 29.97 | 29.97 | 29.97 | 29.97 |
| Molecular Weight wet, lb/lb-Mole: | 28.70 | 28.66 | 28.71 | 28.69 |
| Absolute Stack Gas Pressure, in Hg: | 29.18 | 29.08 | 29.08 | 29.11 |
| Isokinetic, %: | 104.0 | 106.4 | 106.5 | 105.6 |

Velocity and Flow Calculations

| | | | | |
|---------------------------------|---------|---------|---------|---------|
| Average Stack Gas Velocity FPS: | 58.14 | 53.37 | 55.12 | 55.54 |
| Stack Gas Flow Rate, ACFM: | 23,965 | 21,999 | 22,720 | 22,895 |
| Stack Gas Flow Rate, SCFM: | 9,506 | 8,799 | 9,044 | 9,116 |
| Stack Gas Flow Rate, DSCF/HR: | 509,899 | 470,302 | 485,337 | 488,513 |
| Stack Gas Flow Rate, DSCFM: | 8,498 | 7,838 | 8,089 | 8,142 |

VOC Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPM as Propane: | 0.8 | 1.1 | 1.2 | 1.0 |
| LBS/DSCF: | 9.14E-08 | 1.26E-07 | 1.37E-07 | 1.18E-07 |
| LBS/HR: | 0.1 | 0.1 | 0.1 | 0.1 |
| Brake HP: | 4680 | 4680 | 4680 | 4680.0 |
| Grams/Brake HP HR: | 0.005 | 0.006 | 0.007 | 0.006 |

NOx Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPMv | 29.6 | 30.1 | 36.2 | 32.0 |
| LBS/DSCF: | 3.53E-06 | 3.59E-06 | 4.32E-06 | 3.82E-06 |
| LBS/HR: | 1.80 | 1.69 | 2.10 | 1.9 |
| Brake HP: | 4680 | 4680 | 4680 | 4680.0 |
| Grams/Brake HP HR: | 0.175 | 0.164 | 0.203 | 0.181 |

CO Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPMv | 2.1 | 1.2 | 1.2 | 1.5 |
| LBS/DSCF: | 1.53E-07 | 8.72E-08 | 8.72E-08 | 1.09E-07 |
| LBS/HR: | 0.08 | 0.04 | 0.04 | 0.1 |
| Brake HP: | 4680 | 4680 | 4680 | 4680.0 |
| Grams/Brake HP HR: | 0.008 | 0.004 | 0.004 | 0.005 |

STACK TEST GROUP, INC.
Air Quality Services

Client: GenAcc
Project No: 11-2146
Load: 75%
Source: MTU 3250

| Test No: | T1 | T2 | T3 | Avg. |
|---------------------------------------|-----------|-----------|-----------|--------|
| Start Time: | 10:45 AM | 04:02 PM | 05:20 PM | |
| Finish Time: | 11:47 AM | 05:06 PM | 06:23 PM | |
| Date: | 7/18/2011 | 7/18/2011 | 7/18/2011 | |
| Pilot Cal. Factor: | 0.84 | 0.84 | 0.84 | |
| Meter Calibration Factor: | 1.035 | 1.035 | 1.035 | |
| Stack Length, inches: | 0 | 0 | 0 | |
| Stack Width, inches: | 0 | 0 | 0 | |
| Stack Diameter, inches: | 35.5 | 35.5 | 35.5 | |
| Nozzle Diameter, inches: | 0.342 | 0.342 | 0.342 | |
| Barometric Pressure, inches Hg: | 29.20 | 29.20 | 29.20 | |
| Static Pressure in Stack, Inches H2O: | -0.28 | -0.26 | -0.24 | |
| Duration of Sample, minutes: | 60 | 60 | 60 | |
| Meter Start Volume: | 529.400 | 729.950 | 777.840 | |
| Meter Final Volume: | 574.050 | 777.450 | 825.930 | |
| Average Meter Pressure, Inches H2O: | 2.1500 | 2.1042 | 2.1500 | 2.1347 |
| Average Meter Temperature, degrees F: | 94.1 | 94.63 | 97.46 | 95.4 |
| Average Sqrt. Velocity Pressure: | 0.5837 | 0.5753 | 0.5812 | 0.5801 |
| Stack Gas Temperature, degrees F: | 743.8 | 766.33 | 759.58 | 756.6 |
| % Carbon Dioxide: | 9.1 | 9.1 | 9.1 | 9.1 |
| % Oxygen: | 10.3 | 10.0 | 10.1 | 10.1 |
| % Carbon Monoxide: | 0.0 | 0.0 | 0.0 | 0.0 |
| Liquid Volume Collected, milliliters: | 99 | 97 | 99.5 | 98.5 |

Sample Train Calculations

| | | | | |
|-------------------------------------|--------|--------|--------|--------|
| Meter Volume, Actual: | 44,650 | 47,500 | 48,090 | 46,747 |
| Meter Volume, STP: | 43,192 | 45,902 | 46,236 | 45,110 |
| Volume of Water Vapor Condensed: | 4,660 | 4,566 | 4,683 | 4,636 |
| Total Gas Sampled: | 47,852 | 50,468 | 50,919 | 49,746 |
| % Moisture: | 9.74 | 9.05 | 9.20 | 9.33 |
| Area of Stack, Square Feet: | 6.87 | 6.87 | 6.87 | 6.87 |
| % Excess Air at Test Location: | 93.8 | 88.0 | 89.9 | 90.6 |
| Molecular Weight dry, lb/lb-Mole: | 29.87 | 29.86 | 29.86 | 29.86 |
| Molecular Weight wet, lb/lb-Mole: | 28.71 | 28.79 | 28.77 | 28.76 |
| Absolute Stack Gas Pressure, in Hg: | 29.18 | 29.18 | 29.18 | 29.18 |
| Isokinetic, %: | 97.0 | 104.9 | 104.4 | 102.1 |

Velocity and Flow Calculations

| | | | | |
|---------------------------------|---------|---------|---------|---------|
| Average Stack Gas Velocity FPS: | 50.25 | 49.91 | 50.31 | 50.16 |
| Stack Gas Flow Rate, ACFM: | 20,713 | 20,573 | 20,738 | 20,675 |
| Stack Gas Flow Rate, SCFM: | 8,860 | 8,639 | 8,756 | 8,752 |
| Stack Gas Flow Rate, DSCF/HR: | 479,841 | 471,411 | 477,031 | 476,094 |
| Stack Gas Flow Rate, DSCFM: | 7,997 | 7,857 | 7,951 | 7,935 |

VOC Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPM as Propane: | 1.8 | 1.6 | 1.7 | 1.7 |
| LBS/DSCF: | 2.06E-07 | 1.83E-07 | 1.94E-07 | 1.94E-07 |
| LBS/HR: | 0.1 | 0.1 | 0.1 | 0.1 |
| Brake HP: | 3509 | 3509 | 3509 | 3509.0 |
| Grams/Brake HP HR: | 0.014 | 0.012 | 0.013 | 0.013 |

NOx Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPMv | 16.9 | 14.7 | 18.1 | 16.6 |
| LBS/DSCF: | 2.02E-06 | 1.75E-06 | 2.16E-06 | 1.98E-06 |
| LBS/HR: | 0.97 | 0.83 | 1.03 | 0.9 |
| Brake HP: | 3509 | 3509 | 3509 | 3509.0 |
| Grams/Brake HP HR: | 0.125 | 0.107 | 0.133 | 0.122 |

CO Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPMv | 1.3 | 1.1 | 1.0 | 1.1 |
| LBS/DSCF: | 9.45E-08 | 7.99E-08 | 7.27E-08 | 8.24E-08 |
| LBS/HR: | 0.05 | 0.04 | 0.03 | 0.0 |
| Brake HP: | 3509 | 3509 | 3509 | 3509.0 |
| Grams/Brake HP HR: | 0.006 | 0.005 | 0.004 | 0.005 |

STACK TEST GROUP, INC.
Air Quality Services

Client: GenAcc
Project No: 11-2146
Load: 50%
Source: MTU 3250

| Test No: | T1 | T2 | T3 | Avg. |
|---------------------------------------|-----------|-----------|-----------|--------|
| Start Time: | 12:05 PM | 01:30 PM | 02:47 PM | |
| Finish Time: | 01:09 PM | 02:33 PM | 03:50 PM | |
| Date: | 7/18/2011 | 7/18/2011 | 7/18/2011 | |
| Pitot Cal. Factor: | 0.84 | 0.84 | 0.84 | |
| Meter Calibration Factor: | 1.035 | 1.035 | 1.035 | |
| Stack Length, inches: | 0 | 0 | 0 | |
| Stack Width, inches: | 0 | 0 | 0 | |
| Stack Diameter, inches: | 35.5 | 35.5 | 35.5 | |
| Nozzle Diameter, inches: | 0.412 | 0.412 | 0.412 | |
| Barometric Pressure, inches Hg: | 29.20 | 29.20 | 29.20 | |
| Static Pressure in Stack, Inches H2O: | -0.16 | -0.14 | -0.15 | |
| Duration of Sample, minutes: | 60 | 60 | 60 | |
| Meter Start Volume: | 577.810 | 627.920 | 679.540 | |
| Meter Final Volume: | 627.550 | 679.250 | 729.520 | |
| Average Meter Pressure, Inches H2O: | 2.4700 | 2.4400 | 2.3400 | 2.4167 |
| Average Meter Temperature, degrees F: | 87.65 | 92.9 | 91.63 | 90.7 |
| Average Sqrt. Velocity Pressure: | 0.4260 | 0.4212 | 0.4149 | 0.4207 |
| Stack Gas Temperature, degrees F: | 679.0 | 684.58 | 688.71 | 684.1 |
| % Carbon Dioxide: | 8.1 | 8.1 | 8.1 | 8.1 |
| % Oxygen: | 11.6 | 11.7 | 11.4 | 11.6 |
| % Carbon Monoxide: | 0.0 | 0.0 | 0.0 | 0.0 |
| Liquid Volume Collected, milliliters: | 74 | 66.5 | 63.5 | 68.0 |

Sample Train Calculations

| | | | | |
|-------------------------------------|--------|--------|--------|--------|
| Meter Volume, Actual: | 49,740 | 51,330 | 49,980 | 50,350 |
| Meter Volume, STP: | 48,717 | 49,797 | 48,590 | 49,035 |
| Volume of Water Vapor Condensed: | 3,483 | 3,130 | 2,989 | 3,201 |
| Total Gas Sampled: | 52,200 | 52,928 | 51,579 | 52,235 |
| % Moisture: | 6.67 | 5.91 | 5.79 | 6.13 |
| Area of Stack, Square Feet: | 6.87 | 6.87 | 6.87 | 6.87 |
| % Excess Air at Test Location: | 120.8 | 123.5 | 115.7 | 120.0 |
| Molecular Weight dry, lb/lb-Mole: | 29.76 | 29.76 | 29.75 | 29.76 |
| Molecular Weight wet, lb/lb-Mole: | 28.98 | 29.06 | 29.07 | 29.04 |
| Absolute Stack Gas Pressure, in Hg: | 29.19 | 29.19 | 29.19 | 29.19 |
| Isokinetic, %: | 97.6 | 100.5 | 99.6 | 99.2 |

Velocity and Flow Calculations

| | | | | |
|---------------------------------|---------|---------|---------|---------|
| Average Stack Gas Velocity FPS: | 35.50 | 35.14 | 34.67 | 35.10 |
| Stack Gas Flow Rate, ACFM: | 14,633 | 14,485 | 14,291 | 14,470 |
| Stack Gas Flow Rate, SCFM: | 6,618 | 6,519 | 6,409 | 6,515 |
| Stack Gas Flow Rate, DSCF/HR: | 370,588 | 368,014 | 362,248 | 366,950 |
| Stack Gas Flow Rate, DSCFM: | 6,176 | 6,134 | 6,037 | 6,116 |

VOC Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPM as Propane: | 1.7 | 1.7 | 1.4 | 1.6 |
| LBS/DSCF: | 1.94E-07 | 1.94E-07 | 1.60E-07 | 1.83E-07 |
| LBS/HR: | 0.1 | 0.1 | 0.1 | 0.1 |
| Brake HP: | 2339 | 2339 | 2339 | 2339.0 |
| Grams/Brake HP HR: | 0.015 | 0.015 | 0.012 | 0.014 |

NOx Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPMv | 10.3 | 8.7 | 9.4 | 9.5 |
| LBS/DSCF: | 1.23E-06 | 1.04E-06 | 1.12E-06 | 1.13E-06 |
| LBS/HR: | 0.46 | 0.38 | 0.41 | 0.4 |
| Brake HP: | 2339 | 2339 | 2339 | 2339.0 |
| Grams/Brake HP HR: | 0.088 | 0.074 | 0.079 | 0.080 |

CO Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPMv | 1.2 | 1.3 | 1.1 | 1.2 |
| LBS/DSCF: | 8.72E-08 | 9.45E-08 | 7.99E-08 | 8.72E-08 |
| LBS/HR: | 0.03 | 0.03 | 0.03 | 0.0 |
| Brake HP: | 2339 | 2339 | 2339 | 2339.0 |
| Grams/Brake HP HR: | 0.006 | 0.007 | 0.006 | 0.006 |

STACK TEST GROUP, INC.
Air Quality Services

Client: GenAcc
Project No: 11-2146
Load: 25%
Source: MTU 3250

| Test No: | T1 | T2 | T3 | Avg. |
|---------------------------------------|-----------|-----------|-----------|--------|
| Start Time: | 06:37 PM | 03:42 PM | 05:00 PM | |
| Finish Time: | 07:40 PM | 04:45 PM | 06:03 PM | |
| Date: | 7/18/2011 | 7/19/2011 | 7/19/2011 | |
| Pitot Cal. Factor: | 0.84 | 0.84 | 0.84 | |
| Meter Calibration Factor: | 1.035 | 1.035 | 1.035 | |
| Stack Length, inches: | 0 | 0 | 0 | |
| Stack Width, inches: | 0 | 0 | 0 | |
| Stack Diameter, inches: | 35.5 | 35.5 | 35.5 | |
| Nozzle Diameter, inches: | 0.492 | 0.492 | 0.492 | |
| Barometric Pressure, inches Hg: | 29.20 | 29.10 | 29.10 | |
| Static Pressure in Stack, Inches H2O: | -0.3 | -0.28 | -0.31 | |
| Duration of Sample, minutes: | 60 | 60 | 60 | |
| Meter Start Volume: | 826.480 | 956.350 | 6.430 | |
| Meter Final Volume: | 874.150 | 1005.810 | 54.730 | |
| Average Meter Pressure, Inches H2O: | 2.0800 | 2.1500 | 2.0700 | 2.1000 |
| Average Meter Temperature, degrees F: | 97.38 | 95.79 | 97 | 96.7 |
| Average Sqrt. Velocity Pressure: | 0.2669 | 0.2728 | 0.2682 | 0.2693 |
| Stack Gas Temperature, degrees F: | 595.4 | 605 | 599.79 | 600.1 |
| % Carbon Dioxide: | 7.7 | 7.7 | 7.7 | 7.7 |
| % Oxygen: | 12.6 | 12.6 | 12.6 | 12.6 |
| % Carbon Monoxide: | 0.0 | 0.0 | 0.0 | 0.0 |
| Liquid Volume Collected, milliliters: | 87 | 89 | 89 | 88.3 |

Sample Train Calculations

| | | | | |
|-------------------------------------|--------|--------|--------|--------|
| Meter Volume, Actual: | 47.670 | 49.460 | 48.300 | 48.477 |
| Meter Volume, STP: | 45.832 | 47.536 | 46.312 | 46.560 |
| Volume of Water Vapor Condensed: | 4.095 | 4.189 | 4.189 | 4.158 |
| Total Gas Sampled: | 49.927 | 51.725 | 50.501 | 50.718 |
| % Moisture: | 8.20 | 8.10 | 8.29 | 8.20 |
| Area of Stack, Square Feet: | 6.87 | 6.87 | 6.87 | 6.87 |
| % Excess Air at Test Location: | 149.3 | 149.3 | 149.3 | 149.3 |
| Molecular Weight dry, lb/lb-Mole: | 29.74 | 29.74 | 29.74 | 29.74 |
| Molecular Weight wet, lb/lb-Mole: | 28.78 | 28.79 | 28.77 | 28.78 |
| Absolute Stack Gas Pressure, in Hg: | 29.18 | 29.08 | 29.08 | 29.11 |
| Isokinetic, %: | 100.2 | 102.3 | 101.3 | 101.3 |

Velocity and Flow Calculations

| | | | | |
|---------------------------------|---------|---------|---------|---------|
| Average Stack Gas Velocity FPS: | 21.49 | 22.10 | 21.68 | 21.75 |
| Stack Gas Flow Rate, ACFM: | 8,858 | 9,110 | 8,936 | 8,968 |
| Stack Gas Flow Rate, SCFM: | 4,322 | 4,390 | 4,327 | 4,346 |
| Stack Gas Flow Rate, DSCF/HR: | 238,060 | 242,038 | 238,112 | 239,404 |
| Stack Gas Flow Rate, DSCFM: | 3,968 | 4,034 | 3,969 | 3,990 |

VOC Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPM as Propane: | 1.4 | 0.8 | 0.9 | 1.0 |
| LBS/DSCF: | 1.60E-07 | 9.14E-08 | 1.03E-07 | 1.18E-07 |
| LBS/HR: | 0.0 | 0.0 | 0.0 | 0.0 |
| Brake HP: | 1169 | 1169 | 1169 | 1169 |
| Grams/Brake HP HR: | 0.016 | 0.009 | 0.010 | 0.012 |

NOx Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPMv | 14.6 | 9.9 | 7.4 | 10.6 |
| LBS/DSCF: | 1.74E-06 | 1.18E-06 | 8.83E-07 | 1.27E-06 |
| LBS/HR: | 0.41 | 0.29 | 0.21 | 0.3 |
| Brake HP: | 1169 | 1169 | 1169 | 1169 |
| Grams/Brake HP HR: | 0.161 | 0.111 | 0.082 | 0.118 |

CO Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPMv | 0.9 | 1.1 | 1.2 | 1.1 |
| LBS/DSCF: | 6.54E-08 | 7.99E-08 | 8.72E-08 | 7.75E-08 |
| LBS/HR: | 0.02 | 0.02 | 0.02 | 0.0 |
| Brake HP: | 1169 | 1169 | 1169 | 1169 |
| Grams/Brake HP HR: | 0.006 | 0.008 | 0.008 | 0.007 |

STACK TEST GROUP, INC.
Air Quality Services

Client: GenAcc
Project No: 11-2146
Load: 10%
Source: MTU 3250

| Test No: | T1 | T2 | T3 | Avg. |
|---------------------------------------|-----------|-----------|-----------|--------|
| Start Time: | 02:05 PM | 03:42 PM | 05:00 PM | |
| Finish Time: | 03:29 PM | 04:45 PM | 06:03 PM | |
| Date: | 7/19/2011 | 7/19/2011 | 7/19/2011 | |
| Pitot Cal. Factor: | 0.84 | 0.84 | 0.84 | |
| Meter Calibration Factor: | 1.035 | 1.035 | 1.035 | |
| Stack Length, inches: | 0 | 0 | 0 | |
| Stack Width, inches: | 0 | 0 | 0 | |
| Stack Diameter, inches: | 35.5 | 35.5 | 35.5 | |
| Barometric Pressure, inches Hg: | 29.10 | 29.10 | 29.10 | |
| Static Pressure in Stack, Inches H2O: | -0.02 | -0.02 | -0.02 | |
| Duration of Sample, minutes: | 60 | 60 | 60 | |
| Meter Start Volume: | 55,030 | 99,760 | 141,420 | |
| Meter Final Volume: | 99,470 | 140,980 | 185,340 | |
| Average Meter Pressure, Inches H2O: | 1.7300 | 1.8933 | 1.6917 | 1.7717 |
| Average Meter Temperature, degrees F: | 101.17 | 102.12 | 100.87 | 101.3 |
| Average Sqrt. Velocity Pressure: | 0.1900 | 0.1752 | 0.1880 | 0.1844 |
| Stack Gas Temperature, degrees F: | 469.8 | 467.88 | 457.83 | 465.2 |
| % Carbon Dioxide: | 5.7 | 5.7 | 5.7 | 5.7 |
| % Oxygen: | 14.7 | 14.7 | 14.7 | 14.7 |
| % Carbon Monoxide: | 0.0 | 0.0 | 0.0 | 0.0 |
| Liquid Volume Collected, milliliters: | 62 | 63 | 61.5 | 62.2 |

Sample Train Calculations:

| | | | | |
|-------------------------------------|--------|--------|--------|--------|
| Meter Volume, Actual: | 44,440 | 41,220 | 43,920 | 43,193 |
| Meter Volume, STP: | 42,255 | 39,147 | 41,794 | 41,066 |
| Volume of Water Vapor Condensed: | 2,918 | 2,965 | 2,895 | 2,926 |
| Total Gas Sampled: | 45,174 | 42,112 | 44,689 | 43,992 |
| % Moisture: | 6.46 | 7.04 | 6.48 | 6.66 |
| Area of Stack, Square Feet: | 6.87 | 6.87 | 6.87 | 6.87 |
| % Excess Air at Test Location: | 232.8 | 232.8 | 232.8 | 232.8 |
| Molecular Weight dry, lb/lb-Mole: | 29.50 | 29.50 | 29.50 | 29.50 |
| Molecular Weight wet, lb/lb-Mole: | 28.76 | 28.69 | 28.75 | 28.73 |
| Absolute Stack Gas Pressure, in Hg: | 29.10 | 29.10 | 29.10 | 29.10 |
| Isokinetic, %: | 105.6 | 106.5 | 104.8 | 105.6 |

Velocity and Flow Calculations:

| | | | | |
|---------------------------------|---------|---------|---------|---------|
| Average Stack Gas Velocity FPS: | 14.38 | 13.26 | 14.14 | 13.93 |
| Stack Gas Flow Rate, ACFM: | 5,927 | 5,466 | 5,829 | 5,741 |
| Stack Gas Flow Rate, SCFM: | 3,274 | 3,025 | 3,261 | 3,187 |
| Stack Gas Flow Rate, DSCF/HR: | 183,737 | 168,722 | 182,985 | 178,481 |
| Stack Gas Flow Rate, DSCFM: | 3,062 | 2,812 | 3,050 | 2,975 |

VOC Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPM as Propane: | 2.2 | 2.2 | 2.1 | 2.2 |
| LBS/DSCF: | 2.51E-07 | 2.51E-07 | 2.40E-07 | 2.47E-07 |
| LBS/HR: | 0.0 | 0.0 | 0.0 | 0.0 |
| Brake HP: | 468 | 468 | 468 | 468 |
| Grams/Brake HP HR: | 0.048 | 0.044 | 0.045 | 0.046 |

NOx Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPMv | 75.2 | 81.3 | 79.7 | 78.7 |
| LBS/DSCF: | 8.98E-06 | 9.71E-06 | 9.52E-06 | 9.40E-06 |
| LBS/HR: | 1.65 | 1.64 | 1.74 | 1.7 |
| Brake HP: | 468 | 468 | 468 | 468 |
| Grams/Brake HP HR: | 1.599 | 1.587 | 1.688 | 1.625 |

CO Calculations:

| | | | | |
|--------------------|----------|----------|----------|----------|
| PPMv | 2.4 | 2.3 | 2.1 | 2.3 |
| LBS/DSCF: | 1.74E-07 | 1.67E-07 | 1.53E-07 | 1.65E-07 |
| LBS/HR: | 0.03 | 0.03 | 0.03 | 0.0 |
| Brake HP: | 468 | 468 | 468 | 468 |
| Grams/Brake HP HR: | 0.031 | 0.027 | 0.027 | 0.028 |

STACK TEST GROUP, INC.
Air Quality Services

Particulate Sampling Train Calculations

Client: GenAcc (CONTROLLED)
Load: 100%
Source: MTU 3250

| Test No: | T1 | T2 | Avg. |
|---------------------------------------|-----------|-----------|--------|
| Start Time: | 10:33 AM | 11:17 AM | |
| Finish Time: | 11:05 AM | 11:49 AM | |
| Date: | 9/16/2011 | 9/16/2011 | |
| Pitot Cal Factor: | 0.84 | 0.84 | |
| Meter Calibration Factor: | 1.018 | 1.018 | |
| Stack Length, inches: | 0 | 0 | |
| Stack Width, inches: | 0 | 0 | |
| Stack Diameter, inches: | 35.5 | 35.5 | |
| Nozzle Diameter, inches: | 0.384 | 0.384 | |
| Barometric Pressure, inches Hg: | 29.10 | 29.10 | |
| Static Pressure in Stack, Inches H2O: | -0.2 | -0.23 | |
| Duration of Sample, minutes: | 30 | 30 | |
| Meter Start Volume: | 772.120 | 799.890 | |
| Meter Final Volume: | 799.770 | 829.310 | |
| Average Meter Pressure, Inches H2O: | 2.9700 | 3.1800 | 3.0750 |
| Average Meter Temperature, degrees F: | 67.33 | 72.83 | 70.1 |
| Average Sqrt. Velocity Pressure: | 0.5610 | 0.5811 | 0.5711 |
| Stack Gas Temperature, degrees F: | 756.2 | 780.17 | 768.2 |
| % Carbon Dioxide: | 8.2 | 8.3 | 8.3 |
| % Oxygen: | 10.0 | 9.9 | 10.0 |
| % Carbon Monoxide: | 0.0 | 0.0 | 0.0 |
| Liquid Volume Collected, milliliters: | 38.5 | 37 | 37.8 |
| Total Weight of PM, (Front 1/2) Mg: | 3.4 | 3.0 | 3.2 |

REVISED TO
INCLUDE
BACK HALF PM
DATA FROM
PREVIOUS TESTING
ON SAME ENGINE
W/ CONTROLS

Sample Train Calculations

| | | | |
|-------------------------------------|--------|--------|--------|
| Meter Volume, Actual: | 27.650 | 29.420 | 28.535 |
| Meter Volume, STP: | 27.607 | 29.087 | 28.347 |
| Volume of Water Vapor Condensed: | 1.812 | 1.742 | 1.777 |
| Total Gas Sampled: | 29.419 | 30.828 | 30.124 |
| % Moisture: | 6.16 | 5.65 | 5.90 |
| Area of Stack, Square Feet: | 6.87 | 6.87 | 6.87 |
| % Excess Air at Test Location: | 86.2 | 84.7 | 85.4 |
| Molecular Weight dry, lb/lb-Mole: | 29.71 | 29.72 | 29.72 |
| Molecular Weight wet, lb/lb-Mole: | 28.99 | 29.06 | 29.02 |
| Absolute Stack Gas Pressure, in Hg: | 29.09 | 29.08 | 29.08 |
| Isokinetic, %: | 99.6 | 101.9 | 100.7 |

Velocity and Flow Calculations

| | | | |
|---------------------------------|---------|---------|---------|
| Average Stack Gas Velocity FPS: | 48.38 | 50.55 | 49.47 |
| Stack Gas Flow Rate, ACFM: | 19,942 | 20,837 | 20,389 |
| Stack Gas Flow Rate, SCFM: | 8,418 | 8,622 | 8,520 |
| Stack Gas Flow Rate, DSCF/HR: | 473,953 | 488,099 | 481,026 |
| Stack Gas Flow Rate, DSCFM: | 7,899 | 8,135 | 8,017 |

Front 1/2 Particulate Calculations:

| | | | |
|------------------|----------|----------|----------|
| Grains Per DSCF: | 0.0019 | 0.0016 | 0.0017 |
| LBS/DSCF: | 2.72E-07 | 2.27E-07 | 2.49E-07 |
| LBS/HR: | 0.13 | 0.11 | 0.12 |

Organics: (based on previous test results)

| | | | |
|------------------|----------|----------|----------|
| Grains Per DSCF: | 0.0012 | 0.0012 | 0.0012 |
| LBS/DSCF: | 1.76E-07 | 1.67E-07 | 1.71E-07 |
| LBS/HR: | 0.08 | 0.08 | 0.08 |

Aqueous: (based on previous test results)

| | | | |
|------------------|----------|----------|----------|
| Grains Per DSCF: | 0.0023 | 0.0023 | 0.0023 |
| LBS/DSCF: | 3.35E-07 | 3.22E-07 | 3.29E-07 |
| LBS/HR: | 0.16 | 0.16 | 0.16 |

Total Particulate: (revised to include back-half data from previous test results)

| | | | |
|--------------------|----------|----------|----------|
| Grains Per DSCF: | 0.0055 | 0.0050 | 0.0052 |
| LBS/DSCF: | 7.83E-07 | 7.16E-07 | 7.50E-07 |
| LBS/HR: | 0.37 | 0.35 | 0.36 |
| Brake HP: | 4680 | 4680 | 4680.0 |
| Grams/Brake HP HR: | 0.036 | 0.034 | 0.035 |

STACK TEST GROUP, INC.
Air Quality Services

Particulate Sampling Train Calculations

Client: GenAcc
Load: 50% **(CONTROLLED)**
Source: MTU 3250

| Test No: | T1 | T2 | Avg. |
|---------------------------------------|----------------|----------------|--------|
| Start Time: | 12:00 PM | 12:44 PM | |
| Finish Time: | 12:32 PM | 01:16 PM | |
| Date: | 9/16/2011 | 9/16/2011 | |
| Pitot Cal. Factor: | 0.84 | 0.84 | |
| Meter Calibration Factor: | 1.018 | 1.018 | |
| Stack Length, inches: | 0 | 0 | |
| Stack Width, inches: | 0 | 0 | |
| Stack Diameter, inches: | 35.5 | 35.5 | |
| Nozzle Diameter, inches: | 0.384 | 0.384 | |
| Barometric Pressure, inches Hg: | 29.20 | 29.10 | |
| Static Pressure in Stack, Inches H2O: | -0.1 | -0.09 | |
| Duration of Sample, minutes: | 30 | 30 | |
| Meter Start Volume: | 829.510 | 854.630 | |
| Meter Final Volume: | 854.420 | 877.350 | |
| Average Meter Pressure, Inches H2O: | 2.4500 | 2.0700 | 2.2600 |
| Average Meter Temperature, degrees F: | 75.33 | 76.33 | 75.8 |
| Average Sqrt. Velocity Pressure: | 0.4876 | 0.4432 | 0.4654 |
| Stack Gas Temperature, degrees F: | 648.7 | 658.67 | 653.7 |
| % Carbon Dioxide: | 6.0 | 6.1 | 6.1 |
| % Oxygen: | 12.7 | 12.6 | 12.7 |
| % Carbon Monoxide: | 0.0 | 0.0 | 0.0 |
| Liquid Volume Collected, milliliters: | 36.5 | 34 | 35.3 |
| Total Weight of PM, (Front 1/2) Mg: | 2.5 | 1.4 | 2.0 |

REVISED TO INCLUDE
BACK HALF PM
DATA FROM
PREVIOUS TESTING
ON SAME ENGINE
W/ CONTROLS

Sample Train Calculations

| | | | |
|-------------------------------------|--------|--------|--------|
| Meter Volume, Actual: | 24.910 | 22.720 | 23.815 |
| Meter Volume, STP: | 24.551 | 22.254 | 23.403 |
| Volume of Water Vapor Condensed: | 1.718 | 1.600 | 1.659 |
| Total Gas Sampled: | 26.269 | 23.854 | 25.062 |
| % Moisture: | 6.54 | 6.71 | 6.62 |
| Area of Stack, Square Feet: | 6.87 | 6.87 | 6.87 |
| % Excess Air at Test Location: | 144.9 | 142.2 | 143.5 |
| Molecular Weight dry, lb/lb-Mole: | 29.47 | 29.48 | 29.47 |
| Molecular Weight wet, lb/lb-Mole: | 28.72 | 28.71 | 28.71 |
| Absolute Stack Gas Pressure, in Hg: | 29.19 | 29.09 | 29.14 |
| Isokinetic, %: | 97.0 | 97.6 | 97.3 |

Velocity and Flow Calculations

| | | | |
|---------------------------------|---------|---------|---------|
| Average Stack Gas Velocity FPS: | 40.27 | 36.83 | 38.55 |
| Stack Gas Flow Rate, ACFM: | 16,599 | 15,181 | 15,890 |
| Stack Gas Flow Rate, SCFM: | 7,712 | 6,967 | 7,340 |
| Stack Gas Flow Rate, DSCF/HR: | 432,485 | 389,951 | 411,218 |
| Stack Gas Flow Rate, DSCFM: | 7,208 | 6,499 | 6,854 |

Front 1/2 Particulate Calculations:

| | | | |
|------------------|----------|----------|----------|
| Grains Per DSCF: | 0.0016 | 0.0010 | 0.0013 |
| LBS/DSCF: | 2.25E-07 | 1.39E-07 | 1.82E-07 |
| LBS/HR: | 0.10 | 0.05 | 0.08 |

Organics: (based on previous test results)

| | | | |
|------------------|----------|----------|----------|
| Grains Per DSCF: | 0.0007 | 0.0007 | 0.0007 |
| LBS/DSCF: | 9.88E-08 | 1.04E-07 | 1.01E-07 |
| LBS/HR: | 0.04 | 0.04 | 0.04 |

Aqueous: (based on previous test results)

| | | | |
|------------------|----------|----------|----------|
| Grains Per DSCF: | 0.0025 | 0.0026 | 0.0025 |
| LBS/DSCF: | 3.59E-07 | 3.67E-07 | 3.63E-07 |
| LBS/HR: | 0.16 | 0.14 | 0.15 |

Total Particulate: (revised to include back half data from previous test results)

| | | | |
|--------------------|----------|----------|----------|
| Grains Per DSCF: | 0.0048 | 0.0043 | 0.0045 |
| LBS/DSCF: | 6.83E-07 | 6.09E-07 | 6.46E-07 |
| LBS/HR: | 0.30 | 0.24 | 0.27 |
| Brake HP: | 2339 | 2339 | 2339 |
| Grams/Brake HP HR: | 0.057 | 0.046 | 0.052 |

Total Controlled (NTE) PM Emissions
Engine Emission Specs

| Fuel Consumption | Gal/hr | Power (kW) | Power (bhp) | Exhaust Mass Flow (kg/hr) | Exhaust Mass Flow (acfm) | Power Output (eKW) | Exhaust Temperature after turbine (°C) | Exhaust Temperature after turbine (°F) |
|---|--------|------------|-------------|---------------------------|--------------------------|--------------------|--|--|
| 100% Load | 232 | 3490 | 4680 | 19529 | 22895 | 3256 | 495 | 923 |
| 75% Load | 183 | 2617 | 3509 | 17631 | 20675 | 2426 | 431 | 807.8 |
| 50% Load | 127 | 1744 | 2339 | 14079 | 14770 | 1597 | 386 | 726.8 |
| 25% Load | 76 | 872 | 1169 | 9354 | 8968 | 768 | 350 | 662 |
| 10% Load | 39 | 349 | 468 | 6825 | 5741 | 272 | 311 | 591.8 |
| 100% | | | | | | | | |
| 100% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.00209 | 0.012 | 86.0% |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.063 | 0.047 | 0.000103 | 0.484 | 0.086 | 0.012 | 0.035 |
| 90% | | | | | | | | |
| 90% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.00183 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.061 | 0.046 | 0.000100 | 0.425 | | | |
| 80% | | | | | | | | |
| 80% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.00158 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.059 | 0.044 | 0.000097 | 0.366 | | | |
| 75% | | | | | | | | |
| 75% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.00145 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.059 | 0.0436 | 0.000096 | 0.337 | | | |
| 70% | | | | | | | | |
| 70% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.00147 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.071 | 0.053 | 0.000117 | 0.340 | | | |
| 60% | | | | | | | | |
| 60% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.00148 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.084 | 0.062 | 0.000137 | 0.344 | | | |
| 50% | | | | | | | | |
| 50% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.0015 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.09 | 0.067 | 0.00015 | 0.345 | | | |
| 40% | | | | | | | | |
| 40% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.00230 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.110 | 0.082 | 0.000180 | 0.314 | | | |
| 30% | | | | | | | | |
| 30% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.00312 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.130 | 0.097 | 0.000213 | 0.283 | | | |
| 25% | | | | | | | | |
| 25% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.00352 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.140 | 0.104 | 0.000229 | 0.268 | | | |
| 20% | | | | | | | | |
| 20% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.00400 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.177 | 0.132 | 0.00029 | 0.243 | | | |
| 10% | | | | | | | | |
| 10% Load - Controlled emissions (NTE) @ 85% Reduction Efficiency | | | | | | | | |
| Total Controlled PM emissions (NTE) | | g/kWh | g/bhp-hr | lbs/bhp-hr | lbs/hr | 0.0050 | | |
| MTU 20V4000GB3L 3D EPA Tier2 (L,800 ppm) | | 0.252 | 0.188 | 0.00041 | 0.194 | | | |

Final Tier IV Emission Standards - Generator Sets > 900 kW

| Pollutant | Tier IV Final Emission Standards | | | |
|-----------|----------------------------------|---------------|-------|------------|
| | 0.001100352 | lbs/b.h.p.-hr | 0.5 | gr./bhp-hr |
| NOx | 0.005721831 | lbs/b.h.p.-hr | 2.6 | gr./bhp-hr |
| CO | - | lbs/b.h.p.-hr | - | gr./bhp-hr |
| SO2 | 0.000308099 | lbs/b.h.p.-hr | 0.14 | gr./bhp-hr |
| NMHC | 4.84155E-05 | lbs/b.h.p.-hr | 0.022 | gr./bhp-hr |
| PM | | | | |

Uncontrolled

Engine Emission Specs

| | Gal/hr | Power (kW) | Power (bhp) | Exhaust Mass Flow (kg/h) | Exhaust Mass Flow (acfm) | Power Output (eKW) | Exhaust Temperature after turbine (°C) | Exhaust Temperature after turbine (°F) |
|------------------|--------|------------|-------------|--------------------------|--------------------------|--------------------|--|--|
| Fuel Consumption | 232 | 3010 | 4036 | 17802 | 22895 | 2800 | 446 | 834.8 |
| 100% Load | 183 | 2257 | 3027 | 16060 | 20675 | 2084 | 417 | 782.6 |
| 75% Load | 127 | 1505 | 2018 | 12748 | 14470 | 1370 | 385 | 725 |
| 50% Load | 39 | 752 | 1008 | 8668 | 8968 | 654 | 337 | 638.6 |
| 10% Load | 31 | 301 | 404 | 6643 | 5741 | 226 | 303 | 577.4 |

100% Load

| Uncontrolled emissions (nominal) | g/kWh | lbs/bhp-hr | lbs/bhp-hr | lbs/hr |
|--|--------|------------|------------|--------|
| MTU 20V4000G83L 3B EPA Tier2 (1,800 rpm) | 7.8 | 5.8 | 0.013 | 51.7 |
| NOx | 0.50 | 0.37 | 0.0062 | 3.3 |
| CO | 0.18 | 0.13 | 0.0030 | 1.2 |
| HC | 0.060 | 0.045 | 0.0010 | 0.40 |
| PM | 0.0072 | 0.0054 | 0.00012 | 0.048 |
| SO2 | 628 | 468.3 | 1.03 | 4159.9 |
| CO2 | | | | |

75% Load

| Uncontrolled emissions (nominal) | g/kWh | lbs/bhp-hr | lbs/bhp-hr | lbs/hr |
|--|--------|------------|------------|--------|
| MTU 20V4000G83L 3B EPA Tier2 (1,800 rpm) | 5.4 | 4.0 | 0.009 | 26.8 |
| NOx | 0.70 | 0.52 | 0.0115 | 3.5 |
| CO | 0.24 | 0.18 | 0.0039 | 1.2 |
| HC | 0.080 | 0.060 | 0.0013 | 0.40 |
| PM | 0.0076 | 0.0057 | 0.00012 | 0.038 |
| SO2 | 662 | 493.7 | 1.09 | 3288.1 |
| CO2 | | | | |

50% Load

| Uncontrolled emissions (nominal) | g/kWh | lbs/bhp-hr | lbs/bhp-hr | lbs/hr |
|--|--------|------------|------------|--------|
| MTU 20V4000G83L 3B EPA Tier2 (1,800 rpm) | 4.5 | 3.4 | 0.007 | 14.9 |
| NOx | 1.0 | 0.75 | 0.0164 | 3.3 |
| CO | 0.39 | 0.22 | 0.0048 | 0.96 |
| HC | 0.18 | 0.13 | 0.0030 | 0.60 |
| PM | 0.0079 | 0.0059 | 0.00013 | 0.026 |
| SO2 | 693 | 516.8 | 1.14 | 2295 |
| CO2 | | | | |

25% Load

| Uncontrolled emissions (nominal) | g/kWh | lbs/bhp-hr | lbs/bhp-hr | lbs/hr |
|--|-------|------------|------------|--------|
| MTU 20V4000G83L 3B EPA Tier2 (1,800 rpm) | 4.4 | 3.3 | 0.007 | 7.3 |
| NOx | 2.4 | 1.8 | 0.00394 | 3.97 |
| CO | 0.52 | 0.39 | 0.0085 | 0.86 |
| HC | 0.29 | 0.22 | 0.0048 | 0.48 |
| PM | 0.005 | 0.0036 | 0.00008 | 0.008 |
| SO2 | 767 | 572.0 | 1.26 | 1269 |
| CO2 | | | | |

10% Load

| Uncontrolled emissions (nominal) | g/kWh | lbs/bhp-hr | lbs/bhp-hr | lbs/hr |
|--|-------|------------|------------|--------|
| MTU 20V4000G83L 3B EPA Tier2 (1,800 rpm) | 7.0 | 5.2 | 0.011 | 4.6 |
| NOx | 3.9 | 2.9 | 0.0064 | 2.6 |
| CO | 0.73 | 0.54 | 0.0012 | 0.48 |
| HC | 0.58 | 0.43 | 0.0095 | 0.384 |
| PM | 0.012 | 0.009 | 0.00020 | 0.008 |
| SO2 | 1195 | 891.1 | 1.96 | 792 |
| CO2 | | | | |

SO2 Emissions Basis

| SO2 emissions generated from diesel fuel consumed | ppm (TIER 3 and Tier 4 Limit) | 100% Load | 75% Load | 50% Load | 25% Load | 10% Load |
|---|-------------------------------|-----------|----------|----------|----------|----------|
| Sulfur Content of diesel fuel (ppm) | 15 | 15 | 15 | 15 | 15 | 15 |
| Density of Diesel Fuel (lb/gal) | 6.88 | 6.88 | 6.88 | 6.88 | 6.88 | 6.88 |
| Gal of Diesel Fuel Consumed per hour | 232 | 183 | 183 | 127 | 39 | 39 |
| Pounds (lb) sulfur in consumed diesel fuel | 0.024 | 0.019 | 0.019 | 0.013 | 0.0040 | 0.0040 |
| lbs/hr SO2 based on stoichiometric combustion | 0.048 | 0.038 | 0.038 | 0.026 | 0.008 | 0.008 |

Notes:
Nominal Emissions Values based on OEM Published Uncontrolled Emissions (Nominal) Data

